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A proposed set of popular limit-point buckling benchmark problems

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Abstract. Developers of new finite elements or nonlinear solution techniques rely on discriminative benchmark tests drawn from the literature to assess the advantages and drawbacks of new formulations. Buckling benchmark tests provide a rigorous evaluation of finite elements applied to thin structures, and a complete and detailed set of reference results would therefore prove very useful in carrying out such evaluations. Results are usually presented in the form of load-deflection curves that developers must reconstruct by extracting the points, a procedure which is often tedious and inaccurate. Moreover the curves are usually given without accompanying information such as the calculation time or number of iterations it took for the model to converge, even though this type of data is equally important in practice. This paper presents ten different limit-point buckling benchmark tests, and provides for each one the reference load-deflection curve, all the points necessary to recreate the curve in tabulated form, analysis data such as calculation time, number of iterations and increments, and all of the inputs used to obtain these results.

Keywords: finite element; nonlinear analysis; limit-point buckling benchmarks; post-buckling; path-following strategy; large rotations.

1. Introduction

For the past two decades, many finite element programs have been developed with the aim of simulating, as efficiently and as accurately as possible, various kinds of mechanical and coupled problems. These in-house or commercial software packages usually incorporate different libraries of finite elements and make use of diverse nonlinear solution techniques. There is a widely recognized need for testing and comparing the above-mentioned formulations and strategies. The performance of newly developed finite elements is commonly assessed based on a variety of test problems, ranging from linear analyses to geometric as well as material nonlinear benchmarks. A carefully designed set of standard linear test problems was proposed for such evaluations by MacNeal and Harder (1985). These benchmarks have proven to be very useful and have been used extensively to decide whether a proposed formulation is free from the most important weaknesses that affect accuracy and efficiency; namely spurious mechanisms (also known as rank deficiencies) and locking phenomena. Subsequent publications (Hitchings *et al.* 1987, Prinja and Clegg 1993) by the

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UK's National Agency for Finite Element Methods and Standards (NAFEMS) confirmed that finite element validation has become a matter of primary concern. More recently, Sze *et al.* (2004) proposed a detailed set of popular benchmark problems, for the specific case of geometric nonlinear analysis of thin structures.

The purpose of the current work is to provide developers of new finite element models or new nonlinear solution methods the numerical reference solutions for the most commonly used limit-point buckling benchmark tests. The plots and tables provided in this article are the converged mesh solutions, obtained by the careful analysis of several accurate and reliable shell elements. This information may therefore be used with confidence as a reference for the aforementioned benchmark tests. This implies that the given curves are the ABAQUS state of the art in terms of limit-point buckling simulations. No experimental results are presented in this article. Finally, for each test, two curves are given; the converged mesh and the mesh refined by a factor of two in the relevant directions when compared to the converged mesh. This is done in order to show that the converged mesh density is sufficient. Eight out of the ten benchmark tests have already been studied in the literature, and two of them are new. These new proposed benchmark tests deal with elastic-plastic limit-point buckling.

Since most authors provide results in terms of load-displacement curves, the interested developers and researchers have to extract the data points from these curves and then recreate them in order to be able to test their new finite element models or nonlinear solution methods. This is not only a tedious task, but more importantly, it is often an inaccurate one. Therefore, one of the goals of this article will be to eliminate this intermediate step by providing the results in tabulated form, together with the load-deflection curves. The points provided in the tables are all of the points needed to recreate the original curve.

The load-displacement results by themselves do not suffice when comparing new finite element models or nonlinear solution methods. The computing time, number of iterations, number of increments, and number of cutbacks are also needed in order to compare the speed and relative ease of convergence of the new versus the old techniques. Therefore this type of analysis data is provided in the article as well, which corresponds to the convergence criterion taken equal to its default value (see the detailed documentation in ABAQUS (2007) and the discussion in Section 4.3). To put the calculation times into perspective, all the tests were run on a Dell Precision 380 personal computer with a 2.4 GHz Intel Xeon CPU and 2 GB of RAM. The nonlinear solution method used was a modified path-following Riks method, implemented in ABAQUS. The inputs for the modified Riks method are also reported so that the reader has all the information necessary to recreate the benchmark tests.

2. General comments on limit-point buckling

Typical thin structures are prone to instability phenomena that may occur prior to their conventional strength limit. Such structural instabilities are known as buckling, which in theory is characterized by a sudden deflection of a structure (usually thin) when subjected to compressive loads. Such failure modes occur when the compressive load reaches a critical value. In practice, this phenomenon involves significant changes in the shape of the structure with geometric nonlinear effects. Besides the well-known sensitivity of buckling to geometric imperfections, it is also known to be very sensitive to boundary conditions. It is also well-known that critical points are classified

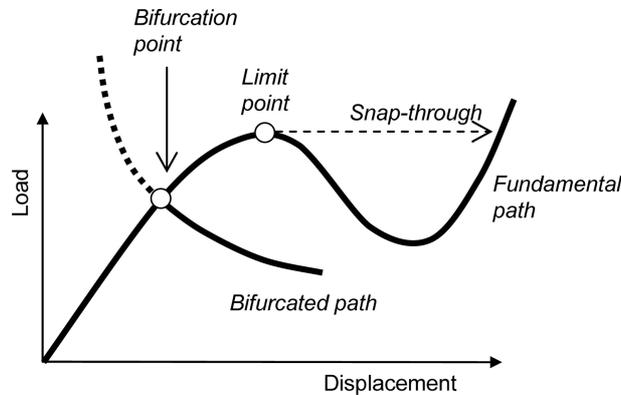


Fig. 1 Schematic representation of bifurcation-type buckling versus limit-point buckling

into limit points and bifurcation points. Over the last three decades, considerable effort has been devoted to the detection of such singular points and the associated post-buckling behavior. Various criteria and efficient algorithms have been developed to deal with this issue as demonstrated by the comprehensive literature in this field (see, for example, Koiter 1945, Timoshenko and Gere 1961, Hutchinson and Koiter 1970, Thompson and Hunt 1973, Budiansky 1974, Abed-Meraim 1999, Abed-Meraim and Nguyen 2007).

Limit-point buckling, also called snap-through buckling, is the type of buckling whereby there is a sudden large movement (jumping) in the direction of the loading, as opposed to bifurcation buckling, where the bifurcated branch intersects the fundamental path (branching), inducing significant changes in the shape of the structure (see Fig. 1). In this work, our attention is focused on limit-point buckling. As stated earlier, the modified path-following Riks method, which is the algorithm implemented in ABAQUS for solving this type of problem, is the method used to obtain the load-deflection curves. Before the benchmark tests are presented, it is important to understand how this algorithm works and how the different inputs affect the way the simulation is carried out. The discussion below is a brief, simplified introduction to the parameters important for the modified Riks algorithm, as implemented in ABAQUS (2007). For further information, the reader is invited

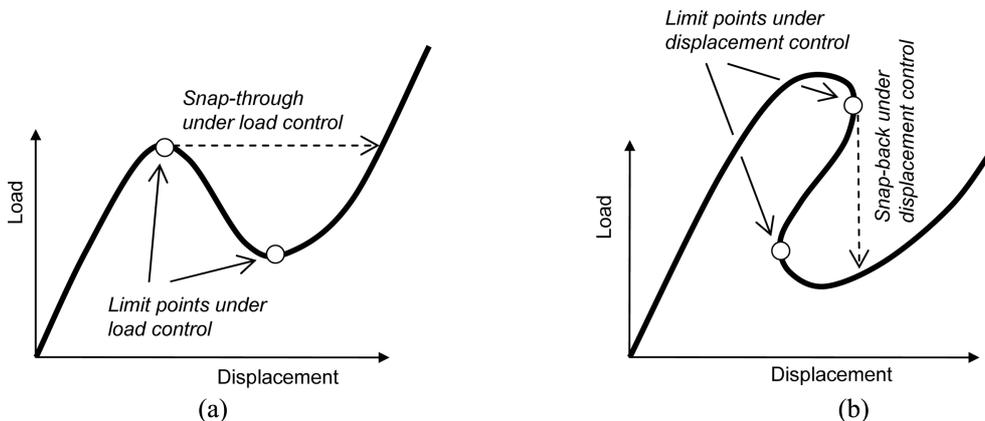


Fig. 2 (a) Typical load-displacement curve for snap-through, (b) typical load-displacement curve for snap-back

to consult the ABAQUS documentation and articles by Riks (1979), Crisfield (1981) and Ramm (1981).

In order to capture the complex load-displacement response, which can exhibit a decrease in load and/or displacement as the solution evolves (see Fig. 2), the equilibrium path is computed by including the load magnitude as an additional unknown in the formulation of the problem. The result of this is proportional loading, as all load magnitudes then vary with a single scalar parameter, called the load proportionality factor. For some of the benchmark cases, the results are given in terms of this load proportionality factor, which is given by ABAQUS as a history output. The method described here is also called an arc-length method because the equilibrium path in the new space, defined by the nodal variables and the loading parameter, is determined by using this so-called arc-length. The arc-length itself multiplies the load by a load factor, allowing both the load and the displacement to vary throughout the time step.

Due to the nature of this technique, the loading applied to the structure is only used as an indication of the direction of loading. The actual load applied in the first increment is the product of this load and the initial arc-length, which is one of the inputs of this procedure. If an increment converges easily, the arc-length in the subsequent increment will be increased by a factor of 1.5. In cases of snap-back, it is possible that by the time the snap-back region is reached, the arc-length is so large that the next point found is further along on the equilibrium path than this snap-back region. In this case, the algorithm will respond by erroneously skipping over this region. This hazard is avoided by limiting the maximum arc-length (whose default value is 10^{36}). It is often necessary to first run a model with the default value and then reduce it gradually to see how the resulting curve is affected. If a small maximum arc-length value is used from the beginning, it is possible that more points will be calculated on the equilibrium path than necessary to trace the curve, which could significantly increase the calculation time.

The number of increments, the number of iterations and the number of cutbacks are all indicators of the relative ease of convergence of a problem. The number of cutbacks is especially useful, as it shows how many times the size of the increment had to be reduced due to the inability of the solver to find a solution for the given increment size. This analysis data depends obviously on the tightness of the convergence criterion, the latter is left to its default value, specified in the ABAQUS documentation (2007), throughout the paper, unless explicitly specified otherwise (see Section 4.3 for more details).

The stopping criterion used is also different from other solution techniques. There are in fact three different ways for a simulation to come to completion. The analysis is terminated when it reaches either an imposed node displacement, an imposed load proportionality factor, or when the (predefined) maximum number of increments is reached. In certain cases, the end point of the load-displacement curve will surpass the imposed stopping criterion. This is because the arc-length for the last segment may be very large. ABAQUS will continue the analysis until the last point is equal to or greater than the stopping criterion, which is to say that ABAQUS will not adjust the final arc-length in order to exactly meet the stopping criterion. The final important point is that the ABAQUS keyword 'NLGEOM', which stands for "nonlinear geometry," must be used for all these analyses in order to take second order effects into account.

All of the previously discussed parameters were considered and optimized for these benchmark tests, in order to guarantee that the solutions obtained are the best ones possible and that the reader can use them with confidence.

3. Benchmark tests

Ten limit-point buckling benchmark tests, which cover a wide range of structures, boundary conditions, and loadings, are presented in this section. These include deep and shallow arches of various cross-sections, thin and thick cylindrical sections, beams, and frames. Hinged and clamped boundary conditions, as well as concentrated, pressure, and inclined loadings are investigated. Elastic-plastic behavior is also treated in the two new benchmark tests proposed at the end of this section. All of these benchmark problems exhibit some common features such as nonlinear pre-buckling and unstable buckling behavior.

As expected, shell elements were found to be the best suited for this type of application and, in most cases, the converged meshes for the three shell elements tested gave the same load-deflection curve. The results stated for each benchmark test are therefore those corresponding to the most efficient element, i.e., the fastest one. Evidently, the accuracy of the solution always prevails over the speed of the calculation. The obtained results were always compared with other literature results in order to understand which element performed the best. Whenever the final result was found different from the one given in the literature, careful investigations of accuracy and convergence were performed with more expensive high-order elements. An analytical solution is available for several cases, however, the reader must keep in mind that all analytical solutions make use of one or more simplifying assumptions. Since much care was taken to arrive at the best numerical solution, a mismatch with a given analytical solution is probably due to one of the assumptions used to derive the latter solution over-simplifying the problem. Another important point regarding numerical solutions drawn from the literature is the fact that the results might be an average of results computed by several different pieces of software, which could introduce deviations to the load-displacement curve.

The nomenclature given below is employed throughout this article. Furthermore, the important features of all the ABAQUS elements tested are given in Table 1.

