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Improved shunt damping with two negative capacitances: an efficient alternative to resonant shunt

M. Berardengo¹, O. Thomas², C. Giraud-Audine³ and S. Manzoni⁴

Abstract

This paper deals with piezoelectric shunt damping enhanced with negative capacitances. A novel electrical circuit layout is addressed, based on the use of two negative capacitances. It is shown that the shunt performances, in terms of vibration reduction and stability margins, are increased as compared with the classical single negative capacitance layouts. Then, the article focuses on the comparison of a simple resistive shunt, enhanced by a pair of negative capacitances, with a classical resonant shunt. It is shown that the newly proposed enhanced resistive shunt can show equivalent performances in terms of vibration attenuation than the resonant shunt, with at the same time an increased robustness to frequency detuning, in the case of mono-modal damping. The broadband control capability of the resistive shunt coupled to the new negative capacitance layout is also evidenced. The main part of the work is analytical, and then the model is validated by an extensive experimental campaign at the end of the paper.

Keywords

negative capacitance, piezoelectric shunt, resistive shunt, resonant shunt, vibration control, damping, smart structure

Introduction

Piezoelectric shunt is a well-known technique for vibration damping. Such a method is based on the electrical link between a piezoelectric actuator, bonded to a given vibrating structure, and a properly designed electrical network (Hagood and von Flotow, 1991). Usually, the most used shunt impedances for single mode control are a simple resistance (R shunt or resistive shunt) and the series of a resistance and an inductance (LR shunt or resonant shunt) (Hagood and von Flotow, 1991; Thomas et al., 2012; Yamada et al., 2010). The resonant shunt is usually preferred because it offers attenuation levels much higher than the resistive shunt (Hagood and von Flotow, 1991; Thomas et al., 2012) when the parameters of the shunt impedance are perfectly tuned on those of the mechanical eigenmode to damp. On the other hand, the resonant shunt is really sensitive to possible mistunings between the mechanical system and the electric impedance (e.g. due to thermal shifts causing a change of the mechanical eigenfrequency to control) (Berardengo et al., 2015a).

It has been proved in the literature (Thomas et al., 2012) that once the electric impedance is optimally tuned, the performance of the control depends just on the modal electromechanical coupling factor (MEMCF) (Ducarne et al., 2012; Thomas et al., 2009,

2012) of each mode of the electromechanical system (EMS, composed by the vibrating structure, the piezoelectric actuator and the shunt impedance). The MEMCF is a function of the geometrical, mechanical and electrical characteristics of the piezoelectric actuator and the structure, and it is also related to the distance between the natural frequencies of the EMS in short circuit (SC) and open circuit (OC) of the mode considered. The higher the MEMCF is, the higher the maximum achievable attenuation is (Thomas et al., 2012). As mentioned, the value of this parameter is fixed by the kind of structure and the actuator used and therefore also the maximum achievable attenuation level is fixed.

One possibility to improve the damping capability of the shunt control is to use negative capacitances (NCs) in the shunt impedance. Indeed, the use of NCs

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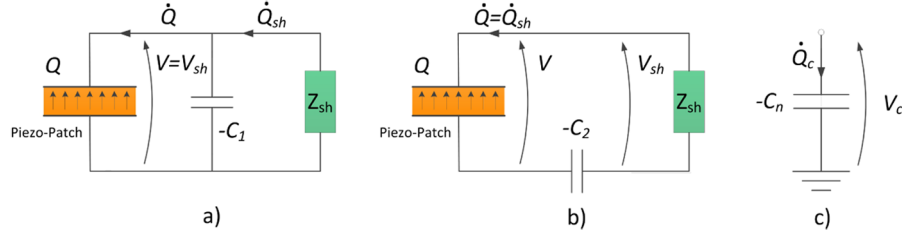


Figure 1. Piezoelectric shunt with addition of a NC: parallel configuration (a), series configuration (b) and definition of a NC (c). Here Z_{sh} is the shunt impedance.

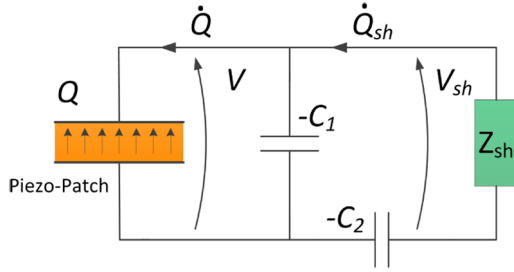


Figure 2. Piezoelectric shunt with addition of two NCs: the newly proposed series + parallel configuration. Here Z_{sh} is the shunt impedance.

has already been proved to enhance the attenuation provided by resistive (Beck et al., 2013, 2014; Behrens et al., 2003; Berardengo et al., 2016; Collet et al., 2011; de Marneffe and Preumont, 2008; Kodejška et al., 2012; Manzoni et al., 2012; Park and Baz, 2005) and resonant shunts (de Marneffe and Preumont, 2008; Heuss et al., 2014). Indeed, the effect of the NC in the shunt impedance is to artificially increase simultaneously the MEMCF (Berardengo et al., 2016) of all of the modes of an EMS. This effect can be fruitfully employed to improve a lot the attenuation achievable by means of a resistive shunt, keeping at the same time its robustness to possible mistunings. This makes the use of NCs in piezoelectric shunt really attractive. Nevertheless, it has to be remarked that a NC is an active component which does not exist in nature. It can be practically implemented by using a supplied circuit based on an operational amplifier (OP-AMP) (Date et al., 2000; Horowitz and Hill, 1989). This leads to the main drawback of NCs: they can lead to instabilities of the EMS, which need to be addressed.

A NC is traditionally coupled to the piezoelectric patch in parallel or series configuration (see Figure 1(a) and (b)), where the NC (i.e. $-C_1$ and $-C_2$ for the parallel and the series layout, respectively) is defined as $-C_n = Q_c/V_c$ (see Figure 1(c)). Recently, the authors proposed a new shunt circuit, based on a pair of NCs and able to further increase the attenuation levels provided by the use of a single NC (Berardengo et al., 2015b, 2016). In this new layout, one of the two NCs is connected in parallel (see $-C_1$ in Figure 2) and the

other in series (see $-C_2$ in Figure 2). According to the scheme of Figure 2, the new layout is thus defined as a series + parallel (SP) configuration.

The aim of this paper is to present some new advantages of the newly proposed SP layout. The SP configuration is indeed able to provide higher attenuation levels if compared with the simple series and parallel layouts, but it can also be used to achieve the same attenuation level guaranteeing a higher margin from instability, as demonstrated further in this paper. Furthermore, we will also compare a resistive shunt, enhanced by the SP layout, to the standard resonant shunt. This comparison will address the attenuation levels achievable by means of these shunt layouts as well as their robustness to mistuning.

The paper is structured as follows: the next two sections discuss the model of the EMS used in this work and introduce the use of NCs (and more particularly the SP), investigating its effects on the system. Furthermore, the stability issues and the achievable performances are addressed. Then, we present the advantages provided by the SP configuration if compared with the traditional series and parallel layouts and investigates its level of robustness. Furthermore, we compare the resistive shunt coupled to SP and the simple resonant shunt. Finally, the last section of the paper shows the experimental activity carried out to validate the model of the resistive shunt coupled to SP and its enhanced attenuation performance if compared with the series and parallel layouts.

Model of the electromechanical system

The model employed to describe the behaviour of the EMS is the one described by Thomas et al. (2012), refined by using a modified value for the piezoelectric patch capacitance, to guarantee a better description of the EMS behaviour in the case of a single degree of freedom approximation, as explained by Berardengo et al. (2016).

If the modal density of the EMS is low, a single-degree-of-freedom approximation can indeed be fruitfully employed to describe the behaviour of the EMS in a frequency band narrowed around the eigenfrequency associated to the mode considered. The original model

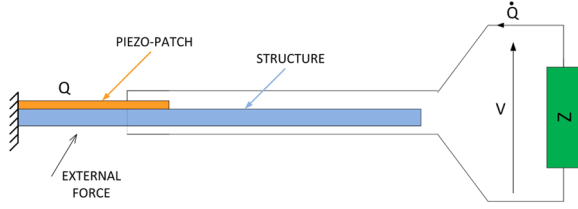


Figure 3. An arbitrary structure with a piezoelectric patch connected to a shunt impedance Z .

of Thomas et al. (2012), as well as its improved version for the single-degree-of-freedom approximation, are briefly summarized in this section in order to allow the reader to have a clear understanding of the analytical treatment developed for the new NC layout described in the following.

A generic elastic structure with one piezoelectric patch bonded on it and excited by an external force F is taken into account (see Figure 3). $U(x, t)$ is the displacement of any point x of the structure at time t . An arbitrary shunt impedance Z is connected to the piezoelectric patch and V is the voltage between the electrodes of the piezoelectric actuator; Q is the electric charge in one of the electrodes and, considering the convention of sign for V in Figure 3, Q is precisely the charge in the upper electrode. A reduced order model of the EMS can be obtained by expressing the displacement U in modal coordinates and considering N (theoretically $N \rightarrow +\infty$) vibration eigenmodes:

$$U(x, t) = \sum_{i=1}^N \Phi_i(x) q_i(t) \quad (1)$$

where q_i is the i th modal coordinate and Φ_i is the i th eigenmode of the structure (normalized to the unit modal mass). If a single-degree-of-freedom approximation is considered by keeping only the i th mode in the modal truncation, the behaviour of the EMS can be described for $\Omega \simeq \omega_i$ (where Ω is the angular frequency) as

$$\ddot{q}_i + 2\xi_i \omega_i \dot{q}_i + \omega_i^2 q_i - \chi_i V = F_i \quad (2)$$

$$C_{pi} V - Q + \chi_i q_i = 0 \quad (3)$$

where Equation (2) is the equation of motion of the EMS and it is coupled to the EMS electrical behaviour, described by Equation (3), by means of the coefficient χ_i . F_i is the modal forcing, that depends on F and the i th mode shape Φ_i . Here ω_i is the i th natural frequency of the EMS in short circuit, ξ_i is the i th structural damping factor and χ_i is a modal coupling coefficient, which is related to the energy transfer between the i th mode shape and the piezoelectric patch. The values of χ_i depend on the geometrical, electrical and mechanical characteristics of the piezoelectric actuator and the

structure, and on the position of the actuator. Those χ_i coefficients can be computed with either an analytical model (Ducarne et al., 2012) or by a finite element discretization (Thomas et al., 2009). It should be noted that Φ_i are the eigenmodes of the EMS with the piezoelectric patch in SC (with $V = 0$).