<u>Nomenclature and naming conventions</u>			
u	Displacement	length (l)	Longest side of the structure
R	Radius	width (w)	Side perpendicular to the loading direction
P	Applied load	thickness (t)	Side parallel to the loading direction
E	Elasticity modulus		
ν	Poisson's ratio	The mesh naming convention is length×width(×thickness)	
I	Area moment of inertia		

3.1 Clamped shallow circular arch subjected to pressure loading

The geometry of this test is shown in Fig. 3. Since the arch, the loading, and the boundary conditions are symmetric, only half of the geometry is modeled. An analytical solution for this problem is given by Schreyer and Masur (1966), and numerical solutions were also developed, notably by Sharifi and Popov (1971). The ABAQUS manual (2007) gives the numerical solution

Table 1 Important features of the S4R, S4 and S4R5 shell elements, of the C3D8, C3D8I and C3D8R continuum elements, and the SC8R continuum-shell element

	S4R	S4	S4R5	
Number of nodes	4	4	4	
Integration points	$1 \times n^*$	$4 \times n^*$	$1 \times n^*$	
Degrees of freedom	6 (3 displacements, 3 rotations)	6 (3 displacements, 3 rotations)	5 (3 displacements, 2 rotations)	
Hourglass treatment	Default stabilization	Not applicable	Not applicable	
Applicable strain	Finite	Finite	Small	
Intended thickness	Thin/thick	Thin/thick	Thin only	
	C3D8	C3D8I	C3D8R	SC8R
Number of nodes	8	8	8	8
Integration points	8	8	1	$1 \times n^*$
Degrees of freedom	3 (displacements)	3 (displacements)	3 (displacements)	3 (displacements)
Hourglass treatment	Not applicable	Not applicable	Default stabilization	Default stabilization
Applicable strain	Finite	Finite	Finite	Finite
Intended thickness	Thin/thick	Thin/thick	Thin/thick	Thin/thick

*an arbitrary number (n) of integration points can be used through the thickness (the default value is five).

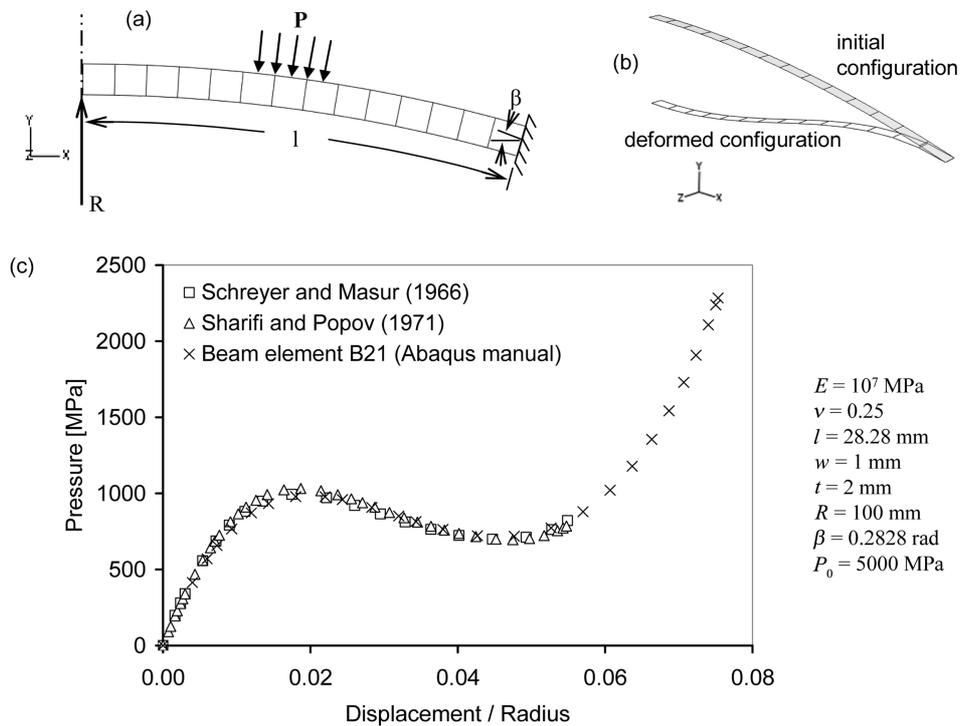


Fig. 3 Clamped shallow circular arch subjected to pressure loading, (a) geometric, material, and loading data, (b) initial and deformed configuration under maximum load, (c) solutions drawn from the literature and from the ABAQUS manual

Table 2 Riks analysis inputs for the clamped shallow circular arch subjected to pressure loading

Stopping criterion	Initial arc-length	Minimum arc-length	Maximum arc-length
Maximum load proportionality factor of 0.4	0.05	10^{-5}	0.1

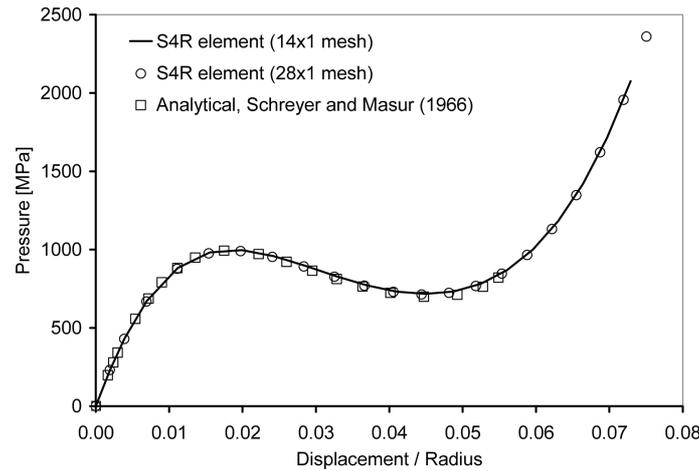


Fig. 4 Load-displacement curves for the clamped shallow circular arch subjected to a pressure load. The plotted displacement is the vertical displacement of the pole of the arch

Table 3 (a) Results for the clamped shallow circular arch subjected to pressure loading, (b) analysis data

(a)

$-u_y/R$	P [MPa]						
0.0000	0	0.0199	996	0.0449	717	0.0664	1418
0.0019	231	0.0243	958	0.0487	732	0.0697	1714
0.0039	431	0.0286	895	0.0525	781	0.0729	2075
0.0070	671	0.0329	828	0.0561	869		
0.0112	883	0.0370	771	0.0596	1001		
0.0155	982	0.0410	731	0.0630	1182		

(b)

Element	Mesh	CPU time [sec]	Number of increments	Number of iterations
S4R	14×1	1.24	20	53
S4R	28×1	1.52	21	53

obtained with beam elements. These solutions, given in terms of pressure versus normalized displacement (u/R), are shown in Fig. 3(c). This figure shows that the literature does not provide a complete picture of the post-buckling behavior. The results obtained with the ABAQUS linear beam element (B21) are very close to those given by Schreyer and Masur (1966), with the only slight differences occurring before buckling. Since this benchmark test deals with a 3D structure, one cannot assume that the correct results can be calculated using beam elements. Shell, continuum, and

continuum-shell ABAQUS elements were therefore tested to obtain the reference solution. The Riks analysis inputs used to set up the ABAQUS simulation are summarized in Table 2.

The results obtained using shell elements are very close to the analytical solution. Fig. 4 shows the plot of pressure versus normalized displacement of the arch apex. Table 3 shows tabulated results as well as analysis data such as calculation time for the S4R element, which was the fastest out of the three ABAQUS linear shell elements tested.

3.2 Clamped-hinged deep circular arch subjected to a concentrated load

The characteristics of this test are presented in Fig. 5. One end of the arch is hinged, and the other one is clamped. DaDeppo and Schmidt (1975) provide the analytical solution for this problem, and it is also considered in the ABAQUS manual (2007). The solution is given in terms of normalized force (PR^2/EI) versus normalized displacement (u/R), where ($I = wt^3/12$). The displacement is given

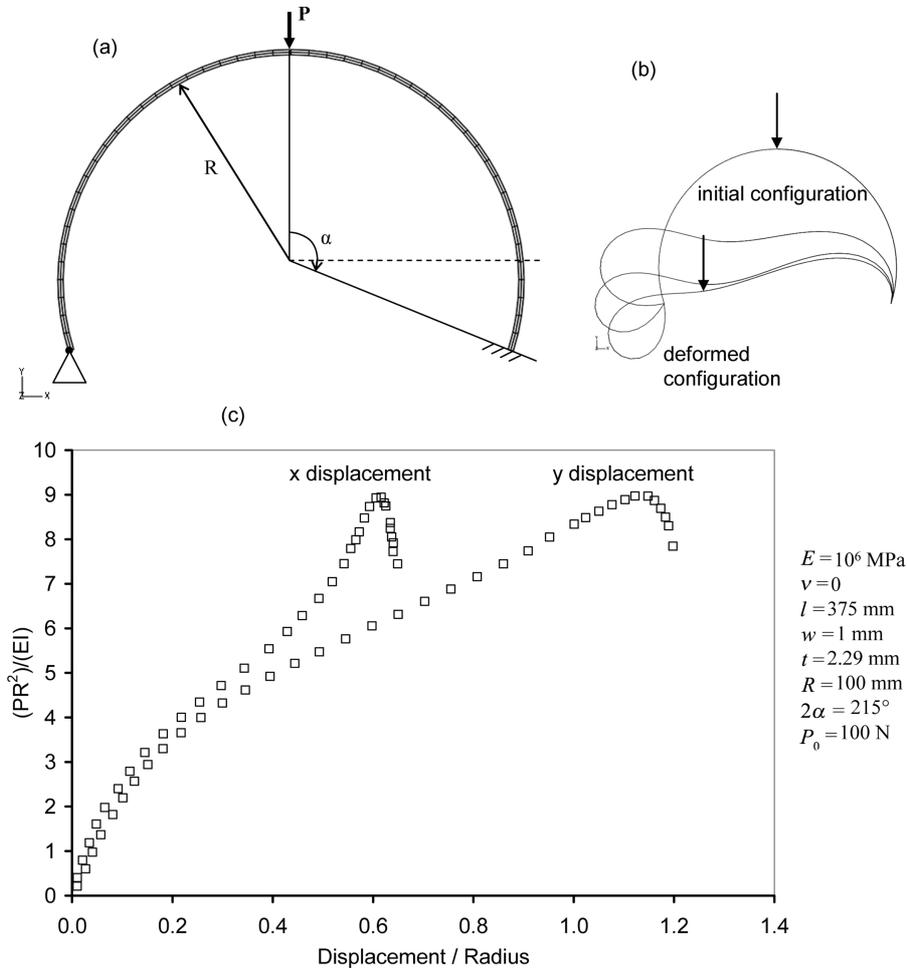


Fig. 5 (a) Geometric, material, and loading data for the clamped-hinged deep circular arch subjected to a concentrated load, (b) evolution of the structure shape and of the load location, (c) DaDeppo and Schmidt (1975) analytical solution

Table 4 Riks analysis inputs for the clamped-hinged deep circular arch subjected to a concentrated load

Stopping criterion	Initial arc-length	Minimum arc-length	Maximum arc-length
Maximum central point displacement of 120 mm in the negative y direction	0.5	10^{-5}	default value

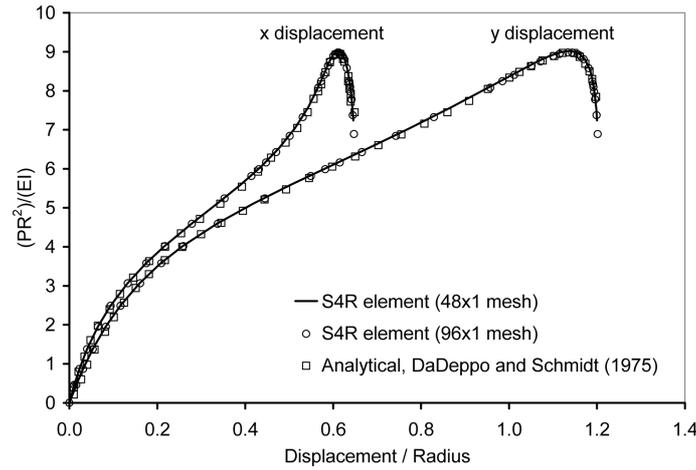


Fig. 6 Load-displacement curves for the clamped-hinged deep circular arch subjected to a concentrated load

Table 5 (a) Tabulated displacement and load results for the clamped-hinged deep circular arch subjected to a concentrated load, (b) analysis data

(a)

$-u_x/R$	$-u_y/R$	PR^2/EI	$-u_x/R$	$-u_y/R$	PR^2/EI	$-u_x/R$	$-u_y/R$	PR^2/EI
0.000	0.000	0.000	0.513	0.774	7.042	0.612	1.140	9.024
0.023	0.031	0.869	0.543	0.869	7.581	0.619	1.158	8.972
0.065	0.083	1.956	0.569	0.967	8.171	0.626	1.172	8.818
0.132	0.159	3.060	0.590	1.057	8.705	0.633	1.184	8.542
0.216	0.257	4.016	0.594	1.075	8.809	0.639	1.192	8.120
0.336	0.417	5.101	0.599	1.093	8.897	0.644	1.198	7.557
0.436	0.590	6.054	0.605	1.118	8.993	0.646	1.200	7.237

(b)

Element	Mesh	CPU time [sec]	Number of increments	Number of iterations	Number of cutbacks
S4R	48×1	3.99	33	168	3
S4R	96×1	6.56	36	195	7

for both the x and the y directions. Due to the asymmetry of the boundary conditions, the buckling will be asymmetric as well. Table 4 summarizes the Riks analysis inputs used for this test.

The results obtained with shell elements came closest to the analytical solution. Fig. 6 shows the plot of normalized load versus normalized displacement. Table 5 provides results in tabular form as

well as analysis data such as calculation time.

3.3 Hinged thin cylindrical section subjected to a central concentrated load

This is a very popular benchmark test that has been considered by multiple authors (Crisfield 1981, Ramm 1981, Cho *et al.* 1998, Eriksson *et al.* 1999, Kim and Kim 2001, 2002, Sze and Zheng 2002, Areias *et al.* 2003, Boutyour *et al.* 2004, Sze *et al.* 2004, Kim *et al.* 2005, Alves de Sousa *et al.* 2006, Wardle 2006, 2008). The geometry of this test is presented in Fig. 7, while Table 6 gives the basic simulation inputs for the path-following algorithm. The lateral, straight sides are hinged, while the two other curved sides are free. Only numerical results are available for this particular test, given in terms of load versus displacement at the middle point of the structure, where the load is applied. Fig. 7 also provides a plot of the results obtained by several authors. Notice that Eriksson *et al.* (1999) and Alves de Sousa *et al.* (2006) obtained slightly different solutions than the other authors. Despite the symmetry of the problem, the geometry was modeled in its entirety because some authors (Wardle 2006, 2008) noticed that this particular test could also exhibit a bifurcation

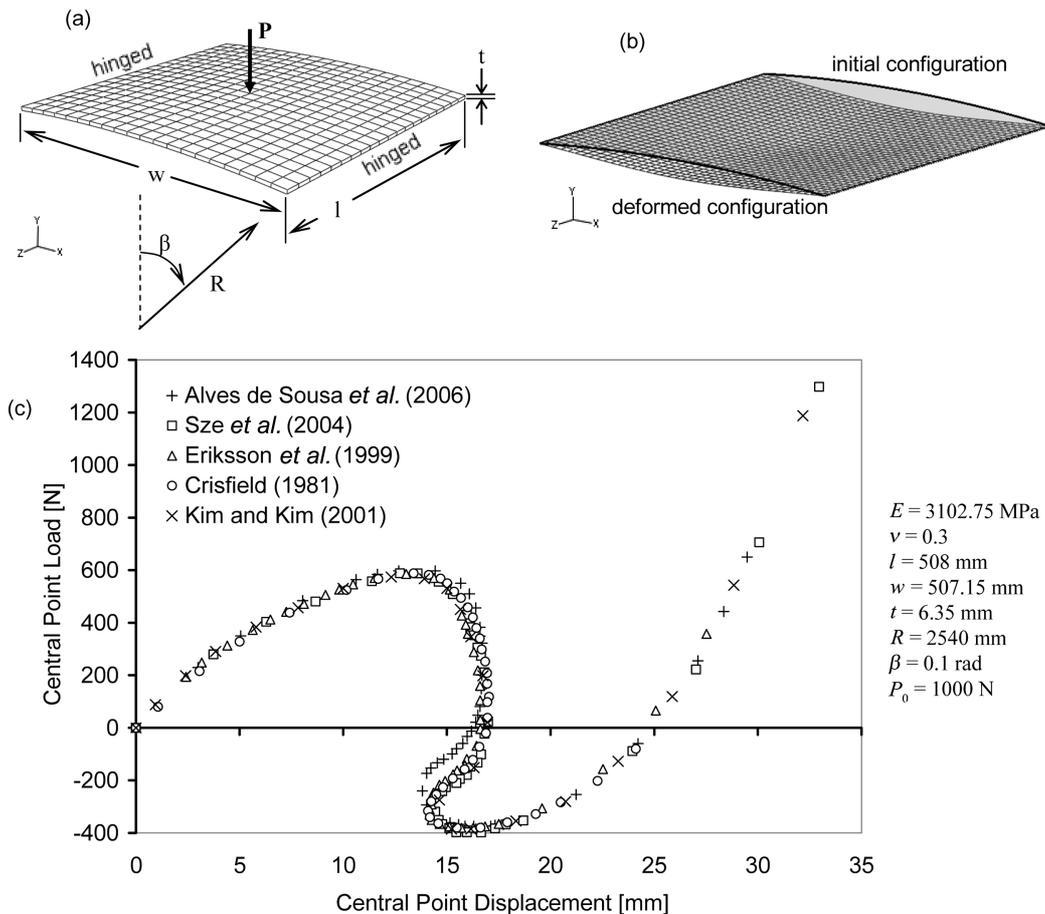


Fig. 7 Hinged thin cylindrical section subjected to a central concentrated load, (a) geometric and loading data, (b) deformed configuration under maximum load, (c) solutions drawn from the literature

Table 6 Riks analysis inputs for the hinged thin cylindrical section subjected to a central concentrated load

Stopping criterion	Initial arc-length	Minimum arc-length	Maximum arc-length
Maximum central point displacement of 30 mm in the negative y direction	0.1	10^{-5}	0.2

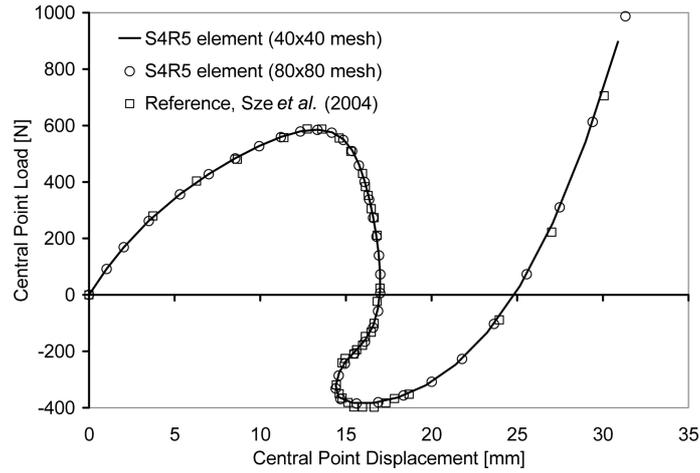


Fig. 8 Load-displacement curves for the hinged thin cylindrical section subjected to a central concentrated load

Table 7 (a) Displacement and load results for the hinged thin cylindrical section subjected to a central concentrated load, (b) analysis data

(a)

$-u_y$ [mm]	P [N]						
0.00	0	14.86	551	14.60	-276	21.40	-247
3.49	262	15.37	511	14.41	-322	25.15	31
8.54	485	16.36	342	14.57	-362	28.98	541
12.36	580	16.91	145	15.39	-383		
13.35	586	16.87	-49	16.60	-383		
14.19	576	15.55	-199	18.04	-363		

(b)

Element	Mesh	CPU time [sec]	Number of increments	Number of iterations
S4R5	40×40	46.3	39	114
S4R5	80×80	212.2	39	115

solution. This aspect will be further discussed in Section 4.

The three shell elements used here gave the same results, which were very close to those drawn from the literature. The S4R5 element had the fastest computation time. Fig. 8 shows the plot of load versus displacement, and Table 7 gives tabular results as well as relevant analysis data.

3.4 Hinged thick cylindrical section subjected to a central concentrated load

This test is the same as the previous one with the exception of the thickness, which is now twice as large ($t = 12.7$ mm). Several authors have examined this test (Klinkel and Wagner 1997, Sze and Zheng 2002, Legay and Combescure 2003, Sze *et al.* 2004, Kim *et al.* 2005). Only numerical results are available for this particular test, given in terms of load versus displacement at the middle point of the structure, where the load is applied. Fig. 9 and Table 8 give the important characteristics and input data used for this test.

Despite the symmetry of the problem, the entire geometry is again meshed according to the previous, similar-but-thin case. The results obtained with shell elements come closest to the

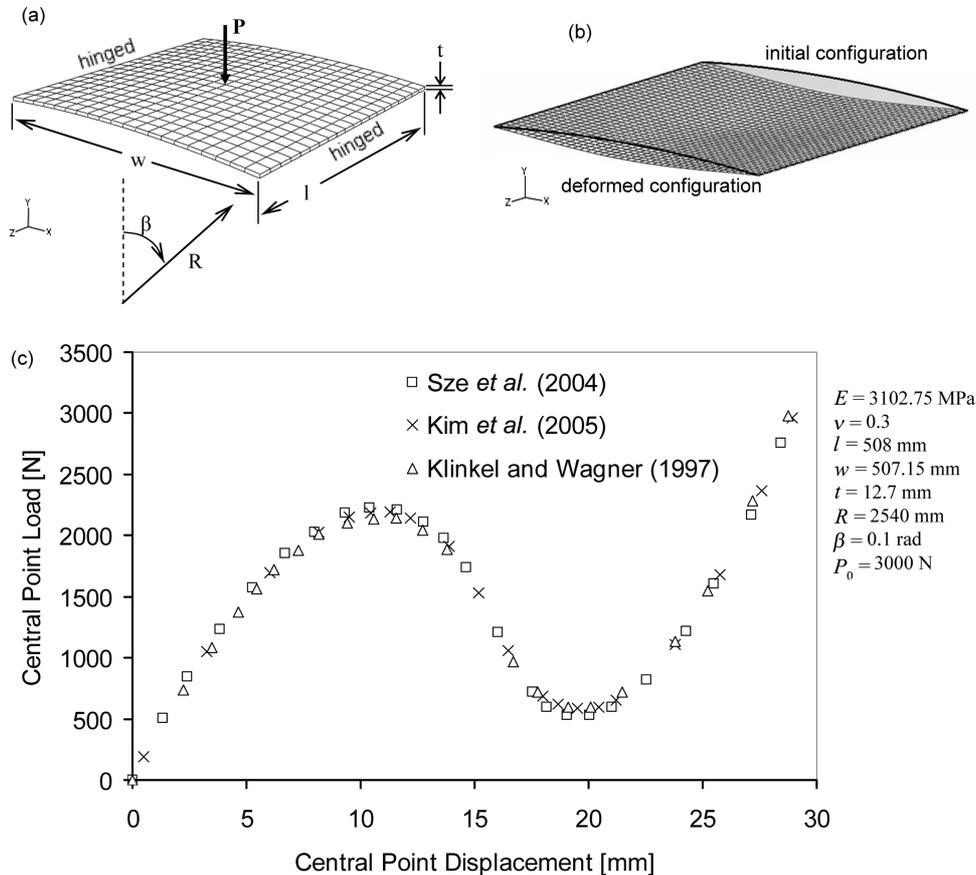


Fig. 9 Hinged thick cylindrical section subjected to a central concentrated load, (a) geometric and loading data, (b) deformed configuration under maximum load, (c) solutions drawn from the literature

Table 8 Riks analysis inputs for the hinged thick cylindrical section subjected to a central concentrated load

Stopping criterion	Initial arc-length	Minimum arc-length	Maximum arc-length
Maximum central point displacement of 30 mm in the negative y direction	0.1	10^{-5}	1

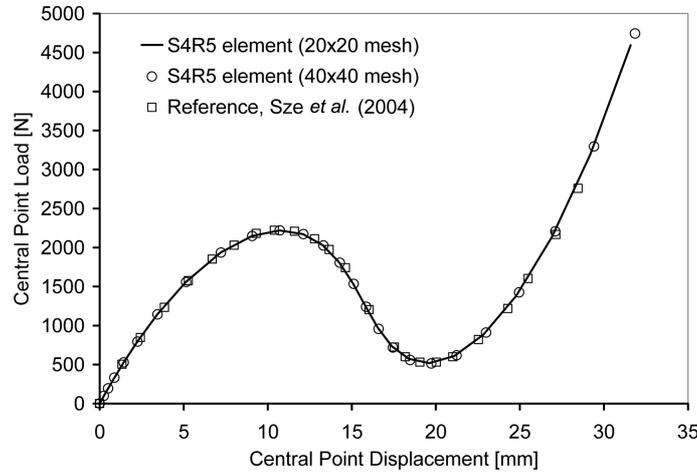


Fig. 10 Load-displacement curves for the hinged thick cylindrical section subjected to a central concentrated load

Table 9 (a) Tabulated displacement and load results for the hinged thick cylindrical section subjected to a central concentrated load, (b) analysis data

(a)

$-u_y$ [mm]	P [N]						
0.00	0	5.14	1562	15.07	1542	22.82	883
0.25	99	7.21	1939	15.80	1255	24.77	1378
0.50	194	9.07	2149	16.54	976	26.90	2134
0.88	332	10.70	2220	17.37	738	29.18	3192
1.43	528	12.10	2172	18.37	573	31.58	4594
2.25	796	13.27	2028	19.61	518		
3.44	1145	14.25	1809	21.09	609		

(b)

Element	Mesh	CPU time [sec]	Number of increments	Number of iterations
S4R5	20×20	7.62	25	69
S4R5	40×40	29.5	25	69

literature results. Fig. 10 shows the load versus displacement plot. Tabulated results as well as analysis data are provided in Table 9.