The term C_{pi} in Equation (3) is the value of the capacitance of the piezoelectric patch at frequencies above ω_i when a single-degree-of-freedom approximation is performed on the complete model, and it is defined as

$$C_{pi} = C_\infty + \sum_{n=i+1}^N \frac{\chi_n^2}{\omega_n^2} \quad (4)$$

where C_∞ is the electrical blocked capacitance of the piezoelectric patch (with $U(x, t) = 0 \forall x \Rightarrow q_i = 0 \forall i$). The second term of the right-hand side of Equation (4) accounts for the contribution to the capacitance value of the modes higher than the i th, which are neglected in the single-degree-of-freedom approximation. This static correction, introduced in Berardengo et al. (2016), is an improvement to the model proposed in Thomas et al. (2012) and allows us to obtain a better description of the EMS when a single-degree-of-freedom approximation is taken into account. The value of C_{pi} can be estimated by measuring the capacitance of the piezoelectric patch between the i th and $(i+1)$ th modes. More details about the definition of C_{pi} and its estimation can be found in Berardengo et al. (2016).

The model described by Equations (2) and (3) is related to the case of a simple piezoelectric shunt where no NC is included in the circuit. Now the addition of NCs is addressed, according to the schemes of Figures 1 and 2. Following the procedure described in Berardengo et al. (2016), it is convenient to apply the change of variables:

$$\bar{V}_{sh} = V_{sh} \sqrt{C_{eq}}, \quad \bar{Q}_{sh} = \frac{Q_{sh}}{\sqrt{C_{eq}}} \quad (5)$$

where V_{sh} and Q_{sh} are the voltage and the charge seen by the shunt impedance Z_{sh} , and C_{eq} is an equivalent capacitance, defined in Table 1. Such an equivalent capacitance depends on the NC connected to the capacitance of the piezoelectric patch, and thus depends on the type of connection (parallel, series or SP). Substituting Equation (5) in Equations (2) and (3), the following system of equations is obtained:

$$\ddot{q}_i + 2\xi_i \omega_i \dot{q}_i + (\omega_i^{sc})^2 q_i - \omega_i \tilde{k}_i \bar{V}_{sh} = F_i \quad (6)$$

$$\ddot{q}_i + 2\xi_i \omega_i \dot{q}_i + (\omega_i^{oc})^2 q_i - \omega_i \tilde{k}_i \bar{Q}_{sh} = F_i \quad (7)$$

$$\bar{V}_{sh} - \bar{Q}_{sh} + \omega_i \tilde{k}_i q_i = 0 \quad (8)$$

It should be noted that Equations (6) and (7) play the same role: one is expressed as function of \bar{V}_{sh} (i.e. Equation (6)) and the other as function of \bar{Q}_{sh} (i.e.

Table 1. Parameters of the EMS enhanced by a single NC in parallel and series configuration and by two NCs for the series + parallel (SP) configuration.

		Parallel configuration	Series configuration	SP configuration
SC frequency	ω_i^{sc}	ω_i	$\sqrt{\omega_i^2 - \frac{\chi_i^2}{C_2 - C_{pi}}}$	$\sqrt{\omega_i^2 - \frac{\chi_i^2}{C_1 + C_2 - C_{pi}}}$
OC frequency	ω_i^{oc}	$\sqrt{\omega_i^2 + \frac{\chi_i^2}{C_{pi} - C_1}}$	$\hat{\omega}_i = \sqrt{\omega_i^2 + \frac{\chi_i^2}{C_{pi}}}$	$\sqrt{\omega_i^2 + \frac{\chi_i^2}{C_{pi} - C_1}}$
Equivalent capacitance	C_{eq}	$C_{pi} - C_1$	$\frac{C_{pi} C_2}{C_2 - C_{pi}}$	$\frac{(C_{pi} - C_1) C_2}{C_1 + C_2 - C_{pi}}$
EMEMCF	\tilde{k}_i	$\frac{k_i}{\sqrt{1 - \frac{C_1}{C_{pi}}}}$	$\frac{k_i}{\sqrt{1 - \frac{C_{pi}}{C_2}}}$	$\frac{k_i}{\sqrt{\left(1 - \frac{C_1}{C_{pi}}\right) \left(1 + \frac{C_1}{C_2} - \frac{C_{pi}}{C_2}\right)}}$

Equation (7)). Here ω_i^{sc} and ω_i^{oc} are respectively the natural frequency of the EMS with the shunt short-circuited ($V_{sh} = 0$) or in open circuit ($Q_{sh} = 0$), defined in Table 1. It should be noted that their values depend on the NCs C_1 and C_2 . The term \tilde{k}_i , which appears naturally in the system, is defined as the enhanced modal electromechanical coupling factor (EMEMCF) and assumes the following expression:

$$\tilde{k}_i = \sqrt{\frac{(\omega_i^{oc})^2 - (\omega_i^{sc})^2}{\omega_i^2}} \quad (9)$$

We can observe that if we fix $\omega_i^{sc} = \omega_i$ and $\omega_i^{oc} = \hat{\omega}_i$ (where $\hat{\omega}_i$ and ω_i are the OC and SC eigenfrequency respectively of the EMS without the addition of any NCs), we obtain the classical expression of the MEMCF k_i (which is close to the i th effective coupling factor) (Berardengo et al., 2016; Thomas et al., 2012):

$$k_i = \frac{\chi_i}{\omega_i \sqrt{C_{pi}}} = \sqrt{\frac{(\hat{\omega}_i)^2 - (\omega_i)^2}{\omega_i^2}} \quad (10)$$

Therefore the EMEMCF is a parameter analogous to the MEMCF, but enhanced by the presence of the NCs. The analytical formulations of all of these parameters involved in the definition of the EMEMCF \tilde{k}_i depend on the layout used to connect the NCs and they are gathered in Table 1.

Enhanced resistive shunt

Model

If a simple resistance R_{sh} is used as the shunt impedance Z_{sh} in Figures 1 and 2, one has

$$V_{sh} = -R_{sh} \dot{Q}_{sh} \Rightarrow \bar{V}_{sh} = -\tau_e \dot{\bar{Q}}_{sh} \quad \text{with } \tau_e = R_{sh} C_{eq} \quad (11)$$

where τ_e is the electric time constant and where the change of variables of Equation (5) has been used. Using Equations (6), (7) and (8), the following

frequency response function (FRF) can be defined (Berardengo et al., 2016):

$$H_i(\Omega) = \frac{q_i}{F_i} = \frac{1 + j\tau_e \Omega}{(\omega_i^{sc})^2 - (1 + 2\xi_i \omega_i \tau_e) \Omega^2 + j\Omega [\tau_e (\omega_i^{oc})^2 + 2\xi_i \omega_i - \tau_e \Omega^2]} \quad (12)$$

where j is the imaginary unit.

According to Berardengo et al. (2016), the analytical expression of this FRF is the same of that describing a pure resistive shunt without NCs added in the circuit (Thomas et al., 2012), except that one has to use the proper value of the parameters in Equation (12): $\omega_i^{sc} = \omega_i$, $\omega_i^{oc} = \hat{\omega}_i$ and $C_{eq} = C_{pi}$. Thanks to this equivalence between the analytical representations of the EMS with and without NCs, the same procedure presented in Thomas et al. (2012) for the optimal tuning of R_{sh} and for the estimation of the attenuation performance can be used here. This procedure allows us to define the optimal value of τ_e (named τ_e^{opt}), and thus of R_{sh} , which minimizes the resonance peak amplitude at given mode, as

$$\tau_e^{opt} = \sqrt{\frac{2}{(\omega_i^{oc})^2 + (\omega_i^{sc})^2}} \simeq \frac{1}{\omega_i} \sqrt{\frac{2}{\tilde{k}_i^2 + 2}} \quad (13)$$

It depends only on the EMEMCF \tilde{k}_i and on the natural frequency of the targeted mode.

The performances of the present enhanced resistive shunt are evaluated by the resonance peak attenuation parameter A_{dB} , measured at the resonance of the mode on which τ_e has been tuned, defined as (Berardengo et al., 2016)

$$A_{dB} = 20 \log_{10} \frac{H_{sc}}{H_{sh}} \simeq 20 \log_{10} \frac{\tilde{k}_i^2 + 2\sqrt{2}\xi_i \sqrt{2 + \tilde{k}_i^2}}{4\xi_i \sqrt{1 - \xi_i^2}} \quad (14)$$

where H_{sc} is the FRF peak amplitude of the EMS in SC and without NCs (i.e. uncontrolled EMS), while H_{sh} is

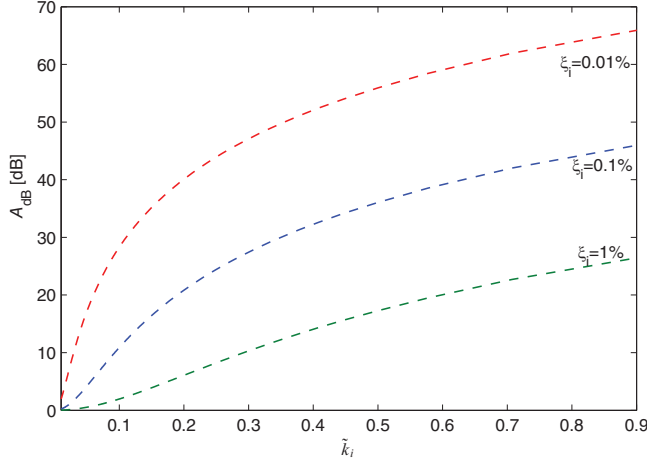


Figure 4. Trend of A_{dB} (see Equation (14)) as a function of \tilde{k}_i for different values of ξ_i .

the peak amplitude of the FRF when the optimized shunt is employed (i.e. $\tau_e = \tau_e^{opt}$). The performance of the control (measured by A_{dB}) depends only on the structural damping ξ_i and on the EMEMCF \tilde{k}_i of the targeted mode, as illustrated in Figure 4; it increases as a function of \tilde{k}_i .

Stability of the negative capacitance

As mentioned previously, the NC is an active component which can be built in practice using an OP-AMP. The use of active components in the shunt impedance makes the control strategy no more passive. Therefore, the study of the stability of the system is mandatory. To this purpose, the Routh–Hurwitz criterion (Gopal, 2002) has been applied to the FRF of Equation (12) and the stability conditions are found to be

$$\begin{aligned} \text{parallel : } & C_1 < C_{pi} \\ \text{series : } & C_2 > C_{pi}(1 + k_i^2) \\ \text{SP : } & C_1 < C_{pi} \quad \& \quad C_2 + C_1 > C_{pi}(1 + k_i^2) \end{aligned} \quad (15)$$

It should be noted that there are two stability conditions for the SP because two NCs are used together.

Since Equation (12) is the EMS FRF when a single degree of freedom is considered, Equation (15) gives the stability limits associated just to the mode taken into account. However, when a stability analysis is carried out, the whole EMS must be taken into account in order to avoid problems due to spillover (Burns, 2001). Therefore, the stability conditions related to the EMS are the strictest ones found by applying the Routh–Hurwitz criterion to all of the modes of the EMS. Such stability conditions are found to be

$$\begin{aligned} \text{parallel : } & C_1 < C_\infty \\ \text{series : } & C_2 > C_0 \\ \text{SP : } & C_1 < C_\infty \quad \& \quad C_2 + C_1 > C_0 \end{aligned} \quad (16)$$

where $C_0 = C_{pi}(1 + k_i^2)$ is the value of the capacitance of the piezoelectric patch at the null frequency (Berardengo et al., 2016). It should be noted that the conditions of Equation (16) depend on all of the modes of the structure.