3.5 Lee's frame

This benchmark test is named after S.L. Lee, who was the first to look at this problem (Lee *et al.* 1968). The problem has subsequently been examined by several authors (Smolenski 1999, Planinc and Saje 1999). The geometry and loading (concentrated load) are shown in Fig. 11. The input data for the Riks algorithm is given in Table 10. The results are given in terms of load proportionality factor (LPF) versus displacement in the x and the y directions at the point where the load is applied.

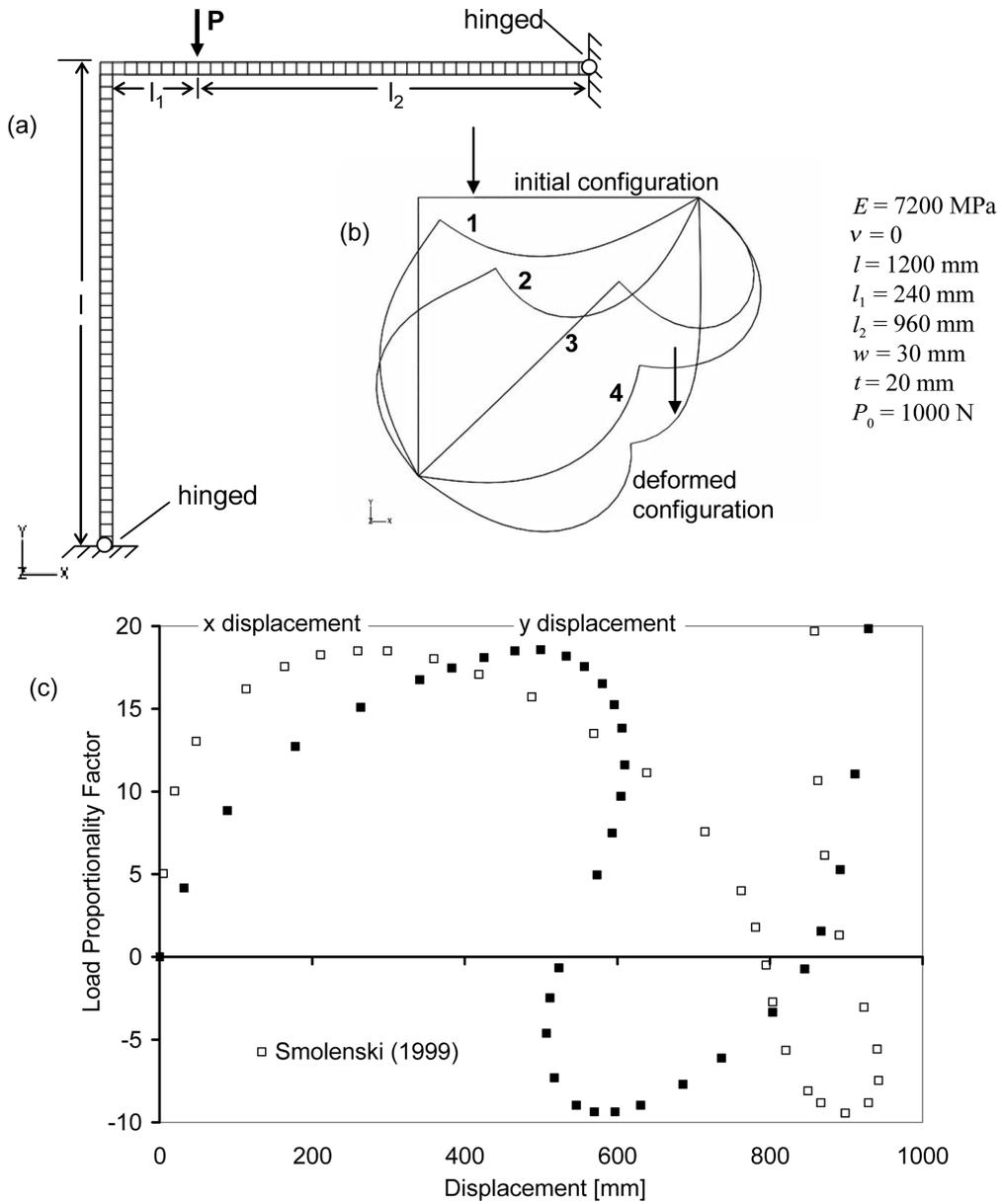


Fig. 11 Lee's frame, (a) geometric, material, and loading data, (b) initial and deformed configurations up to the maximum load, (c) results drawn from Smolenski (1999)

Table 10 Riks analysis inputs for Lee's frame

Stopping criterion	Initial arc-length	Minimum arc-length	Maximum arc-length
Maximum load point displacement of 940 mm in the negative y direction	0.1	10^{-5}	5

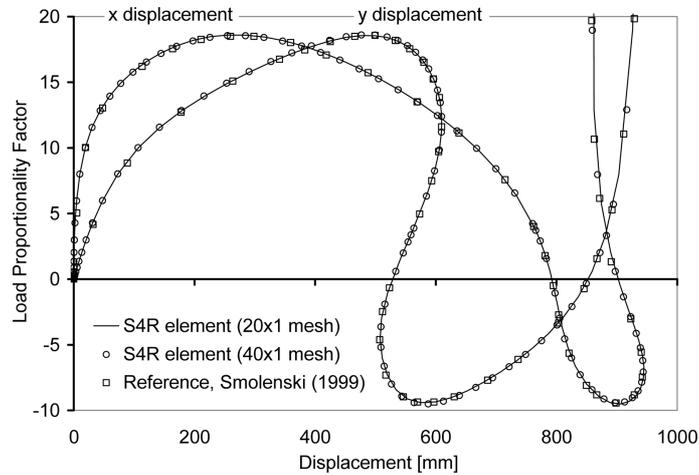


Fig. 12 Load-displacement curves for Lee's frame benchmark test

Table 11 (a) Tabulated displacement and load proportionality factor results for Lee's frame, (b) analysis data (a)

u_x [mm]	$-u_y$ [mm]	LPF	u_x [mm]	$-u_y$ [mm]	LPF	u_x [mm]	$-u_y$ [mm]	LPF
0.00	0.00	0.00	474.75	588.26	16.01	906.42	587.37	-9.51
0.96	20.45	2.99	572.42	607.41	13.45	932.10	639.13	-8.86
10.06	73.00	8.02	670.61	605.74	9.84	944.00	694.11	-7.52
43.76	178.49	12.85	763.93	563.63	3.88	942.23	748.80	-5.74
120.32	326.87	16.57	789.47	533.69	0.59	928.26	800.94	-3.50
226.02	451.60	18.47	808.96	509.16	-3.63	889.87	872.05	2.02
285.31	499.16	18.59	831.17	514.39	-6.63	862.06	916.49	12.91
378.73	552.82	17.78	869.72	543.60	-8.92			

(b)

Element	Mesh	CPU time [sec]	Number of increments	Number of iterations
S4R	20×1	6.02	66	253
S4R	40×1	7.63	65	236

The results obtained with the shell elements match the solution in Lee *et al.* (1968) exactly. Fig. 12 shows the plot of load proportionality factor versus displacement. Tabulated results as well as analysis data such as calculation time are also provided in Table 11. For this geometry the same number of elements was used on the vertical and on the horizontal side. In Fig. 12, the first number stated for the mesh is the number of elements along one side (vertical or horizontal), and not along the entire structure.

3.6 Hinged deep circular arch subjected to a concentrated load

The geometry of this test is presented in Fig. 13. This test is very similar to the previous deep

circular arch; however, in this particular case, the cross-section has different dimensions and both ends are hinged. Boutyour *et al.* (2004) provide a numerical solution in terms of load proportionality factor versus displacement. The entire geometry was modeled in this test as well; the Riks analysis parameters used are reported in Table 12.

The results obtained with the shell elements are the closest to the solution in the literature. Fig. 14

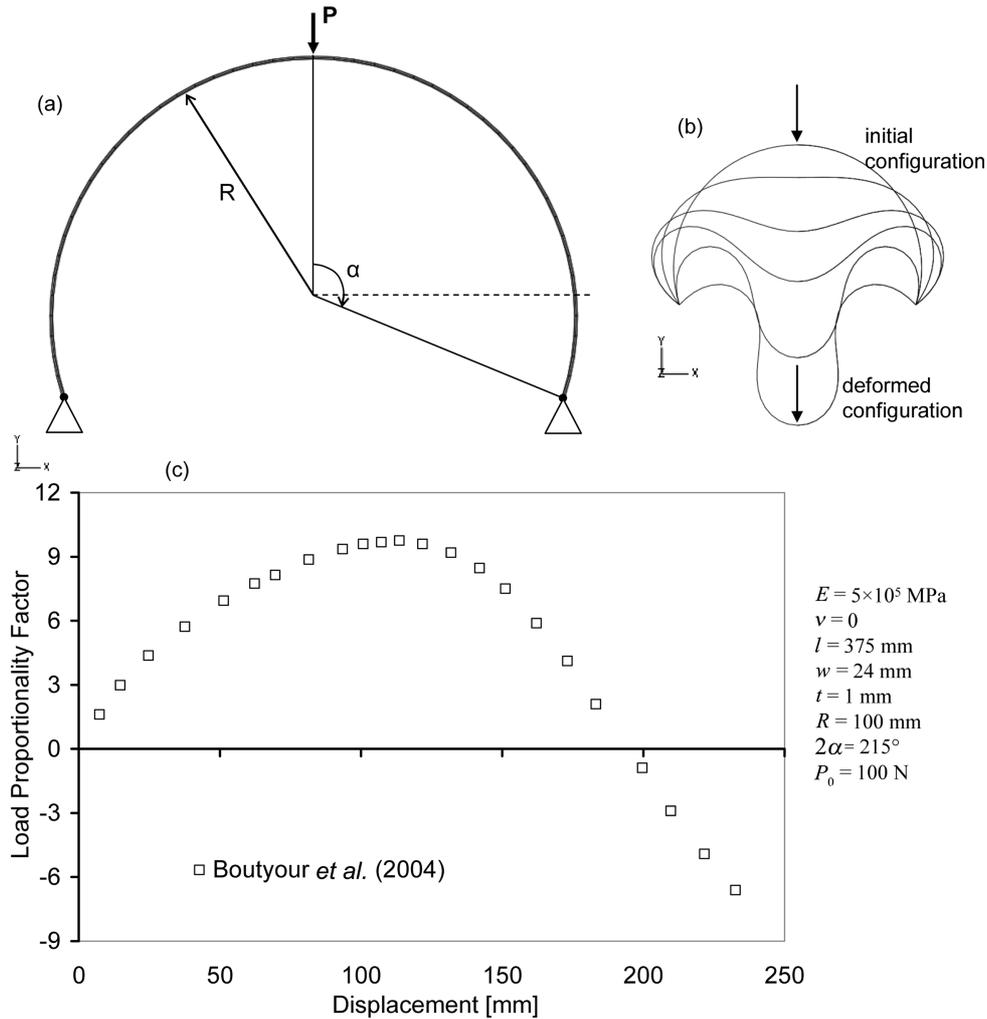


Fig. 13 (a) Geometric, material, and loading data for the hinged deep circular arch subjected to a concentrated load, (b) intermediate and final deformed configurations, (c) load-displacement curve drawn from the literature

Table 12 Riks analysis inputs for the hinged deep circular arch subjected to a concentrated load

Stopping criterion	Initial arc-length	Minimum arc-length	Maximum arc-length
Maximum load point displacement of 220 mm in the negative y direction	0.5	10^{-5}	default value

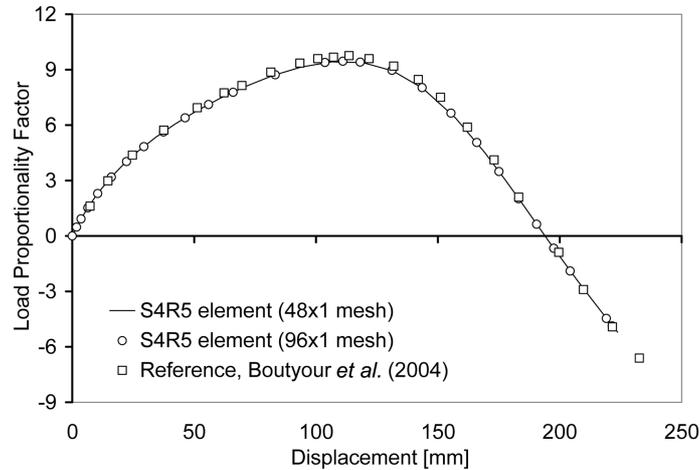


Fig. 14 Load-displacement curves for the hinged deep circular arch benchmark test

Table 13 (a) Tabulated displacement and load proportionality factor results for the hinged deep circular arch subjected to a concentrated load, (b) analysis data

(a)

$-u_y$ [mm]	LPF	$-u_y$ [mm]	LPF	$-u_y$ [mm]	LPF	$-u_y$ [mm]	LPF
0.00	0.00	60.79	7.46	143.80	7.99	201.56	-1.39
10.37	2.29	71.21	8.10	157.21	6.38	206.96	-2.36
21.26	3.91	82.29	8.68	169.23	4.51	212.42	-3.31
27.14	4.60	93.99	9.14	177.85	2.99	218.00	-4.26
34.25	5.34	106.46	9.42	184.68	1.74	223.77	-5.21
42.22	6.06	119.25	9.38	190.62	0.63		
51.09	6.77	131.42	8.93	196.16	-0.40		

(b)

Element	Mesh	CPU time [sec]	Number of increments	Number of iterations	Number of cutbacks
S4R5	48×1	3.09	29	144	0
S4R5	96×1	4.11	26	144	2

shows the plot of load proportionality factor versus displacement. The results as well as relevant analysis data are provided in Table 13.