It is worth highlighting that when the stability conditions of Equation (16) are fulfilled, the value of \tilde{k}_i is bigger than the original MEMCF k_i (see Table 1) and its value depends on the value of the NC which is used: the closer the NC is to the stability limit, the higher the value of \tilde{k}_i is.

Table 1 provides evidence of another interesting aspect related to the use of a NC. The NC in parallel configuration does not change the SC eigenfrequency (i.e. the SC eigenfrequency is the same with and without NC), while the OC eigenfrequency is shifted. If the condition of Equation (16) for the parallel layout is fulfilled, the OC eigenfrequency increases thanks to the use of the NC. This also explains the reason why the value of \tilde{k}_i is increased if compared with k_i : the SC and OC eigenfrequencies are farther than in the case of absence of NC. The series configuration of the NC again makes the SC and OC eigenfrequencies to be farther than in the case of absence of the NC. This time the OC eigenfrequency does not change adding or removing the NC, but the SC eigenfrequency is shifted towards lower frequency values. Now, if we consider the SP configuration, we note that the SC and OC eigenfrequencies are both shifted at the same time: the SC towards lower frequency values and the OC towards higher frequency values, and this explains why the SP is able to increase the value of \tilde{k}_i if compared with the traditional series and parallel layouts (see the next section).

The SP configuration could be coupled to whatever kind of shunt impedance (e.g. a LR shunt) because the effect on the value of \tilde{k}_i is not related to the layout of Z_{sh} . Previously in this section we have considered a simple resistance as shunt impedance. Usually, the pure resistive shunt is avoided due to its low attenuation performance but one of the goal of this paper is to show that the enhancement of the MEMCF provided by the SP NC is able to make this kind of shunt really competitive, keeping at the same time its advantages: ease of use, robustness to uncertainty and biases, and capability to damp many modes together on a wide frequency range.

Advantages of the resistive series + parallel configuration

In this section the advantages provided by the use of the SP configuration in terms of performances and robustness are evidenced and its behaviour is compared with that of traditional NC layouts: series and parallel. To this purpose, it is convenient to introduce four indexes:

Table 2. EMEMCF as a function of the parameters β .

	R shunt	Parallel configuration	Series configuration	SP configuration
EMEMCF	\tilde{k}_i	k_i	$\frac{k_i}{\sqrt{1-\beta_1}}$	$\frac{k_i}{\sqrt{\frac{(1-\beta_{sp1})(1-\beta_{sp2})}{1-\beta_{sp1}\beta_{sp2}}}}}$

$$\beta_1 = \frac{C_1}{C_{pi}}, \quad \beta_2 = \frac{C_{pi}}{C_2}, \quad \beta_{sp1} = \frac{C_1}{C_{pi}}, \quad \beta_{sp2} = \frac{C_{pi}}{C_1 + C_2} \quad (17)$$

where β_1 is related to the parallel configuration, β_2 to the series, and β_{sp1} and β_{sp2} to the SP configuration. These indices are positive and define how much the NCs are close to the value of C_{pi} : the closer the β indexes are to 1, the closer the NCs are to C_{pi} . Null values of β means, instead, absence of the NCs (i.e. simple piezoelectric shunt). It should be noted that the β coefficients are strictly smaller than the value of 1 because in this case the NC value would be over the instability threshold (see Equation (16)). According to Equation (17) and to Table 1, the EMEMCF \tilde{k}_i can be defined also as function of the β coefficients as shown in Table 2.

Enhancement of attenuation and stability margins

The expressions of the EMEMCF in Tables 1 and 2 allow us to highlight that when the values of the β coefficients increase, the values of the EMEMCF increase as well: the closer the NCs are to the stability limits, the higher the value of \tilde{k}_i is. This increase of \tilde{k}_i leads to an increase of the attenuation A_{dB} (see Equation (14)) and explains why the shunt performances are improved.

Despite the stability limits of Equation (16) imply that values of β equal to 1 cannot be reached, it is still possible to achieve high values of β and thus of \tilde{k}_i . To measure the coupling factor enhancement, we define the following quantity:

$$G = \tilde{k}_i/k_i \quad (18)$$

Figure 5 shows that, given a fixed value of β ($\beta_1 = \beta_2 = \beta_{sp1} = \beta_{sp2}$), the SP configuration enables us to obtain higher values of \tilde{k}_i if compared with the series and parallel layouts (these curves are obtained using the expressions of Table 2). This is a remarkable result since, according to Equation (14) and Figure 4, this implies that the SP configuration allows to have higher attenuation levels. Therefore, the SP layout is able to enhance the attenuation levels achievable by means of the traditional series and parallel layouts.

As already mentioned, it is not possible to pull the β values to 1 because the stability limits discussed previously must be taken into account. Hence, there exists an unstable area, as shown in grey in Figure 5, whose

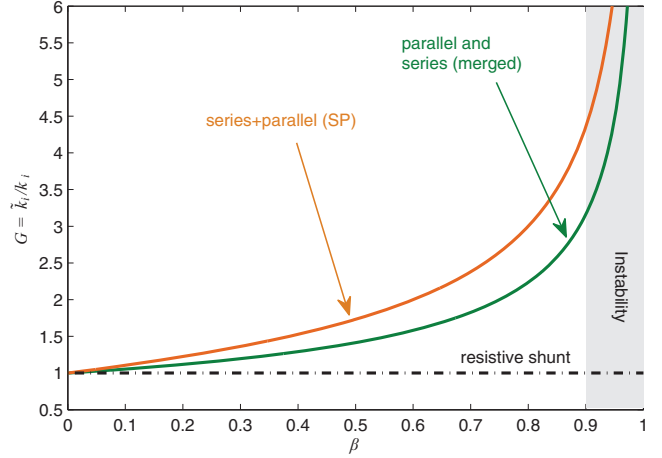


Figure 5. Trend of G as function of β (with $\beta = \beta_1 = \beta_2 = \beta_{sp1} = \beta_{sp2}$) for different negative capacitance layouts: parallel (Figure 1(a)), series (Figure 1(b)) and SP (Figure 2).

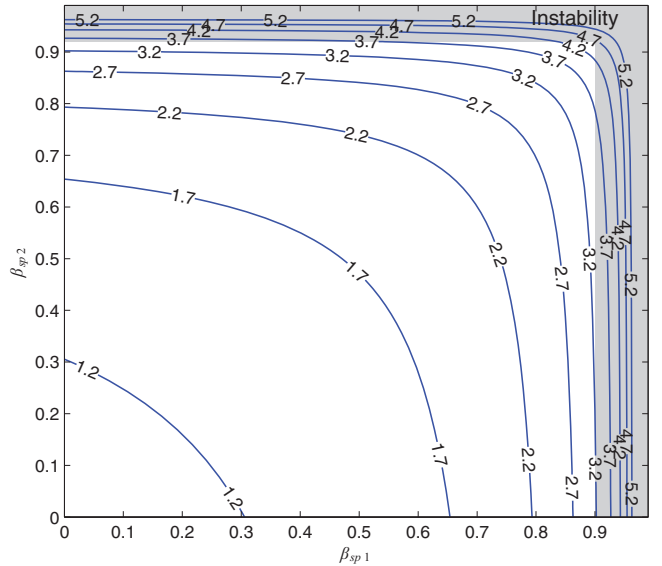


Figure 6. Relationship between β_{sp1} and β_{sp2} providing given values of G .

extension depends upon the system and the mode taken into account (Berardengo et al., 2016).

The same considerations can be drawn by looking at Figure 6 where the G value for the SP configuration (last column of Table 2) is shown in isolines as a function of β_{sp1} and β_{sp2} . This plot also shows the G values

achievable with the NC in parallel (values for $\beta_{sp2} = 0$) and in series (values for $\beta_{sp1} = 0$) configurations as well, thus leading to a more general and detailed comparison.

It should be noted that the value of G increases in the areas of the figure far from the plot axes, thus highlighting the benefits provided by the SP configuration. To illustrate this point, consider, as an example, a series or parallel NC configuration with $G = 1.7$. This value of G is achieved by using $\beta_2 \simeq 0.65$ for the series and $\beta_1 \simeq 0.65$ for the parallel (see Table 2). These values of β_2 and β_1 can be found also by looking at the intersection points between the isoline with a value of G equal to 1.7 and the axes in Figure 6. If we use a SP configuration with $\beta_{sp1} = \beta_{sp2} = 0.65$ (thus we move away from the figure axes), we obtain a higher G value: about 2.17.

Figure 6 provides evidence that the SP configuration can be employed even to achieve another remarkable goal: it is able to provide the same value of \tilde{k}_i , and thus of the attenuation A_{dB} , by employing lower values of the β coefficients with respect to the simple parallel and series layouts. This allows to use NC values which guarantee a higher margin from the instability limits. Indeed, the isolines of Figure 6 show that the pairs of β_{sp1} and β_{sp2} which allow us to have the same G value than that achievable with a given value of β_1 or β_2 are such that β_{sp1} and β_{sp2} are lower than β_1 or β_2 . This is a remarkable result especially when structures with low values of k_i (e.g. thick metal structures) are taken into account. In these cases, the value of the NC must be very close to the instability in order to achieve a good attenuation level, thus leading to more risky working conditions. The use of SP allows us instead to achieve such a high level of attenuation with a higher reliability if compared with the series and the parallel configurations. Indeed, if a shift of some of the EMS parameters occurs (e.g. due to thermal shifts), the SP turns out to be more reliable than the traditional configurations because of the lower values of the β coefficients which can be employed, thus showing higher robustness in terms of stability.

Robustness of the resistive shunt coupled to series + parallel NCs

An important feature of every control system is its capability to be robust against uncertainties and system changes. Indeed, as an example, a thermal shift could cause a change of the eigenfrequency associated to the mode to control, thus leading to a mistuning and then to the worsening of the attenuation performance. Therefore, in order to have a full understanding of the piezoelectric shunt effectiveness, even the EMS behaviour in mistuned conditions must be taken into account. To this purpose, the robustness of the resistive shunt coupled to the SP layout has been studied by

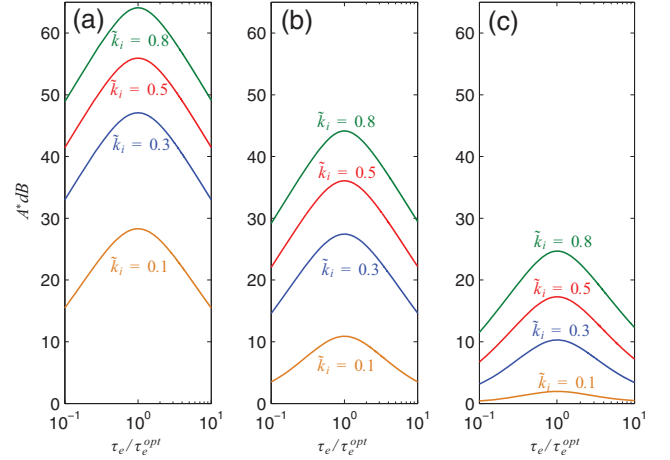


Figure 7. Trend of A_{dB}^* as a function of τ_e/τ_e^{opt} for different values of \tilde{k}_i : $\xi_i = 10^{-4}$ (a), $\xi_i = 10^{-3}$ (b) and $\xi_i = 10^{-2}$ (c).

computing the attenuation A_{dB}^* in mistuned conditions. This latter index is the attenuation provided by the shunt when a value of $\tau_e \neq \tau_e^{opt}$ is used. Here A_{dB}^* is defined as

$$A_{dB}^* = 20 \log_{10} \frac{H_{sc}}{H_{max}} \quad (19)$$

where H_{max} is the FRF peak of the EMS with $\tau_e \neq \tau_e^{opt}$, computed numerically by means of Equation (12).