3.7 Hinged shallow circular arch subjected to an inclined load

The geometry of this test is presented in Fig. 15. This test is set apart from the others by the fact that an inclined load is applied. This leads to asymmetric buckling despite the fact that symmetric boundary conditions are prescribed. Kim and Kim (2001) provide a numerical solution in terms of load proportionality factor versus radial and circumferential displacement. The loading is applied at the apex of the 90° arch, for which the straight edges are hinged while the curved edges are free. Table 14 gives the numerical parameters used in the Riks algorithm.

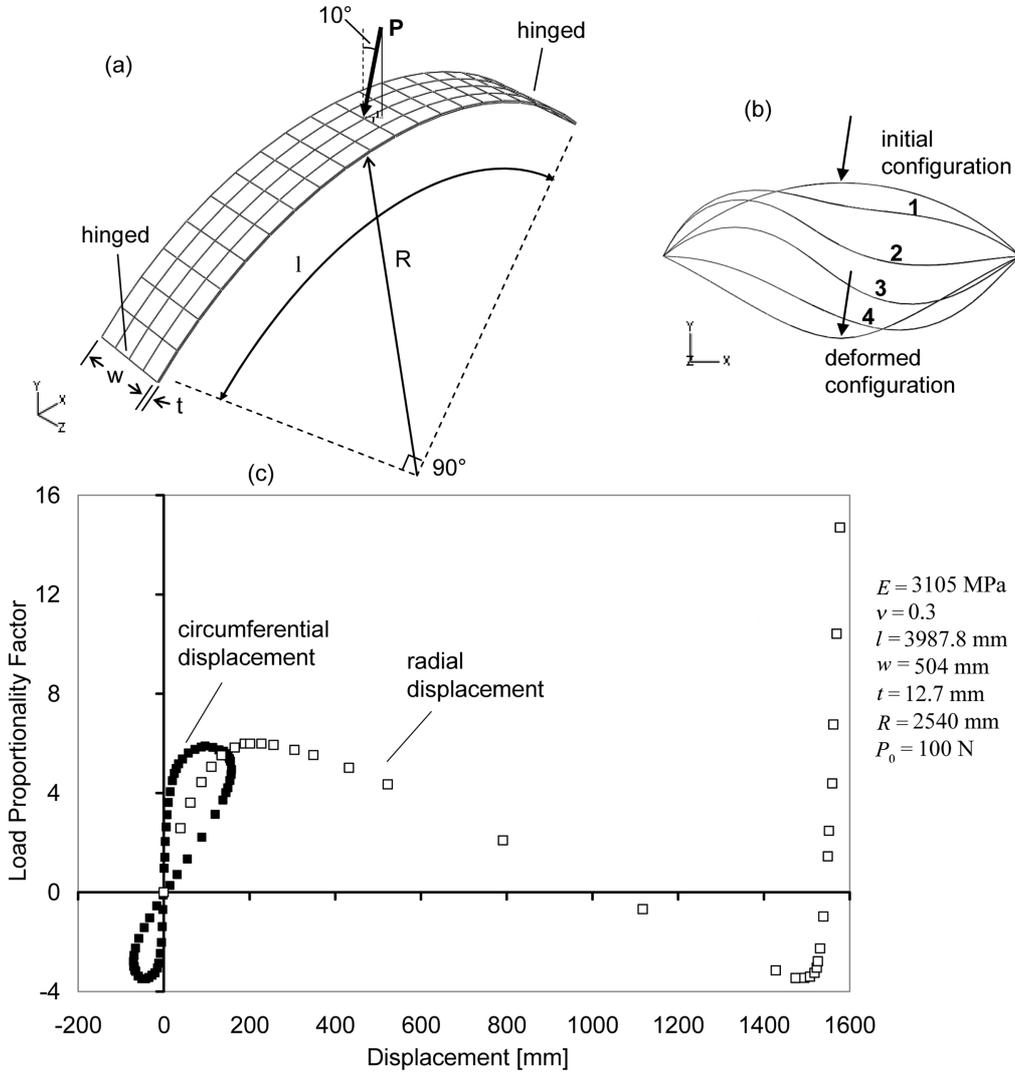


Fig. 15 (a) Geometric, material and loading data for the hinged shallow circular arch subjected to an inclined load, (b) evolution of deformation and load location, (c) solution drawn from Kim and Kim (2001)

Table 14 Riks analysis inputs for the hinged shallow circular arch subjected to an inclined load

Stopping criterion	Initial arc-length	Minimum arc-length	Maximum arc-length
Maximum load proportionality factor of 15	1	10^{-5}	default value

The results obtained with the shell elements match the literature solution exactly. Fig. 16 and Fig. 17 show the plots of load proportionality factor versus radial displacement and circumferential displacement, respectively. Tabulated results as well as analysis data such as calculation time are also provided in Table 15.

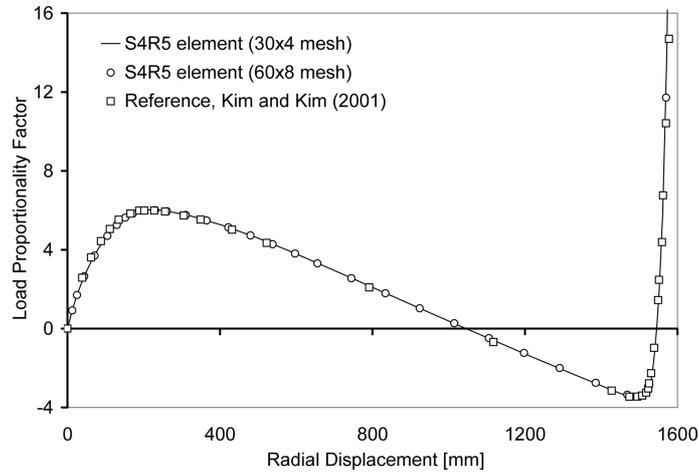


Fig. 16 Load-radial displacement curves for the hinged shallow circular arch subjected to an inclined load

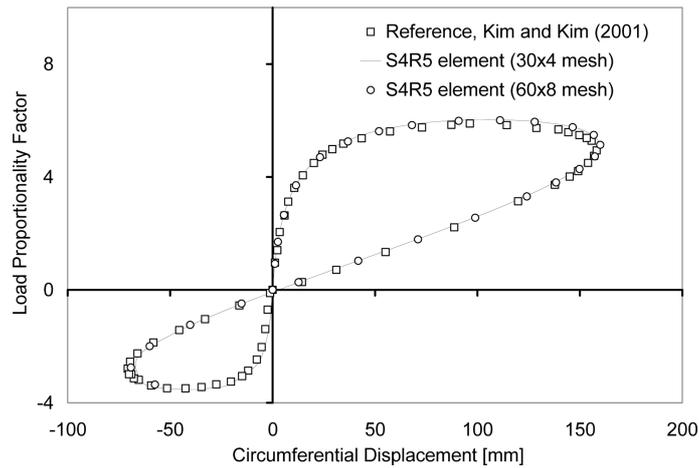


Fig. 17 Load-circumferential displacement curves for the hinged shallow circular arch subjected to an inclined load

Table 15 (a) Tabulated displacement and load proportionality factor results for the hinged shallow circular arch subjected to an inclined load, (b) analysis data

(a)

$-u_x$ [mm]	$-u_y$ [mm]	LPF	$-u_x$ [mm]	$-u_y$ [mm]	LPF	$-u_x$ [mm]	$-u_y$ [mm]	LPF	$-u_x$ [mm]	$-u_y$ [mm]	LPF
0	0	0.00	68	172	5.83	150	538	4.28	-40	1198	-1.24
1	13	0.92	91	201	5.98	138	597	3.80	-60	1291	-2.00
3	25	1.70	111	230	6.01	124	656	3.31	-69	1386	-2.75
6	44	2.65	128	261	5.95	99	745	2.55	-57	1468	-3.35
11	71	3.70	146	310	5.76	71	834	1.79	1	1570	11.72
23	105	4.70	157	365	5.49	42	924	1.03	1	1583	28.13
37	130	5.26	160	422	5.14	13	1015	0.27			
52	152	5.62	157	480	4.73	-15	1106	-0.49			

Table 15 Continued
(b)

Element	Mesh	CPU time [sec]	Number of increments	Number of iterations	Number of cutbacks
S4R5	30×4	6.79	41	210	4
S4R5	60×8	15.16	29	151	1

3.8 Cantilever channel section beam

The geometry of this test is presented in Fig. 18, and some numerical input parameters are listed in Table 16. This is an interesting test due to the out-of-plane or lateral deflection that is taking place, a characteristic phenomenon for these particular geometries that has not been seen in the previous tests. Several authors have looked at this problem (Chrosielewski *et al.* 1992, Betsch *et*

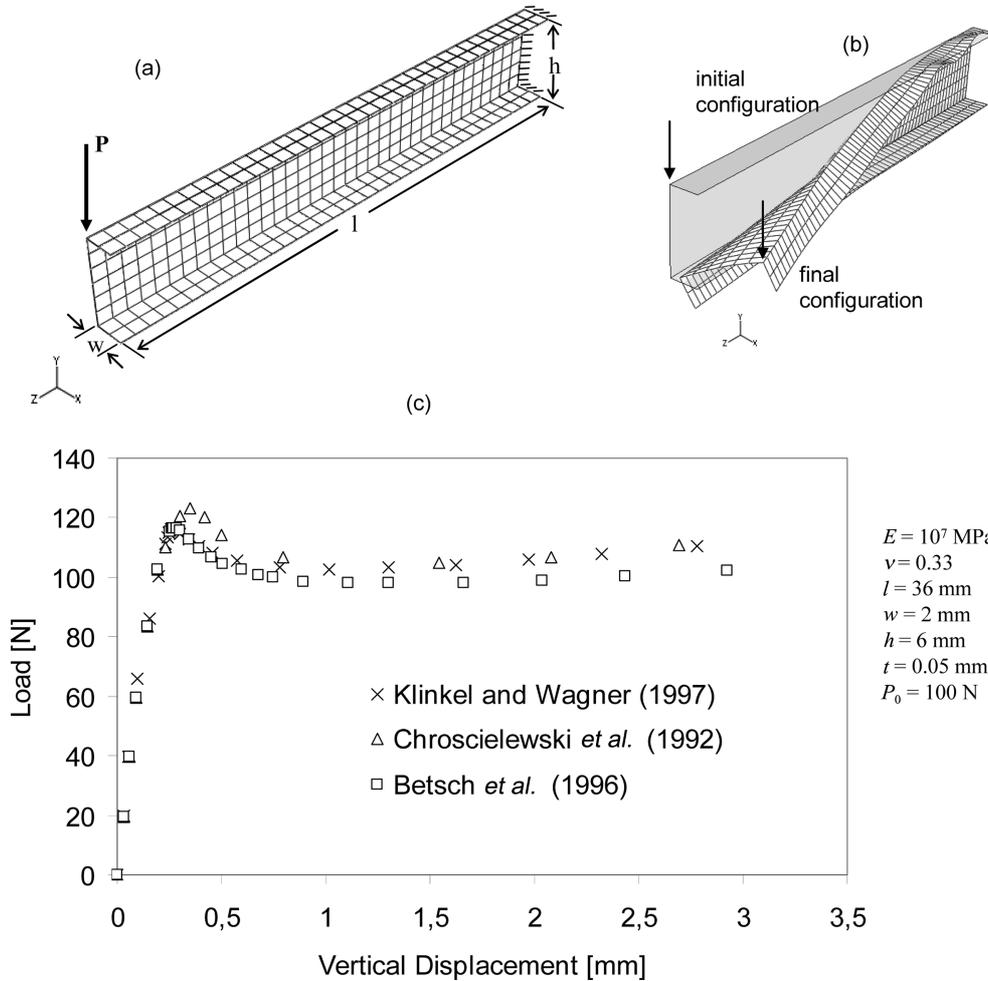


Fig. 18 Cantilever channel section beam, (a) geometric, material, and loading data, (b) evolution of deformation and load location, (c) solutions drawn from the literature