The use of a generic value of $\tau_e \neq \tau_e^{opt}$ is representative of a mistuned working condition where the shunt is mistuned. This situation can occur if the shunt is not well tuned or if the natural frequency of the targeted mode has changed as compared with its reference value ω_i used for the tuning of the shunt. Since τ_e^{opt} is inversely proportional to ω_i (see Equation (13)) and if we denote by ω_i^* the current value of the natural frequency, one has $\tau_e/\tau_e^{opt} = \omega_i^*/\omega_i$.

Figure 7 shows A_{dB}^* for different values of ξ_i and \tilde{k}_i (it should be noted that the value of A_{dB}^* is equal to A_{dB} when $\tau_e = \tau_e^{opt}$, compare Figure 7 and Figure 4). It is evident that the higher \tilde{k}_i is, the higher the attenuation is, even in mistuned conditions. Indeed, the same value of τ_e/τ_e^{opt} guarantees higher attenuation levels when \tilde{k}_i is high than in the case it is low. Therefore, the increase of \tilde{k}_i accomplished by using the SP configuration allows us to assure a high level of attenuation even in presence of mistuning. This means that the use of the SP layout is advantageous if compared with the simple parallel and series NC configurations because it allows us to achieve higher increases of the value of \tilde{k}_i .

Figure 8 shows the same curves of Figure 7 shifted downwards by a quantity equal to the corresponding optimal attenuation value A_{dB} , and therefore such curves show the loss of attenuation. It is noteworthy to underline that the loss of performance does not depend on the value of \tilde{k}_i and ξ_i when the value of A_{dB}^* is high enough

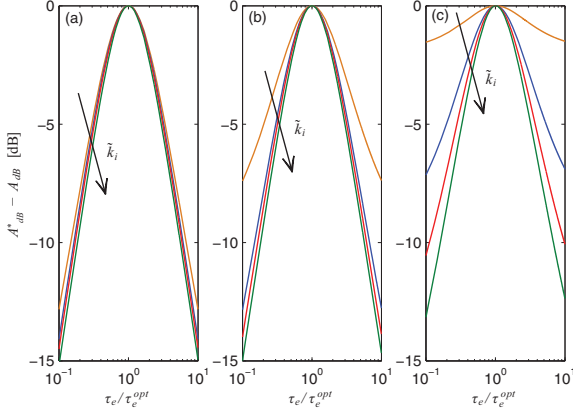


Figure 8. Trend of $A_{dB}^* - A_{dB}$ as a function of τ_e/τ_e^{opt} for different values of \tilde{k}_i (i.e. 0.1, 0.3, 0.5 and 0.8): $\xi_i = 10^{-4}$ (a), $\xi_i = 10^{-3}$ (b) and $\xi_i = 10^{-2}$ (c).

(higher than about 10 dB), since in this case all of the curves of the three plots of Figure 8 are almost superimposed. This means that the percentage loss of performance depends just on the percentage mistuning on τ_e (i.e. τ_e/τ_e^{opt}). When the attenuation is lower than about 10 dB, the plots of Figure 8 show a change of behaviour (e.g. the curve for $\tilde{k}_i = 0.1$ in Figure 8(b)) but it is still possible to notice that the features of the system have no influence on the trend of the loss of attenuation. Indeed, the curve with $\tilde{k}_i = 0.1$ in Figure 7(b) and that with $\tilde{k}_i = 0.3$ in Figure 7(c) show almost the same value of the optimized attenuation A_{dB} and their trends for $\tau_e \neq \tau_e^{opt}$ are almost equal (the curve with $\tilde{k}_i = 0.1$ in Figure 8(b) and that with $\tilde{k}_i = 0.3$ in Figure 8(c) match if plotted on the same graph).

$$H_i^{LR}(\Omega) = \frac{q_i}{F_i} = \frac{1 - \frac{\Omega^2}{\omega_e^2} + 2j\xi_e \frac{\Omega}{\omega_e}}{\frac{\Omega^4}{\omega_e^4} - \Omega^2 \left(1 + \frac{\hat{\omega}_i^2}{\omega_e^2} + 4\xi_i \xi_e \frac{\omega_i}{\omega_e}\right) + \omega_i^2 + 2j\Omega \left[\frac{\xi_e}{\omega_e} (\hat{\omega}_i^2 - \Omega^2) + \xi_i \omega_i \left(1 - \frac{\Omega^2}{\omega_e^2}\right)\right]} \quad (24)$$

The benefits provided by the use of NCs with SP configuration have been discussed so far. Now, the resistive shunt coupled to SP (RSP in the following) is compared to the shunt impedance mostly employed for single mode damping: the LR shunt. This comparison is addressed in the next section.

Comparison between RSP and LR shunt

The most frequently used shunt impedance for mono-modal attenuation is the LR shunt. This section focuses on the comparison between this well-established approach and the newly proposed RSP shunt.

Resonant shunt model

The LR shunt is composed by the series of a resistance R_e and an inductance L_e . These two elements form a

resonant circuit together with the capacitance C_{pi} of the piezoelectric patch. Therefore, the LR shunt can be considered as the electrical equivalent of the mechanical tuned mass damper (Preumont, 2011) and thus as a result it is really effective for mono-modal control. We consider here a LR shunt directly coupled to the piezoelectric element with no NC enhancement ($V = V_{sh}$, $Q = Q_{sh}$, $\tilde{k}_i = k_i$). In this case, the following relation holds:

$$V_{sh} = -R_e \dot{Q}_{sh} - L_e \ddot{Q}_{sh} \quad (20)$$

Using the change of variables of Equation (5) with $C_{eq} = C_{pi}$ and introducing it in Equation (8), the latter is replaced by

$$\frac{1}{\omega_e^2} \ddot{Q}_{sh} + \frac{2\xi_e}{\omega_e} \dot{Q}_{sh} + \bar{Q}_{sh} - \omega_i k_i q_i = 0 \quad (21)$$

where ω_e is the electrical angular frequency and ξ_e the electrical damping ratio, defined by

$$\omega_e = \frac{1}{\sqrt{L_e C_{pi}}}, \quad \xi_e = \frac{R_e}{2} \sqrt{\frac{C_{pi}}{L_e}} \quad (22)$$

Their optimal values for single mode control have been investigated in Thomas et al. (2012) and read

$$\omega_e^{opt} = \hat{\omega}_i = \omega_i \sqrt{1 + k_i^2}, \quad \xi_e^{opt} = k_i \sqrt{\frac{3}{8}} \quad (23)$$

The expression of the FRF q_i/F_i obtained by using Equations (2), (3) and (21) is (Thomas et al., 2012)

Finally, according to Thomas et al. (2012), the attenuation provided by the optimized LR shunt, named here A_{dB}^{LR} , can be computed as

$$A_{dB}^{LR} = 10 \log_{10} \frac{\text{num}(k_i, \xi_i)}{8(6k_i^2 + 8 - 3k_i \sqrt{2(1 + k_i^2)}) \xi_i^2 (1 - \xi_i^2)} \quad (25)$$

where

$$\begin{aligned} \text{num}(k_i, \xi_i) = & 8 \left[9k_i^4 + 17k_i^2 + 8 - k_i \sqrt{2(1 + k_i^2)} (6k_i^2 + 7) \right] \xi_i^2 \\ & + 16\sqrt{3}k_i(1 + k_i^2) \left(\sqrt{2(1 + k_i^2)} - k_i \right) \xi_i \\ & - 3k_i^3 \sqrt{2(1 + k_i^2)} (1 + k_i^2) + 6k_i^6 + 14k_i^4 + 8k_i^2 \end{aligned} \quad (26)$$

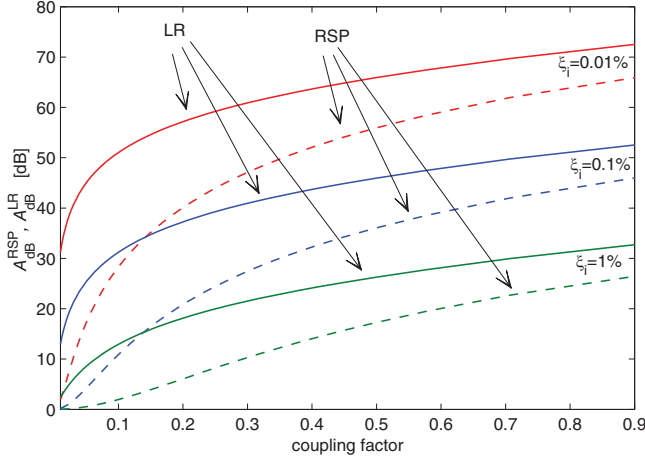


Figure 9. Trend of A_{dB}^{RSP} and A_{dB}^{LR} as functions of the coupling factor: k_i for the LR shunt and \tilde{k}_i for the RSP shunt.

RSP and LR shunt performance comparisons

This section compares the RSP and LR shunts in terms of attenuation performance when they are optimally tuned on the mechanical eigenmode to be damped (i.e. the values of τ_e , ω_e and ξ_e are the ones of Equations (13) and (23)).

Figure 9 shows the comparison between A_{dB} (Equation (14)) for the RSP (named A_{dB}^{RSP} from here on) and A_{dB}^{LR} (Equation (25)). Those two attenuation indexes are shown, for different values of ξ_i , as functions of the coupling factors: k_i for the resonant shunt and \tilde{k}_i for the RSP. One can remark that the higher the coupling factor is, the smaller the difference between the attenuations of the LR and RSP shunts is. Therefore, when the coupling factor is increased, the resistive shunt becomes more and more competitive with respect to the LR shunt.

However, in this case, the comparison between the two shunt techniques must not be carried out considering the same value of the coupling factor, i.e. $k_i = \tilde{k}_i$, since the resistive shunt has a higher coupling factor thanks to the use of the NCs in SP configuration (i.e. $\tilde{k}_i > k_i$). In light of this, Figure 10 is presented. It shows the trend of A_{dB}^{RSP} and A_{dB}^{LR} for different $G = \tilde{k}_i/k_i$ and ξ_i values as function of k_i . The graph clearly shows that the use of the RSP becomes competitive (or even advantageous) if compared with LR shunt and this result is achieved thanks to the enhanced value of the MEMCF accomplished by using the SP.