Table 16 Riks analysis inputs for the cantilever channel section beam

Stopping criterion	Initial arc-length	Minimum arc-length	Maximum arc-length
Maximum load point displacement of 3 mm in the negative y direction	0.1	10^{-5}	default value

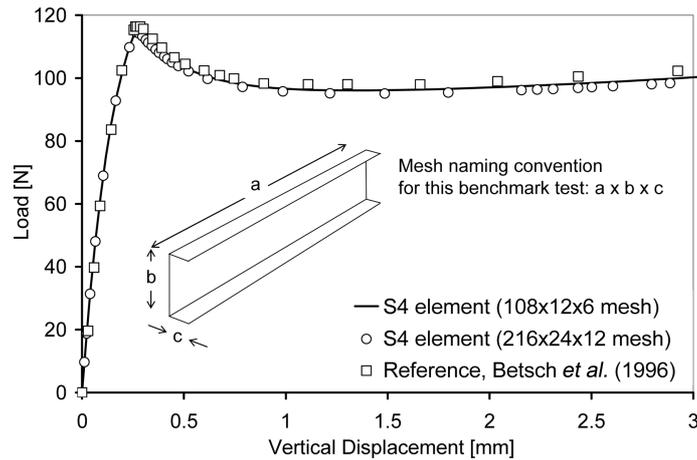


Fig. 19 Load-displacement curves for the cantilever channel section beam

Table 17 (a) Tabulated displacement and load results for the cantilever channel section beam, (b) analysis data

(a)

$-u_y$ [mm]	P [N]						
0.00	0.0	0.17	94.7	0.33	111.6	1.41	96.1
0.02	18.8	0.23	109.5	0.39	108.1	1.81	96.6
0.04	31.4	0.26	114.6	0.54	102.2	2.26	97.7
0.07	48.1	0.28	114.7	0.77	98.2	2.64	98.9
0.12	74.8	0.29	113.9	1.06	96.4	3.05	100.5

(b)

Element	Mesh	CPU time [sec]	Number of increments	Number of iterations	Number of cutbacks
S4	108×12×6	345.8	55	284	0
S4	216×24×12	1028	35	179	7

al. 1996, Klinkel and Wagner 1997). The numerical solutions are given in terms of load versus vertical displacement at the load point. This test exhibits relatively large differences between the different results found in the literature. Our calculations indicate that this is probably due to different mesh densities used.

The results obtained with the shell elements were the closest to the results found in the literature. There were some differences with the literature, however, that we find are most likely due to mesh

refinement. The S4 element performed the best. The plot of load versus vertical displacement is shown in Fig. 19 and results as well as analysis data are provided in Table 17.

3.9 Elastic-plastic case: Hinged thin cylindrical section subjected to a central concentrated load

All of the cases previously studied were elastic. Plasticity is investigated by looking at how the load-displacement curves of the cylindrical section test cases are affected by various choices of plastic parameters, while keeping all of the previous inputs the same. Voce's saturating type nonlinear isotropic hardening model (Voce 1948) is available in ABAQUS, defining the yield stress σ^0 as a function of the equivalent plastic strain $\bar{\varepsilon}^{pl}$

$$\sigma^0 = \sigma|_0 + Q_\infty(1 - e^{-b\bar{\varepsilon}^{pl}}) \quad (1)$$

where $\sigma|_0$ is the initial yield stress of the material, while Q_∞ and b are hardening parameters corresponding to the saturation value and saturation rate of hardening, respectively. Two sensitivity studies were carried out, the first one to investigate the effect of initial yield stress on the buckling response and the second to investigate the effect of the hardening saturation value Q_∞ on the buckling response. The second isotropic hardening parameter b was held constant throughout at $b = 2$. For the first study, the initial yield stress was varied between 3 and 11 MPa, while Q_∞ was held constant at 9 MPa (Fig. 20). Note that a larger displacement (55 mm) was imposed as a stopping criterion instead of the previous displacement of 30 mm (Section 3.3), so that the effects of the elastic-plastic behavior could be clearly seen. Table 18 provides the tabular data for the three elastic-plastic simulations, in which the entire geometry was modeled.

Another aspect, which is important for elastic-plastic applications, concerns the selection of the adequate number of through-thickness integration points. This issue has been discussed in several contributions, through extensive testing over a large number of selective and representative benchmark problems (see, e.g., Abed-Meraim and Combescure 2009). It has been revealed that

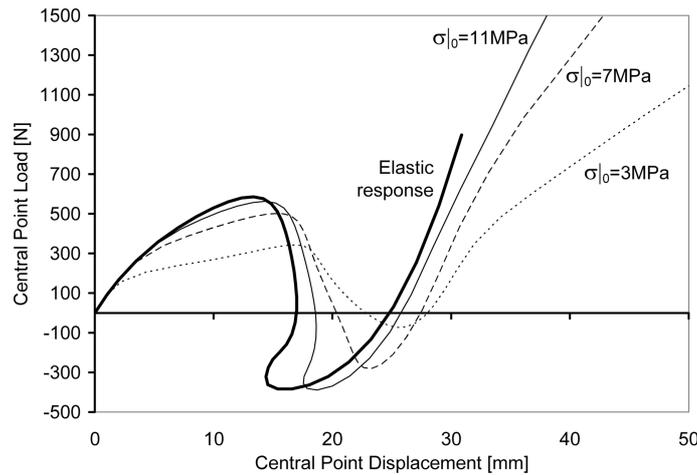


Fig. 20 Elastic-plastic hinged thin cylindrical section subjected to a central concentrated load. The initial yield stress was varied between 3 and 11 MPa, keeping Q_∞ constant at 9 MPa

Table 18 Elastic-plastic hinged thin cylindrical section subjected to a central concentrated load; $Q_\infty = 9$ MPa, (a) displacement and load results for initial yield stress = 3 MPa, (b) displacement and load results for initial yield stress = 7 MPa, (c) displacement and load results for initial yield stress = 11 MPa

(a)

$-u_y$ [mm]	P [N]						
0.00	0	18.20	317	24.32	-54	36.84	603
1.04	92	18.74	278	24.93	-67	39.60	719
2.23	158	19.22	231	25.56	-73	42.19	828
4.36	206	19.72	187	26.23	-70	44.64	930
7.05	239	20.25	146	26.95	-53	47.01	1026
9.47	264	20.80	108	27.72	-19	49.29	1116
11.62	288	21.38	73	28.57	39	51.49	1203
13.49	312	21.95	41	29.51	122	53.62	1286
15.11	331	22.54	12	30.58	227	55.70	1367
16.47	343	23.13	-13	31.97	348		
17.49	340	23.72	-36	34.09	479		

(b)

$-u_y$ [mm]	P [N]						
0.00	0	16.47	491	20.95	-86	29.00	201
1.03	92	17.11	461	21.27	-134	30.73	436
2.04	169	17.57	413	21.56	-179	33.13	706
3.57	259	17.95	355	21.86	-220	36.19	991
5.74	337	18.31	295	22.19	-254	39.87	1273
7.86	388	18.67	235	22.63	-276	43.66	1564
9.82	427	19.06	177	23.25	-281	47.23	1854
11.58	458	19.45	121	24.08	-262	50.58	2137
13.15	483	19.85	67	25.08	-211	53.78	2406
14.51	498	20.24	14	26.26	-120	56.85	2663
15.62	502	20.61	-37	27.58	15		

(c)

$-u_y$ [mm]	P [N]						
0.00	0	15.91	530	18.47	-185	28.48	333
1.03	92	16.44	491	18.23	-237	30.76	621
2.04	169	16.84	439	17.92	-282	33.52	949
3.50	262	17.17	380	17.62	-320	36.55	1325
5.38	355	17.47	318	17.57	-355	40.02	1727
7.20	421	17.75	255	17.86	-381	43.97	2141
8.96	471	18.01	190	18.73	-389	47.95	2580
10.56	510	18.24	126	19.99	-369	51.75	3028
12.00	539	18.44	61	21.49	-318	55.35	3461
13.28	557	18.58	-3	23.13	-229		
14.36	563	18.65	-66	24.86	-95		
15.22	554	18.62	-127	26.63	91		

while one or two integration points are sufficient in the context of elasticity, at least five integration points are required to capture the nonlinear effects characteristic of elasto-plasticity.

For the second study, the isotropic hardening parameter Q_∞ was varied between 3 and 15 MPa, while the initial yield stress was held constant at 7 MPa (Fig. 21). The differences are much less pronounced in this sensitivity study, with the stable post-buckling phase the only one affected. The results are found in Table 19, with the combination of initial yield stress equal to 7 MPa and Q_∞ equal to 9 MPa omitted because it was previously presented in Table 18(b). Finally, Table 20 summarizes the parameter values and convergence information for the five simulations of this elastic-plastic benchmark test in which the complete geometry was meshed.

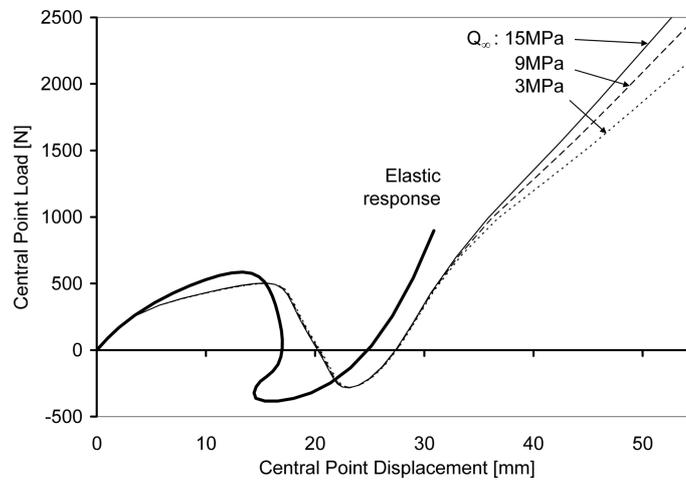


Fig. 21 Elastic-plastic hinged thin cylindrical section subjected to a central concentrated load. The isotropic hardening constant Q_∞ was varied between 3 and 15 MPa, keeping the initial yield stress constant at 7 MPa

Table 19 Elastic-plastic hinged thin cylindrical section subjected to a central concentrated load; initial yield stress = 7 MPa, (a) tabulated displacement and load results for $Q_\infty = 3$ MPa, (b) tabulated displacement and load results for $Q_\infty = 15$ MPa

(a)

$-u_y$ [mm]	P [N]						
0.00	0	16.56	490	21.07	-86	29.12	208
1.03	92	17.20	460	21.39	-134	30.87	443
2.04	169	17.67	413	21.69	-179	33.39	711
3.57	259	18.05	354	21.99	-219	36.72	988
5.74	337	18.41	293	22.32	-252	40.94	1257
7.89	387	18.78	234	22.76	-274	45.37	1542
9.85	426	19.16	176	23.38	-278	49.51	1830
11.63	457	19.56	120	24.21	-258	53.37	2104
13.22	481	19.96	66	25.22	-206	57.07	2362
14.59	497	20.35	14	26.39	-115		
15.71	501	20.73	-37	27.69	21		

Table 19 Continued
(b)

$-u_y$ [mm]	P [N]						
0.00	0	16.39	492	20.85	-86	28.89	194
1.03	92	17.02	462	21.16	-134	30.59	429
2.04	169	17.49	414	21.45	-180	32.92	700
3.57	259	17.86	356	21.74	-221	35.81	990
5.73	337	18.22	296	22.07	-255	39.17	1281
7.85	389	18.58	236	22.50	-278	42.61	1575
9.79	428	18.96	178	23.12	-284	45.86	1868
11.53	460	19.36	122	23.95	-265	48.95	2155
13.09	484	19.75	68	24.96	-215	51.91	2431
14.43	500	20.13	15	26.14	-125	54.74	2695
15.54	504	20.50	-36	27.46	10	57.48	2949

Table 20 Analysis data for elastic-plastic hinged thin cylindrical section subjected to a central concentrated load

Element	Mesh	Initial yield stress [MPa]	Q_∞ [MPa]	CPU time [sec]	Number of increments	Number of iterations
S4R5	40×40	3	9	65.7	41	143
S4R5	40×40	7	9	59.9	42	135
S4R5	40×40	11	9	59.5	44	137
S4R5	40×40	7	3	58.6	41	134
S4R5	40×40	7	15	62.1	43	141

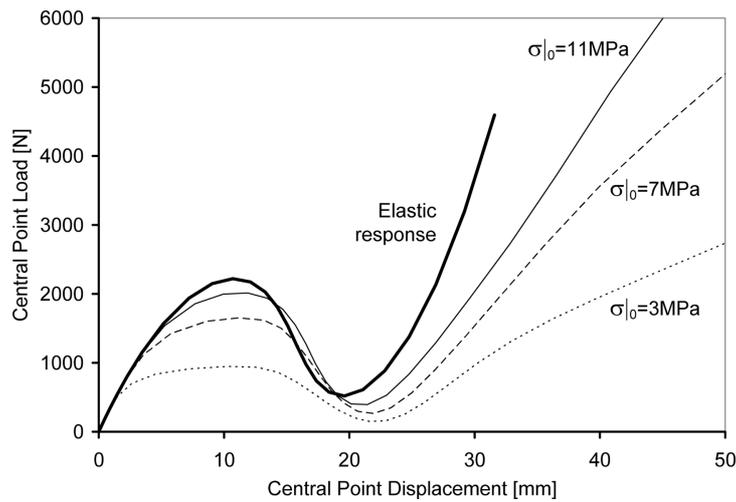


Fig. 22 Elastic-plastic hinged thick cylindrical section subjected to a central concentrated load. The initial yield stress was varied between 3 and 11 MPa, keeping Q_∞ constant at 9 MPa

Table 21 Elastic-plastic hinged thick cylindrical section subjected to a central concentrated load; $Q_\infty = 9$ MPa, (a) displacement and load results for initial yield stress = 3 MPa, (b) displacement and load results for initial yield stress = 7 MPa, (c) displacement and load results for initial yield stress = 11 MPa

(a)							
$-u_y$ [mm]	P [N]						
0.00	0	10.35	949	21.61	150	39.64	1926
0.25	99	12.69	934	22.91	159	43.18	2207
0.51	194	14.31	860	24.34	247	46.68	2479
0.89	331	15.65	736	25.97	421	50.11	2742
1.51	513	16.88	588	27.91	681	53.47	3001
2.64	699	18.06	437	30.23	996	56.79	3260
4.50	834	19.21	304	32.96	1316		
7.24	913	20.39	203	36.17	1631		
(b)							
$-u_y$ [mm]	P [N]						
0.00	0	8.65	1603	19.57	416	35.72	2733
0.25	99	11.16	1652	20.67	297	39.93	3549
0.51	194	13.14	1619	21.91	267	44.67	4347
0.88	332	14.58	1499	23.31	345	49.66	5135
1.44	527	15.70	1297	24.94	556	54.61	5913
2.27	793	16.69	1062	26.89	906	59.31	6657
3.59	1118	17.62	818	29.28	1386		
5.77	1426	18.57	596	32.14	1988		
(c)							
$-u_y$ [mm]	P [N]						
0.00	0	7.68	1856	18.13	726	32.80	2723
0.25	99	9.95	1995	19.06	524	36.56	3728
0.51	194	11.89	2013	20.15	403	40.85	4936
0.88	332	13.46	1936	21.45	395	45.87	6215
1.44	527	14.69	1776	22.97	530	51.62	7496
2.26	795	15.69	1547	24.74	833	57.73	8814
3.47	1141	16.54	1273	26.93	1298		
5.27	1539	17.31	985	29.58	1929		

3.10 Elastic-plastic case: Hinged thick cylindrical section subjected to a central concentrated load

Plasticity is investigated for the thick cylindrical section using the same approach that was used for its thin counterpart. For the first study, the initial yield stress was varied between 3 and 11 MPa, while Q_∞ was held constant at 9 MPa (Fig. 22). The results are listed in Table 21. Again, as for the elastic case treated in Section 3.4, the model is meshed entirely.

For the second study, the isotropic hardening parameter Q_∞ was varied between 3 and 15 MPa,

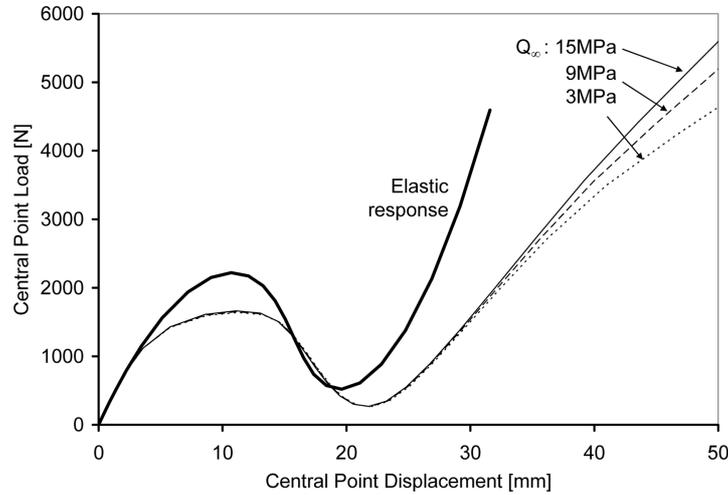


Fig. 23 Elastic-plastic hinged thick cylindrical section subjected to a central concentrated load. The isotropic hardening parameter Q_∞ was varied between 3 and 15 MPa, keeping the initial yield stress constant at 7 MPa

Table 22 Elastic-plastic hinged thick cylindrical section subjected to a central concentrated load; initial yield stress = 7 MPa, (a) tabulated displacement and load results for $Q_\infty = 3$ MPa, (b) tabulated displacement and load results for $Q_\infty = 15$ MPa

(a)

$-u_y$ [mm]	P [N]						
0.00	0	8.70	1594	19.69	408	36.25	2726
0.25	99	11.24	1641	20.79	293	40.96	3491
0.51	194	13.24	1607	22.03	265	46.60	4226
0.88	332	14.68	1488	23.44	347	52.92	4985
1.44	527	15.81	1286	25.07	561	59.18	5776
2.27	793	16.80	1051	27.03	915		
3.59	1117	17.73	808	29.46	1396		
5.79	1423	18.68	587	32.43	1995		

(b)

$-u_y$ [mm]	P [N]						
0.00	0	8.60	1611	19.46	423	35.31	2732
0.25	99	11.09	1663	20.55	302	39.24	3576
0.51	194	13.05	1630	21.79	268	43.52	4410
0.88	332	14.49	1509	23.20	344	47.93	5219
1.44	527	15.61	1308	24.82	551	52.28	6007
2.27	793	16.60	1072	26.77	898	56.46	6755
3.58	1118	17.53	829	29.12	1377		
5.75	1429	18.47	605	31.90	1980		

Table 23 Analysis data for elastic-plastic hinged thick cylindrical section subjected to a central concentrated load

Element	Mesh	Yield stress [MPa]	Q_∞ [MPa]	CPU time [sec]	Number of increments	Number of iterations
S4R5	40×40	3	9	51.0	29	108
S4R5	40×40	7	9	44.4	29	95
S4R5	40×40	11	9	41.9	29	92
S4R5	40×40	7	3	44.4	28	94
S4R5	40×40	7	15	44.2	29	96

while the initial yield stress was held constant at 7 MPa (Fig. 23). The tabulated results are found in Table 22, with the combination of initial yield stress equal to 7 MPa and Q_∞ equal to 9 MPa omitted because it was previously presented in Table 22(b). Convergence information for this elastic-plastic benchmark test is provided in Table 23.

4. Further investigation of the benchmark tests

This section presents some additional notable observations including, for instance, comments on the application of boundary conditions and the convergence tolerance used for running buckling simulations. Some aspects of the performance of solid and solid-shell elements in this type of simulation are also discussed. For more details, the reader may refer to a recent contribution by Killpack and Abed-Meraim (2011).

4.1 Solid and solid-shell elements

Developers of continuum-based finite elements can also use the benchmark tests presented in this paper to address the performance of new elements in this category. More specifically, solid-shell elements with a three-dimensional geometry but exhibiting shell-type behavior as well as enhanced assumed strain (EAS) or assumed natural strain (ANS) solid elements have been developed during the last decade and are intended for use in the simulation of thin structures (see, for example, Klinkel and Wagner 1997, Cho *et al.* 1998, Hauptmann and Schweizerhof 1998, Sze and Zheng 2002, Abed-Meraim and Combescure 2002, Areias *et al.* 2003, Legay and Combescure 2003, Chen and Wu 2004, Kim *et al.* 2005, Alves de Sousa *et al.* 2006, Reese 2007, Abed-Meraim and Combescure 2009, 2011). In this framework, the SC8R solid-shell element available in ABAQUS performed well in several of the tests selected in this paper. It is quite powerful in terms of speed, with the calculation time about the same or even faster in certain cases than that of the shell elements. The main problem with this solid-shell element is that convergence difficulties may be encountered in certain situations.

As mentioned in the introduction, the C3D8, C3D8I, and C3D8R solid elements were also tested. It is well-known that linear, low-order elements like these suffer from various locking problems (shear, membrane, volumetric), and thus are not well-suited for this type of structural analysis. In such bending-dominated problems where thin structures are subjected to large rotations, there are two main numerical problems associated with the C3D8 and the C3D8R elements. The C3D8

element, which is a fully integrated linear brick element, is subject to shear and membrane locking. This phenomenon makes the element overly stiff in bending applications; therefore, the displacement calculated for a given force would be smaller than the actual solution. The C3D8I element includes incompatible modes specifically implemented to get rid of this effect, and therefore performs much better. The drawback is that it is also more expensive. The C3D8R element, which is a reduced integration linear brick element, is subject to hourglassing. This phenomenon makes the element excessively flexible in bending applications; therefore, the displacement calculated for a given force would be larger than the actual solution. Most of these problems can be overcome if the mesh is sufficiently fine, though at the cost of extra computing time.

For illustration, Fig. 24 shows the results for the clamped shallow arch subjected to pressure loading (Section 3.1) where all shell, solid, and solid-shell elements gave good results. Given the fact that this is a shallow arch and hence that the rotations are not that large, the solid elements did not have many difficulties; for the C3D8I element, however, the calculation time was twice that of the shell or solid-shell elements, as shown in Table 24.

4.2 Application of boundary conditions for solid and solid-shell elements

The way boundary conditions are applied is very important for both solid and solid-shell

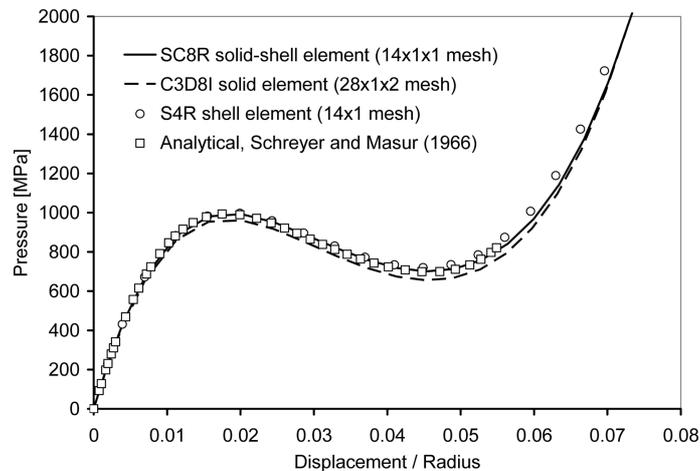


Fig. 24 Load-displacement curves for the clamped shallow arch subjected to pressure loading that include the results for the SC8R and the C3D8I elements

Table 24 Analysis data for the converged shell, solid, and solid-shell meshes for the clamped shallow arch subjected to pressure loading

Element	Mesh	CPU time [sec]	Number of increments	Number of iterations	Number of cutbacks
S4R	14×1	1.2	20	53	0
SC8R	14×1×1	1.2	20	51	0
C3D8I	28×1×2	2.3	20	51	0

elements. The hinged thin cylindrical section subjected to a central concentrated load (Section 3.3) is used here to illustrate this issue. The C3D8I solid element and the SC8R solid-shell element were studied. As illustrated in Fig. 25(b,c,d), hinged boundary conditions can be prescribed on the top edge, on the bottom edge, or on the neutral axis. Note that in order to place the boundary conditions on the neutral axis, two elements have to be placed along the thickness. The results vary significantly with boundary condition placement, with the response corresponding to shell elements obtained when the boundary conditions are placed on the neutral axis. This effect of boundary conditions was also pointed out in Legay and Combescure (2003) for the hinged thick cylindrical section subjected to a central concentrated load (Section 3.4), by applying boundary conditions on both the bottom edge and the neutral axis. For the hinged thin cylindrical section test investigated here, the results obtained with the SC8R solid-shell element were very similar to those yielded by