To give another insight into the performance comparison between RSP and LR shunt, we define k_{lim} as the value of k_i for which $A_{dB}^{RSP} = A_{dB}^{LR}$ (i.e. defined in Figure 10 by the intersection of the dashed black curve with the others). Here k_{lim} is by definition a function of G and ξ_i . Figure 11 shows k_{lim} as a function of G for several values of ξ_i . One remarkable result is that the dependence of k_{lim} on ξ_i is almost negligible. Therefore,

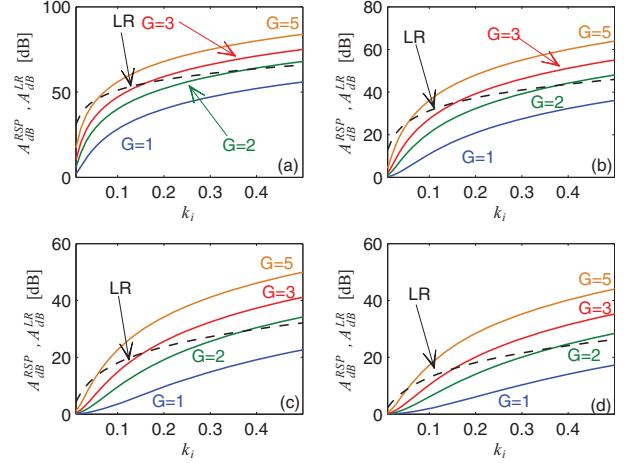


Figure 10. Trend of A_{dB}^{RSP} (coloured solid lines) and A_{dB}^{LR} (black dashed lines) as a function of k_i for different values of ξ_i : $\xi_i = 10^{-4}$ (a), $\xi_i = 10^{-3}$ (b), $\xi_i = 5 \times 10^{-3}$ (c) and $\xi_i = 10^{-2}$ (d).

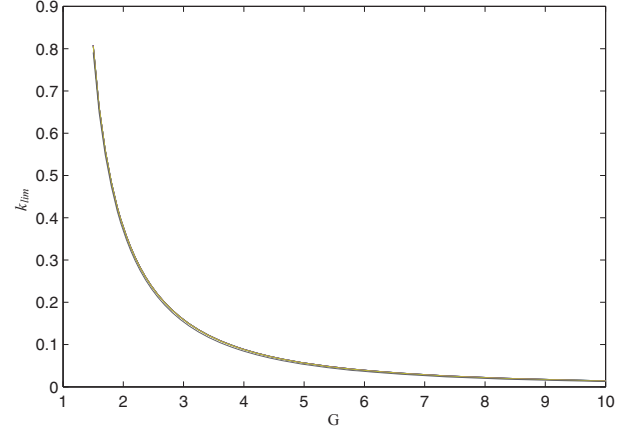


Figure 11. Trend of k_{lim} as a function of G for different values of ξ_i (i.e. from 10^{-8} to 10^{-2}). The lines are not plotted for G values lower than 1.5 because k_{lim} would be higher than 1, which is not physical.

k_{lim} can be considered a function of G only: it depends just on the MEMCF enhancement due to the use of NCs, whichever system is considered. As a consequence, Figure 11 plays an important role in the design process since it gives the relation between G and k_i for which the RSP shunt is as powerful as the traditional LR shunt. For instance, for values of G and k_i achievable in practical applications, such as $G = 2.7$ (see further in the paper, i.e. the section related to the experimental tests) and k_i greater than 0.2 (see Ducarne et al., 2012), the RSP shunt guarantees better performances than the traditional LR shunt.

Robustness of LR shunt

This section addresses the robustness of a LR shunt to a detuning of the electrical parameter, as a preliminary step towards its comparison with the behaviour of the

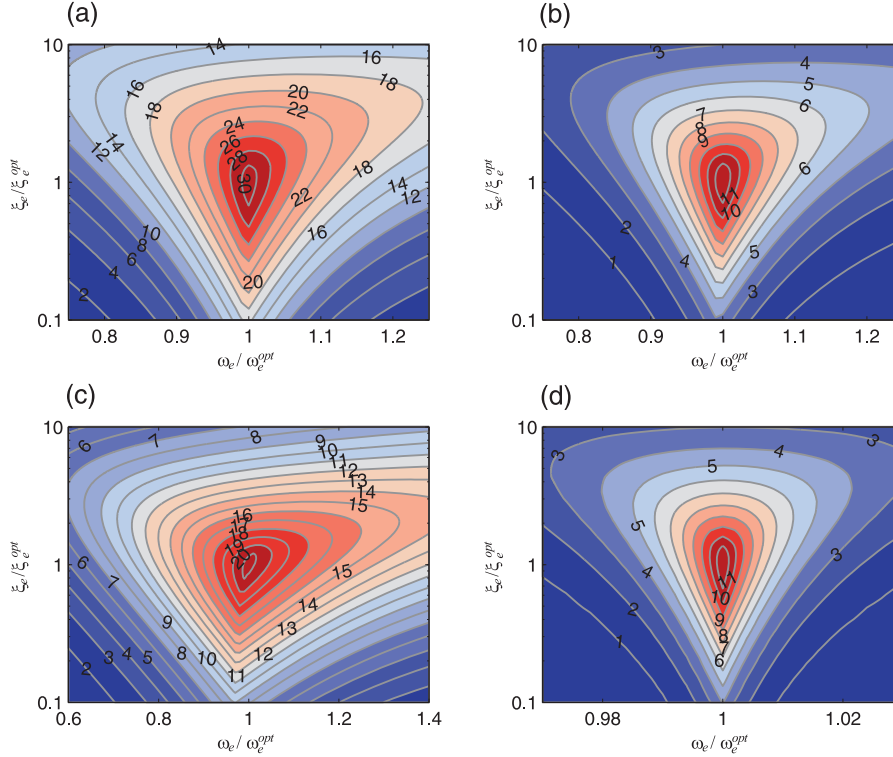


Figure 12. Attenuation A_{dB}^{*LR} provided by LR shunt in the presence of mistuning on the electrical parameters: (a) $(k_i, \xi_i) = (0.1, 10^{-3})$; (b) $(k_i, \xi_i) = (0.1, 10^{-2})$; (c) $(k_i, \xi_i) = (0.3, 10^{-2})$; (d) $(k_i, \xi_i) = (0.01, 10^{-3})$.

RSP shunt (see the next section). It is well known in the literature (Behrens et al., 2003; Berardengo et al., 2015a) that the traditional LR shunt undergoes significant attenuation losses when biases occur on the shunt parameters. As already done for the resistive shunt coupled to the SP layout, we analyse the effect of a mistuning of the shunt parameters on the performance in terms of vibration attenuation. Using Equation (24), we compute A_{dB}^{*LR} , defined by Equation (19), with H^{max} being the FRF peak of the EMS with the mistuned shunt, i.e. with $\omega_e \neq \omega_e^{opt}$ and $\xi_e \neq \xi_e^{opt}$. This represents a strict mistuning of the shunt, but also a change of the structural characteristics of the EMS since $\omega_e / \omega_e^{opt} = \omega_i / \omega_i^*$, with ω_i^* the current value of the EMS natural frequency, different from its reference value ω_i .

Figure 12 shows the attenuation performance A_{dB}^{*LR} for LR shunt in the presence of mistuning, i.e. as a function of $\omega_e / \omega_e^{opt} = \omega_i / \omega_i^*$ and ξ_e / ξ_e^{opt} , for some systems chosen as examples (i.e. different values of ξ_i and k_i). These figures show that the vibration attenuation is drastically reduced when the shunt impedance is not perfectly tuned on the mode which must be damped. We also observe, for instance by looking at the limits of the axes on the plots, that the LR shunt is much less robust to a detuning on the electrical frequency (a change of ω_e) than to a detuning of the electrical damping (a change of ξ_e).

Figure 13 shows the trend of $A_{dB}^{*LR} - A_{dB}^{LR}$ for the same cases investigated in Figure 12. The shapes of the plots of Figure 13 change according to the system considered. This means that the percentage loss of performance does not depend just on the percentage mistuning on ω_e and ξ_e , but also on the system considered. This is in contrast with what was evidenced previously for the enhanced resistive shunt. Indeed, in the case of RSP, all of the curves of Figure 8 are almost superimposed for attenuation levels over about 10 dB. This meant that for RSP shunt the percentage loss of performance depends just on the percentage mistuning and not on the system considered.

These aspects related to the robustness of the LR shunt can be clearly inferred also by looking at Figures 14 and 15, that show A_{dB}^{*LR} and $A_{dB}^{*LR} - A_{dB}^{LR}$ as a function of $\omega_e / \omega_e^{opt}$ while the electrical damping is kept at its optimal value (i.e. $\xi_e = \xi_e^{opt}$). The graphical comparison of Figures 14 and 15 to Figures 7 and 8 clearly shows the poor robustness of the LR shunt as compared with the R shunt (or RSP shunt).

RSP and LR shunt robustness comparison

In this section, the robustness of the two shunt impedances, RSP and LR, when changes in the EMS occur, is addressed.

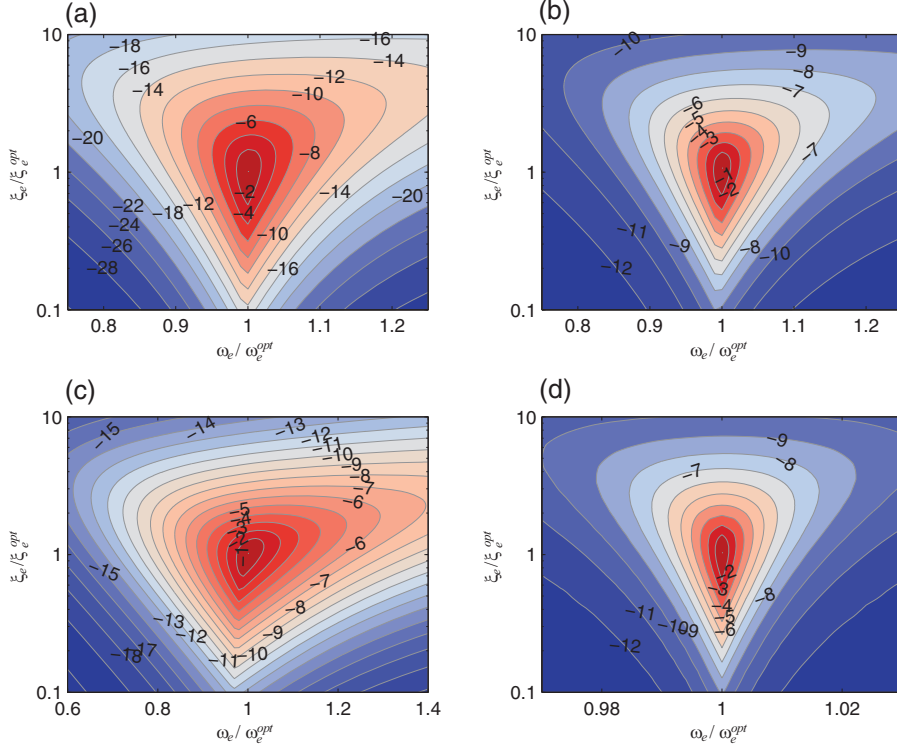


Figure 13. Trend of $A_{dB}^{*LR} - A_{dB}^{LR}$ provided by LR shunt in the presence of mistuning on the electrical parameters: (a) $(k_r, \xi_i) = (0.1, 10^{-3})$; (b) $(k_r, \xi_i) = (0.1, 10^{-2})$; (c) $(k_r, \xi_i) = (0.3, 10^{-2})$; (d) $(k_r, \xi_i) = (0.01, 10^{-3})$.

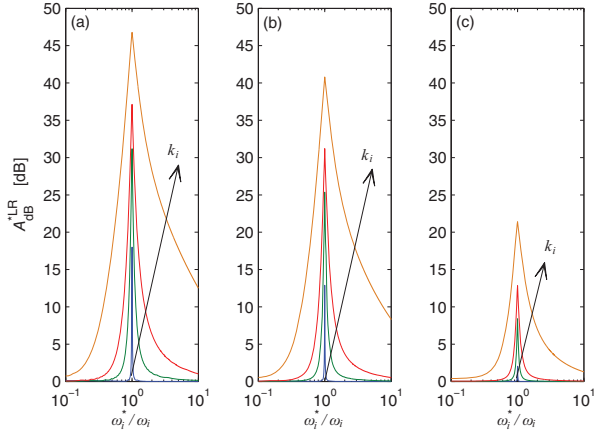


Figure 14. Trend of A_{dB}^{LR} as a function of ω_i^*/ω_i for different values of k_i (i.e. 0.01, 0.05, 0.1, 0.3) for: $\xi_i = 5 \times 10^{-4}$ (a), $\xi_i = 10^{-3}$ (b), $\xi_i = 10^{-2}$ (c).

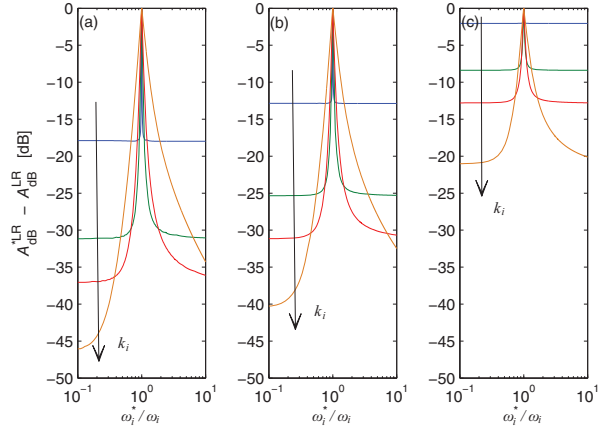


Figure 15. Trend of $A_{dB}^{*LR} - A_{dB}^{LR}$ as a function of ω_i^*/ω_i for different values of k_i (i.e. 0.01, 0.05, 0.1, 0.3) for: $\xi_i = 5 \times 10^{-4}$ (a), $\xi_i = 10^{-3}$ (b), $\xi_i = 10^{-2}$ (c).

The robustness of the shunt methods is here analysed by supposing to start from perfectly tuned situations and then to experience a shift of the system eigenfrequency ω_i (e.g. due to a thermal shift). The shifted value of ω_i is defined here as ω_i^* , as done previously when considering the robustness of the RSP and LR shunts. This natural frequency detuning affects the shunts tuning through τ_e for the RSP shunt ($\omega_i^*/\omega_i = \tau_e/\tau_e^{opt}$) and ω_e for the LR shunt ($\omega_i/\omega_i^* = \omega_e/\omega_e^{opt}$), while it does

not affect the electrical damping ξ_e of the LR shunt. Then, the difference $\Delta^* = A_{dB}^{*RSP} - A_{dB}^{LR}$ (where A_{dB}^{*RSP} is the attenuation in decibels in mistuned conditions for the RSP and it is calculated numerically by means of Equation (12)) has been computed for different values of k_i and ω_i^*/ω_i , and taking into account three different values of ξ_i . This analysis has been repeated considering several values of the coupling factor enhancement $G = \tilde{k}_i/k_i$.

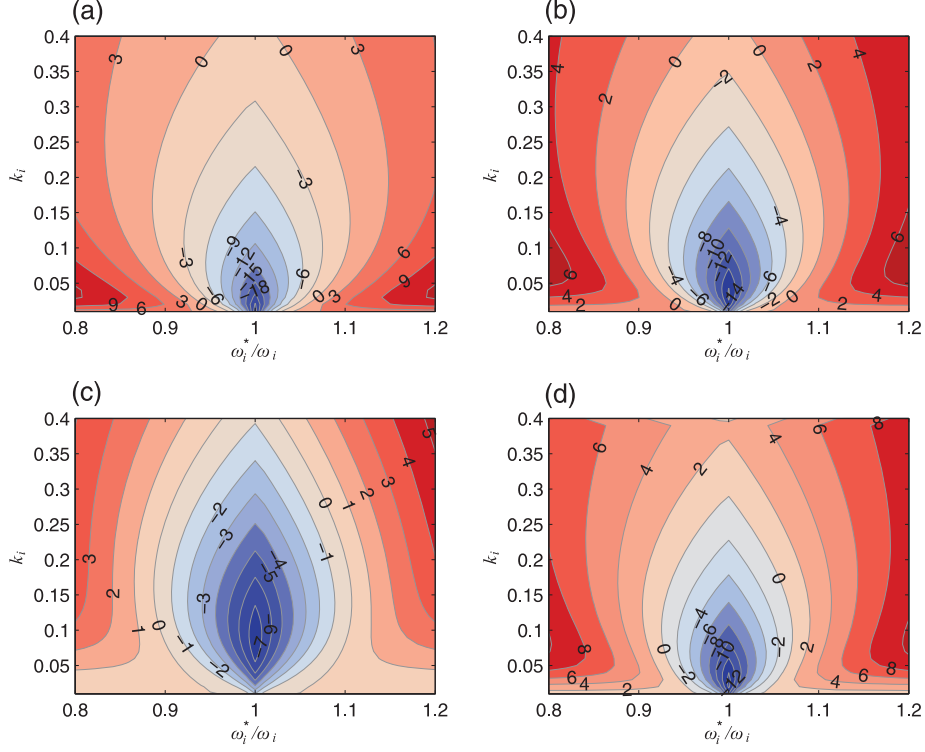


Figure 16. Trend of Δ^* as a function of k_i and ω_i^*/ω_i for different values of ξ_i with: $G = 2.38$ and $\xi_i = 10^{-4}$ (a), $G = 2.38$ and $\xi_i = 10^{-3}$ (b), $G = 2.38$ and $\xi_i = 10^{-2}$ (c), $G = 3.00$ and $\xi_i = 10^{-3}$ (d).

Figure 16(a)–(c) show the case where $\beta_{sp1} = \beta_{sp2} = 0.7$, which in turn leads to a coupling factor enhancement G equal to 2.38. These maps highlight that the performance of the RSP shunt becomes more and more competitive as soon as the value of k_i is increased and the mistuning increases (i.e. values of ω_i^*/ω_i farther and farther from 1). Furthermore, if we increase the value of G (compare Figures 16(c) and (d)), the area in which the RSP provides higher attenuation than the LR shunt (i.e. positive values of Δ^*) increases as well.

This analysis showed that the RSP shunt is much more robust to biases and uncertainty than the pure resonant shunt. Therefore, the use of a resistive shunt coupled to a SP NC configuration is able to improve a lot the performances of simple resistive shunt, thus making it competitive with the LR shunt, keeping at the same time its high robustness.

RSP and LR shunt comparison for broadband damping action

In this section, the broadband control capability of the two circuits (RSP and LR) is analysed. Both R and LR shunts are well-known techniques for single mode control. Nevertheless, it can be deduced from the mechanical analogy with a damper (Preumont, 2011) that the R shunt is characterized by a wideband control action if

compared with the resonant shunt. Indeed, the use of resistive shunt enables to have a significant control action even on the other modes of the EMS, while the resonant shunt works almost on the targeted mode. This can be easily demonstrated by taking into account the following case, as an example. Consider two modes of the same EMS, one at ω_1 and the other at ω_2 with $k_1 = k_2$. The value of τ_e , ω_e and ξ_e are chosen to optimize the attenuation on mode 1 (see Equation (13) for the RSP and Equations (23) for the LR). Then, we compute $\Delta_2 = A_{dB2}^{RSP} - A_{dB2}^{LR}$, where A_{dB2}^{RSP} and A_{dB2}^{LR} are the attenuations on the second mode, in decibels, for the RSP and LR shunt respectively and they are calculated numerically by means of Equations (12) and (24).

Figure 17 shows the attenuation difference on mode 2, i.e. Δ_2 , as function of the ratio ω_2/ω_1 , for different values of G (Figure 17(a)), k_i (Figure 17(b)) and ξ_i (Figure 17(c) and (d)). It is evident that the broadband action provided by the RSP shunt is much higher than that provided by the resonant shunt because its attenuation on mode 2 is much higher even for values of ω_2/ω_1 very low (i.e. close to 0.1) or very high (i.e. close to 10). The RSP shunt has thus shown to be a competitive alternative to the well-established LR shunt thanks to its higher robustness and its capability to damp many modes at the same time. Furthermore, the enhanced value of the MEMCF allows the RSP shunt to achieve maximum attenuations close (or higher) than the resonant shunt.

Table 3. Modal data of the experimental set-up.

Mode	$\omega_i/(2\pi)$ [Hz]	ξ_i	k_i
1	39.72	0.0045	0.2716
2	187.34	0.0030	0.1037
3	509.00	0.0027	0.0710
4	986.42	0.0028	0.1222

Experiments

Experimental set-up

The RSP shunt has been tested experimentally to show its reliability and its capability to improve the attenuation performance, if compared with the resistive shunt coupled to the traditional NC in series and parallel configurations, and to validate the theoretical results shown so far. As for the comparison between the RSP and LR shunt, here no tests with the resonant shunt are shown because the related model has been already experimentally validated in Thomas et al. (2012) and its robustness tested in Berardengo et al. (2015a).

The experimental test set-up was a stainless steel cantilever beam (length of 178.8 mm, width of 30.5 mm and thickness of 1.1 mm) with two PIC 151 piezoelectric patches (with a length of 70 mm each, 0.5 mm of thickness and wrapped electrodes) bonded at the clamped end and electrically connected in series. The modes considered for the experimental activity were the first four bending modes, whose characteristics are given in Table 3 (the shapes of these modes are the usual ones for cantilever beams). Particularly, the values of ω_i and ξ_i were estimated by means of experimental modal analysis, as well as the mode shapes, and the values of k_i were estimated by deriving the ω_i and $\dot{\omega}_i$ values from the measured FRFs of the EMS in SC and OC and using Equation (10).