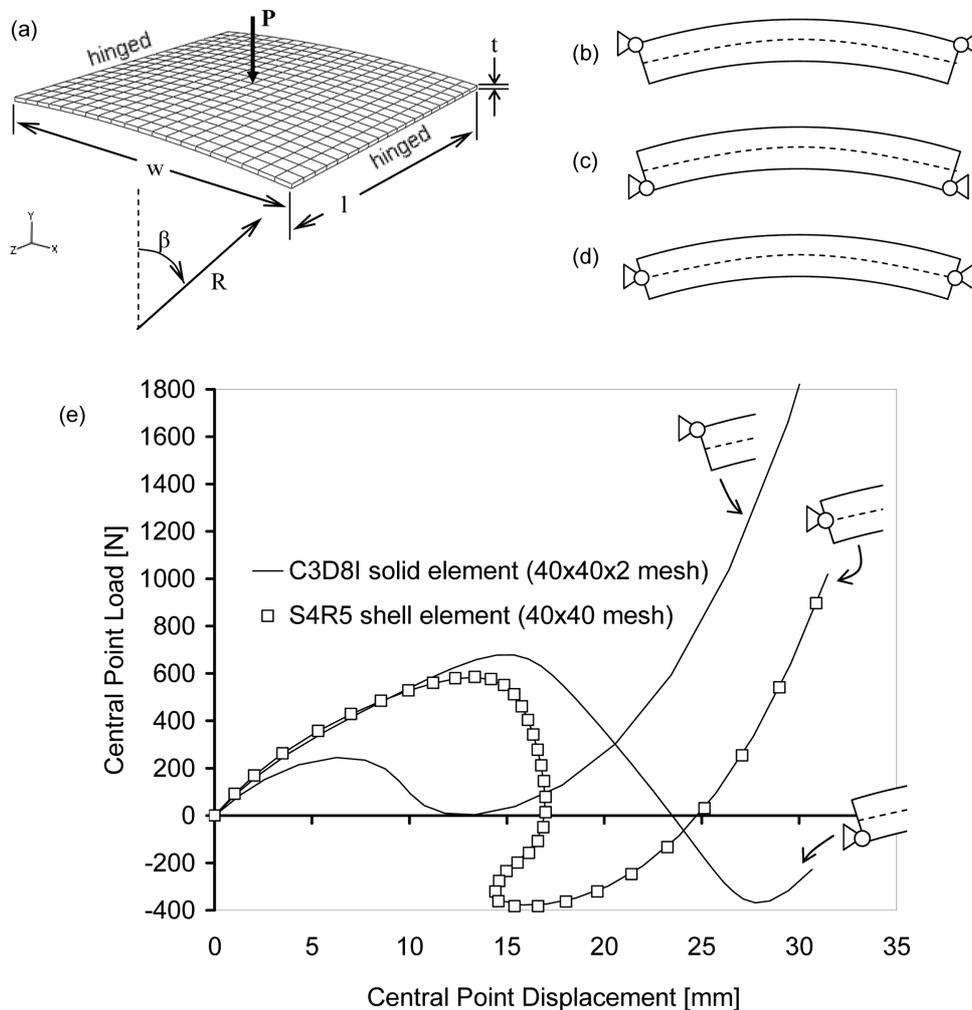


Fig. 25 (a) Hinged thin cylindrical section subjected to a central concentrated load. Hinged boundary condition placement: (b) top edge, (c) bottom edge, (d) neutral axis, (e) results obtained with the C3D8I solid element for different placements of the hinged boundary conditions

the C3D8I solid element; therefore the results shown in Fig. 25 are for the C3D8I solid element.

4.3 Prediction of bifurcation solution paths

Some of the problems presented in this paper may contain more than one equilibrium path. For example, it was seen in certain cases that if the mesh was refined with all other conditions kept identical, the solution was completely different, simply because another equilibrium path was found. In cases like this, a tight convergence tolerance must be used in order to obtain the results shown in Section 3. This convergence criterion is the ratio of the largest residual to the corresponding average flux norm, which basically determines how close the calculated solution has to be to the actual solution before the solver can judge that the calculation is finished. For further information, the interested reader can consult the ABAQUS documentation (2007), in which the default value of the convergence criterion is set to 0.005, but can be modified by the user for some specific applications. The clamped-hinged deep circular arch test illustrates this very well. The model shown in Fig. 26 uses the SC8R element ($192 \times 1 \times 2$ mesh) with the hinged boundary condition applied on the exterior (top) edge. However, this problem is not specific to continuum-based elements.

As seen in Fig. 26(b), some primary as well as secondary bifurcations may lead to either physical (Wardle 2008) or non-physical solutions. Also, note that some bifurcated solution branches occurring prior to limit points could be avoided in certain cases by meshing only a portion of the structure, chosen according to the symmetry of the problem. This symmetry constraint eliminates non-symmetric bifurcation modes.

Wardle (2006, 2008) gives another solution for the hinged thin cylindrical section under a central concentrated load, different from the symmetric buckling solution that involves both a load-limit point ('snap-through') and a deflection-limit point ('snap-back') as shown in Section Hinged thin cylindrical section subjected to a central concentrated load. Most other authors that have studied this test have modeled only a quarter of the geometry, and hence were not able to see the bifurcated

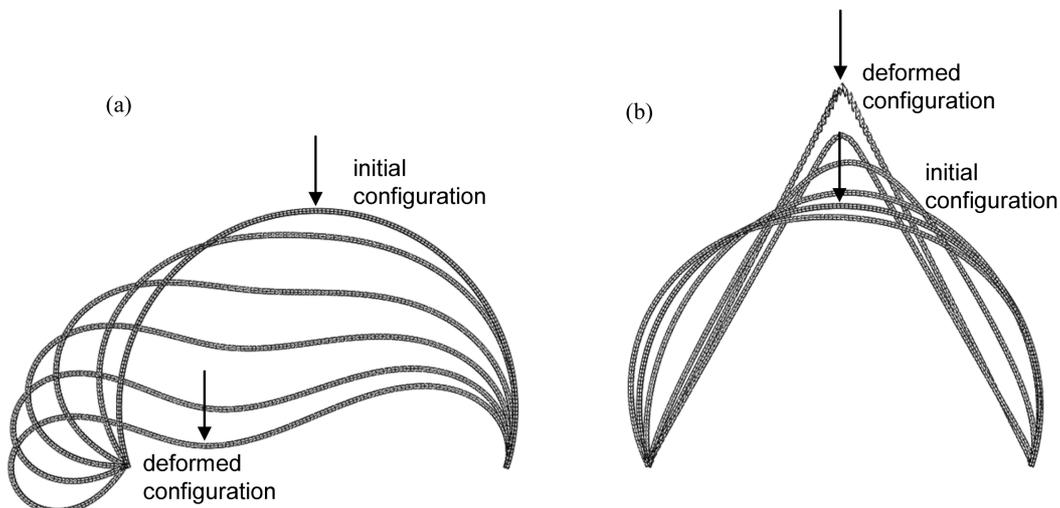


Fig. 26 (a) Intermediate and final configurations for the clamped-hinged deep circular arch, obtained with a tight convergence criterion ($1/1000 \times$ default), (b) results obtained with the default convergence criterion

solution since the latter occurs prior to the first limit point in the form of an asymmetric bifurcation mode. One of the objectives here was to see whether both solutions could be obtained when the whole geometry was considered. Several traditional techniques for identifying and inducing bifurcation in nonlinear finite element problems have been reported in the literature (Weinitshke 1985, Wagner and Wriggers 1988, Kouhia and Mikkola 1989, Wriggers and Simo 1990, Cho *et al.* 1998, Eriksson *et al.* 1999, Planinc and Saje 1999, Ibrahimbegovic and Al Mikdad 2000, Legay and Combescure 2003, Boutyour *et al.* 2004). In practice, there are two techniques that are widely used to achieve this aim. The first technique relies on bifurcation indicators (e.g., minimum eigenvalue or determinant of the tangent stiffness matrix and the associated eigenmode), which have to be evaluated along the nonlinear fundamental path. The second commonly adopted procedure pinpoints bifurcations and tracks such bifurcated solutions by slightly altering the structure, adding to the initial shape a small geometric imperfection along the first Euler buckling mode (first linear eigenmode revealed, e.g., by a preliminary Euler buckling analysis).

The bifurcation-type buckling solution and the more classical symmetric response are shown for the hinged thin cylindrical section in Fig. 27.

This second bifurcation solution can be obtained using the same converged mesh as before (40×40 with S4R5 elements) by modifying the Riks analysis inputs, as shown in Table 25. This yields the solution shown in Fig. 28. Table 26 shows the tabulated results along with the analysis data for this test. The calculation time is significant here because a very small arc-length was used.

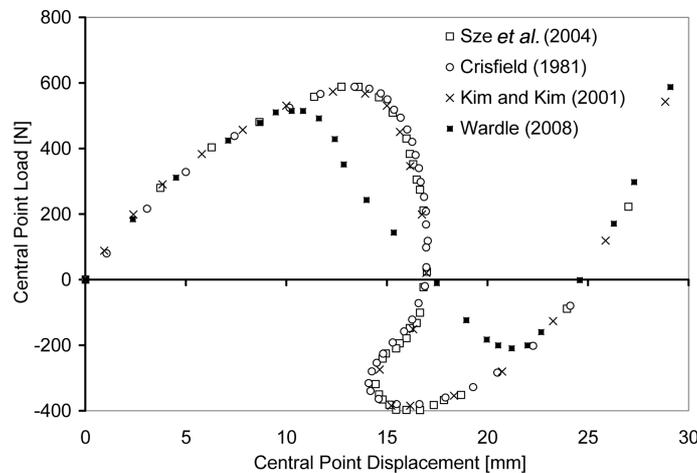


Fig. 27 Fundamental and bifurcated solutions drawn from the literature for the hinged thin cylindrical section subjected to a central concentrated load

Table 25 Riks analysis inputs for the bifurcated branch solution of the hinged thin cylindrical section subjected to a central concentrated load

Stopping criterion	Initial arc-length	Minimum arc-length	Maximum arc-length	Estimated total arc-length
Maximum load proportionality factor of 0.8	0.01	5×10^{-7}	0.1	30

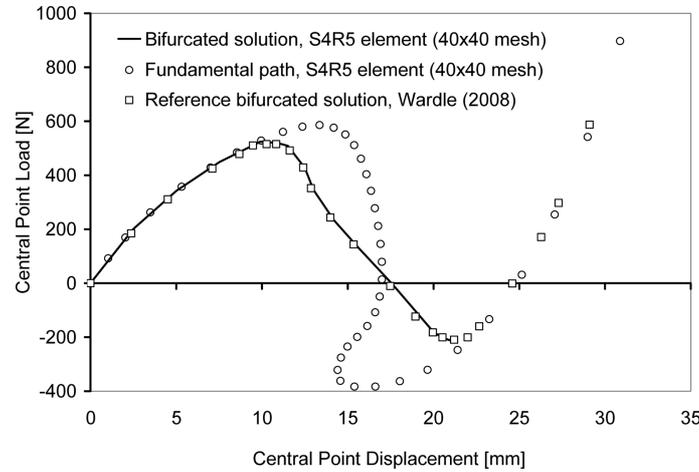


Fig. 28 Fundamental and bifurcated load-displacement curves for the hinged thin cylindrical section subjected to a central concentrated load

Table 26 (a) Displacement and load results for the bifurcation solution of the hinged thin cylindrical section subjected to a central concentrated load, (b) analysis data

(a)

$-u_y$ [mm]	P [N]						
0.00	0	10.12	523	13.00	346	20.51	-201
2.51	201	10.53	521	14.20	233	21.05	-214
5.01	342	11.01	518	15.60	133	21.35	-219
7.52	449	11.51	509	17.61	-4		
9.90	524	12.50	427	20.00	-181		

(b)

Element	Mesh	CPU time [sec]	Number of increments	Number of iterations
S4R5	40×40	2378.2	2000	4002

5. Conclusions

Ten limit-point buckling benchmark problems were selected and presented in this article. For each test, the reference results were given in terms of load-displacement curves as well as in tabulated form. The solutions given here are converged in terms of mesh density and can be confidently used by other researchers as a reference for testing subsequent finite element formulations or new nonlinear solution methods. The convergence performance is presented in terms of calculation time, number of increments, number of iterations and number of cutbacks. The modified path-following Riks algorithm implemented in ABAQUS was used to run all of these tests, with the corresponding inputs presented as well. The aim was to provide a convenient basis of comparison for developers of new finite element models and to eliminate the tedious and inaccurate task of extracting data points from load-displacement curves.

All the tests presented in this article have a relatively simple geometry and loading, however the response is rather complex and can be difficult to model. To this end, all of the necessary data is given so that the reader can recreate the model exactly. It is hoped that this work gathers in a single paper all the necessary information needed by the aforementioned developers when performing limit-point buckling simulations.

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