The value of the capacitance of the piezoelectric patch was measured at a number of frequency values between the first and the fifth mode of the structure with a digital multimeter. The obtained values of C_{pi} were close each other: between 31.1 and 30.0 nF. Since these values are very close each other, we decided to use a sort of average value for all of the modes: $C_{pi} \simeq C_p = 30.5\text{nF}$ for each of them ($i = 1, 2, 3, 4$), denoted by C_p in the following. Here C_0 was estimated by measuring with the digital multimeter the value of C_{p1} at 100 Hz and then calculating $C_0 = C_{p1}(1 + k_1^2)$ (see Berardengo et al., 2016). The result for C_0 was about 33.26 nF. Here C_∞ was estimated measuring the capacitance of the piezoelectric patch at 100 kHz and the result was about 25.9 nF.

The cantilever beam was excited by a contactless electromagnetic actuator, described in Thomas et al. (2003), composed by a fixed coil and a magnet bonded on the beam, close to its tip. The reference signal for

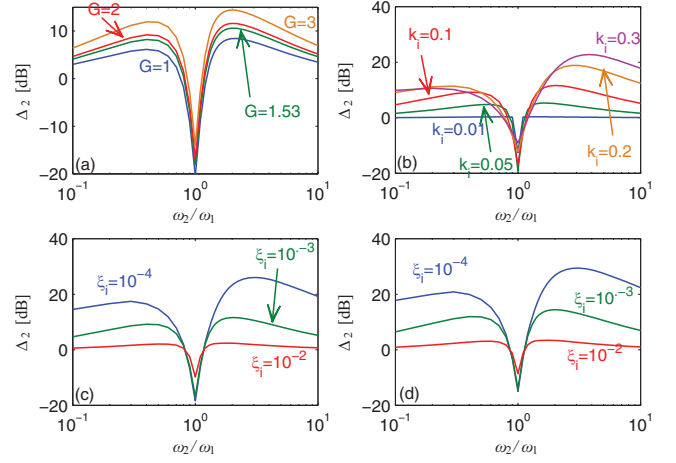


Figure 17. Trend of Δ_2 as a function of ω_2/ω_1 for different values of G with $k_i = 0.1$ and $\xi_i = 10^{-3}$ (a), for different values of k_i with $G = 2$ and $\xi_i = 10^{-3}$ (b), for different values of ξ_i for $k_i = 0.1$ and $G = 2$ (c), for different values of ξ_i for $k_i = 0.1$ and $G = 3$ (d).

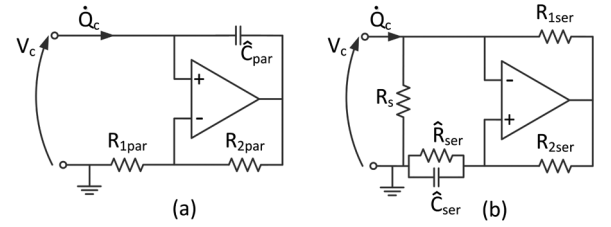


Figure 18. Negative capacitance practical layout using operational amplifiers: parallel NC (a) and series NC (b).

the FRF computation was the intensity of the current which flowed in the coil, measured by a current clamp (Tektronix A622), assumed proportional to the electromagnetic force imposed on the magnet. A Brüel & Kjaer 2712 power amplifier was used to feed the coil. The response of the beam was measured by a laser Doppler velocimeter (Polytec PSV 400). The NCs were built as proposed in Figures 18 and 19 using Texas Instruments OPA445 operational amplifiers (TexasInstruments, 2010), with some of the resistances built using potentiometers for easy tuning.

It should be noted that the NCs in parallel can be considered as pure NCs:

$$-C_1 = -\frac{R_{2par}\hat{C}_{par}}{R_{1par}} \quad (27)$$

Conversely, the NCs in series cannot be considered as pure NCs because of the presence of the resistance \hat{R}_{ser} . This latter component must be added in parallel to the capacitance \hat{C}_{ser} to form together with \hat{C}_{ser} an undesired but necessary high-pass filter used to solve practical problems such as bias-current- and offset-voltage-induced errors (Moheimani and Fleming, 2006).

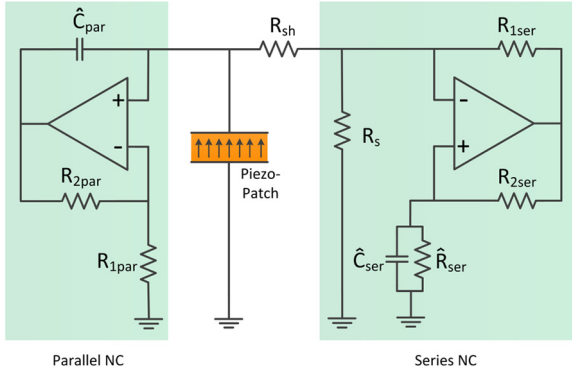


Figure 19. Scheme of the electric shunt for the SP configuration, using two operational amplifiers.

Therefore, the circuit of Figure 18(b) and the series part of Figure 19 composed by \hat{R}_{ser} , \hat{C}_{ser} , R_{1ser} and R_{2ser} can be seen as the parallel of a NC and a negative resistance $-\tilde{R}$:

$$-C_2 = -\frac{R_{2ser}\hat{C}_{ser}}{R_{1ser}}, \quad -\tilde{R} = -\frac{R_{1ser}\hat{R}_{ser}}{R_{2ser}} \quad (28)$$

In order to limit the effect on the circuit behaviour of this negative resistance $-\tilde{R}$ in parallel to the NC, a further resistance R_s is added in the circuits of the NCs in series. This further element is indeed used to compensate for the effects of the negative resistance $-\tilde{R}$, almost cancelling its effects. Indeed, the global resistance R_{eq} given by the parallel between R_s and $-\tilde{R}$ is:

$$R_{eq} = \frac{-\tilde{R}R_s}{R_s - \tilde{R}} \quad (29)$$

If the value of R_s is chosen so that the value of R_{eq} is negative and as high as possible in terms of absolute value, the impedance made up by R_s , $-\tilde{R}$ and $-C_2$ approximates a pure NC. More details about the use of R_s for NCs in series can be found in Berardengo et al. (2016); the same referenced paper also gives details about the possible use of a resistance in parallel to \hat{C}_{par} for NCs in parallel configuration (see Figure 18(a)).

Many tests were carried out to show the benefits provided by the RSP if compared with the series and parallel resistive shunt. Two of them are discussed in the following.

Tests

Here two different tests are taken into account. The first, denoted as Test1, is related to a case in which $\beta_1 = \beta_{sp1} = 0.65$ and $\beta_2 = \beta_{sp2} = 0.82$ were used. The second test considered here, named Test2, has instead the following configuration: $\beta_1 = \beta_{sp1} = 0.65$ and $\beta_2 = \beta_{sp2} = 0.61$. In both tests, NCs in parallel, series and SP configurations, coupled to a resistive shunt,

Table 4. Values of the electric components used in Test1 and Test2.

	Test1	Test2
C_1 [nF]	19.82	19.82
C_2 [nF]	37.21 (series), 17.39 (SP)	50.00 (series), 30.18 (SP)
R_s [M Ω]	2.87	2.87
R_{1par} [k Ω]	4.64	4.64
R_{2par} [k Ω]	4.64	4.64
R_{1ser} [k Ω]	7.24 (series), 15.18 (SP)	5.48 (series), 9.06 (SP)
R_{2ser} [k Ω]	4.64	4.64
\hat{C}_{par} [nF]	19.82	19.82
\hat{C}_{ser} [nF]	58.05 (series), 58.93 (SP)	59.05 (series), 51.81 (SP)
\hat{R}_{ser} [M Ω]	1.79 (series), 0.86 (SP)	2.37 (series), 1.43 (SP)

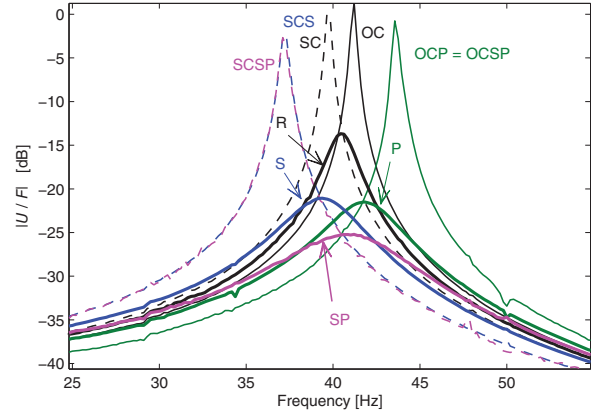


Figure 20. Experimental FRFs (displacement U to force F ratio) for Test2 using the optimal value of τ_e for the first mode: zoom on mode I. Letter S indicates the FRF in series with the optimal value of τ_e , P the optimal parallel, SP the optimal series + parallel. SCSP indicates the short-circuit FRF for the SP, SCS the short-circuit FRF for the series, OCP the open-circuit FRF for the parallel and OCSP the open-circuit FRF for the SP. R indicates the optimal resistive shunt without NCs.

have been investigated; in addition, we tested also the pure resistive shunt without NCs. The τ_e values have been fixed equal to τ_e^{opt} of the first and fourth modes for both the tests and all the three NC configurations. The values of the electric components for the tests are gathered in Table 4. It is remarked that the β values of Test1 were chosen in order to provide the best attenuation value and at the same time a reliable functioning of the electrical impedance.

Figure 20 shows the FRFs (zoomed on the first mode) with the value of τ_e optimized for the damping of the first mode for each NC configuration for Test2. Figure 21 shows the FRFs (zoomed on the third mode) with the value of τ_e optimized for the damping of the

Table 5. Comparison between experimental and theoretical attenuations for Test I.

		Attenuation [dB] Experimental - Numerical			
		Mode 1	Mode 2	Mode 3	Mode 4
Tuning on mode 1	Parallel	21.8 - 22.1	6.2 - 8.1	2.0 - 1.8	2.2 - 2.3
	Series	27.1 - 27.0	8.9 - 8.4	2.6 - 2.6	3.4 - 3.3
	SP	29.3 - 29.6	11.6 - 10.2	3.6 - 3.5	4.4 - 4.4
Tuning on mode 4	Parallel	5.5 - 5.5	5.3 - 5.5	6.4 - 6.4	13.4 - 13.7
	Series	10.3 - 7.3	5.1 - 8.3	9.8 - 9.6	16.3 - 18.1
	SP	12.1 - 9.1	7.2 - 9.9	11.7 - 11.4	19.3 - 20.4

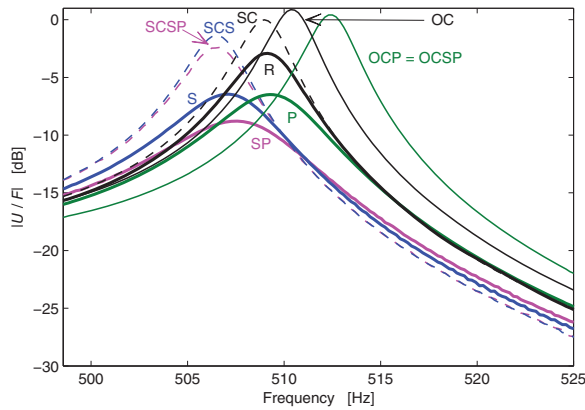


Figure 21. Experimental FRFs (displacement U to force F ratio) for Test2 using the optimal value of τ_e for the fourth mode: zoom on mode 3. Letter S indicates the FRF in series with the optimal value of τ_e , P the optimal parallel, SP the optimal series + parallel. SCS indicates the short-circuit FRF for the SP, SCS the short-circuit FRF for the series, OCP the open-circuit FRF for the parallel and OCSP the open-circuit FRF for the SP. R indicates the optimal resistive shunt without NCs.

fourth mode for each NC configuration for Test2. In both cases, the increased attenuation provided by the SP is evident, as well as its capability to shift both the SC and OC eigenfrequencies (as already explained in the paper). It is remarked that the SP layout improves the attenuation both in tuned (Figure 20) and mistuned (Figure 21) conditions. Moreover, Figure 21 highlights also the broadband control capability of the resistive shunt, which is further enhanced by the use of RSP configuration.

Figures 22 and 23 show the comparison between numerical and experimental FRFs of Test1 for τ_e tuned on the first and fourth mode, respectively. These plots evidence that the analytical model used herein is able to accurately describe the experimental evidence.

Finally, Tables 5 and 6 summarize the attenuations on all of the four modes for all of the tests presented here, showing again the benefits provided by the SP. Indeed, the SP is able to increase the attenuation if compared with the series and parallel layouts both in tuned and mistuned conditions (for this latter case refer

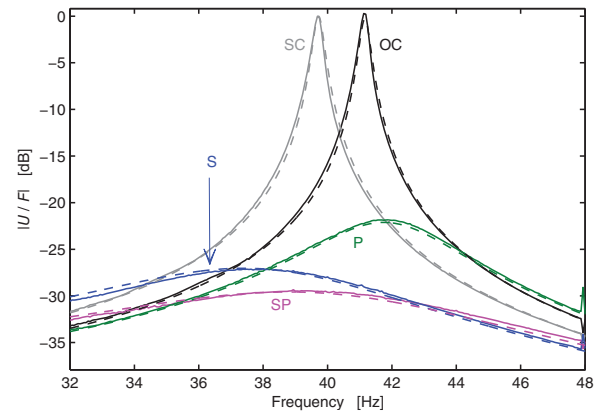


Figure 22. Comparison between the experimental (solid lines) and analytical (dashed lines) FRFs (displacement U to force F ratio) for Test I and τ_e tuned on the first mode around mode 1.

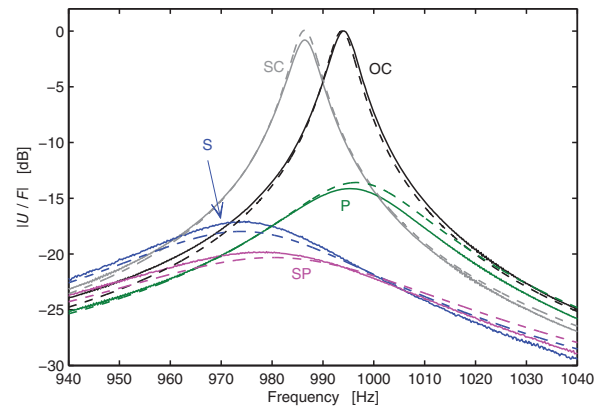


Figure 23. Comparison between the experimental (solid lines) and analytical (dashed lines) FRFs (displacement U to force F ratio) for Test I and τ_e tuned on the fourth mode around mode 4.

to the results achieved for the modes different from that on which the value of τ_e has been tuned). This is made possible by the increased values of G provided by the SP layout, which are gathered in Table 7. Furthermore, the RSP shunt is expected to be more robust than a LR shunt, providing on the first mode almost the same

Table 6. Comparison between experimental and theoretical attenuations for Test2.

		Attenuation [dB] Experimental - Numerical			
		Mode 1	Mode 2	Mode 3	Mode 4
Tuning on mode 1	Parallel	21.5 - 22.1	8.0 - 8.1	1.4 - 1.8	2.5 - 2.3
	Series	2.1 - 2.3	6.2 - 5.7	1.6 - 1.5	2.3 - 2.1
	SP	25.2 - 25.7	9.7 - 8.4	2.3 - 2.5	4.0 - 3.5
Tuning on mode 4	Parallel	5.6 - 5.5	5.3 - 5.5	6.5 - 6.4	13.4 - 13.7
	Series	6.4 - 4.9	4.1 - 5.2	6.4 - 5.9	12.1 - 12.9
	SP	8.6 - 7.3	6.2 - 7.7	8.8 - 8.5	16.1 - 16.8

Table 7. The G values for Test1 and Test2 for the parallel, series and SP layouts.

	Value of G		
	Parallel	Series	SP
Test1	1.69	2.35	2.72
Test2	1.69	1.60	2.10

attenuation in tuned conditions (see Figure 10(c)) for Test2 configuration, and even higher for Test1.

Conclusion

This paper has dealt with the use of a new layout for NCs shunted to piezoelectric actuators for vibration damping. This configuration relies on the use of two NCs, one connected in parallel and the other connected in series to the piezoelectric actuator. This layout (named SP), when coupled to a resistive shunt, is able to increase the attenuation performance provided by the traditional layouts (i.e. a single NC in either parallel or series). The paper has addressed all of the advantages provided by this new layout coupled to resistive shunt (called RSP shunt). Indeed, in the first part of the paper, it has been shown that the SP layout enables us to increase the stability margin for a given performance level, thus improving the reliability of the system. It is also shown quantitatively that the loss of performance of the shunt due to a mistuning (a change in the shunt parameters or in the structural characteristics of the host structure) is decreased with this new SP layout, thus proving the associated increase of robustness. In the second part, the RSP shunt performances are systematically compared with those of the traditional resonant shunt. It has been shown that the RSP shunt can bring to equivalent performances in term of vibration level attenuation than a resonant shunt, even for lightly damped host structures ($\xi_i < 5 \times 10^{-3}$) and standard modal electromechanical coupling factors ($k_i < 0.2$). At the same time, increased robustness to a detuning and broadband action have been demonstrated, as

compared with the traditional resonant shunt, thus proving that the new RSP shunt is promising.

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References

- Beck BS, Cunefare KA and Collet M (2013) The power output and efficiency of a negative capacitance shunt for vibration control of a flexural system. *Smart Materials and Structures* 22(6): 065009.
- Beck BS, Cunefare KA and Collet M (2014) Response-based tuning of a negative capacitance shunt for vibration control. *Journal of Intelligent Material Systems and Structures* 25(13): 1585–1595.
- Behrens S, Fleming AJ and Moheimani SOR (2003) A broadband controller for shunt piezoelectric damping of structural vibration. *Smart Materials and Structures* 12(1): 18–28.
- Berardengo M, Cigada A, Manzoni S and Vanali M (2015a) Vibration control by means of piezoelectric actuators shunted with LR impedances: Performance and robustness analysis. *Shock and Vibration* 2015: 704265.
- Berardengo M, Manzoni S, Thomas O and Giraud-Audine C (2015b) A new electrical circuit with negative capacitances to enhance resistive shunt damping. In: *Proceedings of the ASME 2015 Conference on Smart Materials, Adaptive Structures and Intelligent Systems (SMASIS 2015)*, Colorado Springs, CO, 21–23 September 2015.
- Berardengo M, Thomas O, Giraud-Audine C and Manzoni S (2016) Improved resistive shunt by means of negative

-
- capacitance: new circuit, performances and multi mode-control. *Smart Materials and Structures* 25: 075033.
- Burns R (2001) *Advanced control engineering*. London: Butterworth-Heinemann.
- Collet M, Ouisse M, Cunefare K, Ruzzene M, Beck B, Airoidi L and Casadei F (2011) Vibroacoustic energy diffusion optimisation in beams and plates by means of distributed shunted piezoelectric patches. In: Vasques C and Rodrigues JD (eds.) *Vibration and structural acoustics analysis: current research and related technologies*. Dordrecht: Springer, pp. 265–302.
- Date M, Kutani M and Sakai S (2000) Electrically controlled elasticity utilizing piezoelectric coupling. *Journal of Applied Physics* 87(2): 863–868.
- de Marneffe B and Preumont A (2008) Vibration damping with negative capacitance shunts: theory and experiment. *Smart Materials And Structures* 17(3): 035015.
- Ducarne J, Thomas O and Deü J (2012) Placement and dimension optimization of shunted piezoelectric patches for vibration reduction. *Journal of Sound and Vibration* 331(14): 3286–3303.
- Gopal M (2002) *Control Systems: Principles and Design*, 2nd edn. Tata McGraw-Hill Education.
- Hagood N and von Flotow A (1991) Damping of structural vibrations with piezoelectric materials and passive electrical networks. *Journal of Sound and Vibration* 146: 243–268.
- Heuss O, Solloum R, Mayer D and Melz T (2014) Tuning of a vibration absorber with shunted piezoelectric transducers. *Archive of Applied Mechanics*. DOI: 10.1007/s00419-014-0972-5.
- Horowitz P and Hill W (1989) *The art of electronics*, 2nd edn. Cambridge: Cambridge University Press.
- Kodejška M, Mokřý P, Linhart V, Václavík J and Sluka T (2012) Adaptive vibration suppression system: An iterative control law for a piezoelectric actuator shunted by a negative capacitor. *IEEE Transactions on Ultrasonics, Ferroelectrics, and Frequency Control* 59(12): 2785–2796.
- Manzoni S, Moschini S, Redaelli M and Vanali M (2012) Vibration attenuation by means of piezoelectric transducer shunted to synthetic negative capacitance. *Journal of Sound and Vibration* 331(21): 4644–4657.
- Moheimani S and Fleming A (2006) *Piezoelectric Transducers for Vibration Control and Damping*. Berlin: Springer-Verlag.
- Park CH and Baz A (2005) Vibration control of beams with negative capacitive shunting of interdigital electrode piezoceramics. *Journal of Vibration and Control* 11(3): 331–346.
- Preumont A (2011) *Vibration Control of Active Structures*, 3rd edn. New York: Springer.
- TexasInstruments (2010) OPA445, High Voltage FET-Input Operational Amplifier. Available at: <http://www.ti.com/product/opa445>.
- Thomas O, Deü JF and Ducarne J (2009) Vibration of an elastic structure with shunted piezoelectric patches: efficient finite-element formulation and electromechanical coupling coefficients. *International Journal of Numerical Methods in Engineering* 80(2): 235–268.
- Thomas O, Ducarne J and Deü J (2012) Performance of piezoelectric shunts for vibration reduction. *Smart Materials and Structures* 21(1): 015008.
- Thomas O, Touzé C and Chaigne A (2003) Asymmetric nonlinear forced vibrations of free-edge circular plates. Part II: experiments. *Journal of Sound and Vibration* 265(5): 1075–1101.
- Yamada K, Matsuhisa H, Utsuno H and Sawada K (2010) Optimum tuning of series and parallel LR circuits for passive vibration suppression using piezoelectric elements. *Journal of Sound and Vibration* 329(24): 5036–5057.