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Experimental External Force Estimation Using a Non-Linear Observer for 6 axes Flexible-Joint Industrial Manipulators

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Abstract—This paper proposes a non-linear observer to estimate not only the state (position and velocity) of links but also the external forces exerted by the robot during Friction Stir Welding (FSW) processes. The difficulty of performing this process with a robot lies in its lack of rigidity. In order to ensure a better tracking performance, the data such as real positions, velocities of links and external forces are required. However, those variations are not always measured in most industrial robots. Therefore, in this study, an observer is proposed to reconstruct those necessary parameters by using only measurements of motor side. The proposed observer is carried out on a 6 DOF flexible-joint industrial manipulator used in a FSW process.

I. INTRODUCTION

A. Robot and control

Current studies propose to replace some special machine-tools by industrial robots because of their effective cost and larger workspace compared with usual machine-tools. The technical and economic performances of production can be greatly improved by using a manipulator or a robotic system as a tool holder. However, performance issue is one of the reasons that prevent robotization of industrial manufacturing. Moreover, in industrial production, it is very difficult to change the mechanical elements or the inner robot control system. This study concerns an industrial manipulator KUKA KR500 MT-2, which has a payload of 500 kg and can be used for a FSW process [1], [2] where a very significant interaction force is required. Up to now, this process is usually carried out by some specially developed machines, having strongly rigid axes but more expensive. The objective of this work is to realize the required process with a 6 DOF serial chain industrial manipulator.

The concerned robot only has motor side measurements: the angular positions θ and speeds $\dot{\theta}$ as well as the currents of actuators. Due to flexibility of the transmission chain, the state of links cannot be deduced from the one of motor side. In order to facilitate the realization of these operations, the state of links (q, \dot{q}) and the external torque applied on the tool is required to be known. Either the components of the torque are difficult to measure or the sensor required for high forces of FSW is expensive. One solution is to use an observer to estimate those essential parameters [3].

An extended state observer (ESO) is proposed for the state feedback control of a flexible joint robotic system in [4]. This approach is used for state estimation, which is then validated with a Quanser's flexible-joint module. An acceleration-based observer is presented in [5] for state observation with an experimental validation. However, this observer needs measurement of link accelerations, which are generally not measured by industrial robots. [6] investigates methods for tool position estimation of industrial robots, which also requires tool acceleration measurement. An application of disturbance observers to non-linear systems is given in [7] and an observer-based adaptive robust control (ARC) approach for FSW process is discussed in [8] proving that axial force can also be estimated by an observer, however, these approaches do not consider flexibility of joints. Unique Lyapunov-based non-linear observer is difficult to apply systematically [9]. Disturbance observer technique is widely used in mechanical servo systems, and a disturbance dual observer based control algorithm is proposed for industrial robots having flexible joints in [10], which can use state of motor to construct state of link as well as disturbances. Nevertheless, in this paper the observer is under the assumption that the disturbance dynamics are known and proportional to the error of estimation.

B. Contributions and outline of the paper

The contribution of this paper is mainly about the extension of the observer proposed by [11] to cover estimation of external forces applied by the robot by using only position, velocity and current measurements of motor axes. This paper describes an improved observer of our previous work in [12]. This observer is adapted for a 6 DOF flexible robot system, and modified to deal with variable external forces. Simulations and experiments show that the new proposed observer has much better performance than the one we proposed before. With the new observer, significant and variable external forces can be well estimated for industrial robots. Moreover, in this paper, a complete flexible-mode manipulator model of robot KUKA KR500 MT-2 is described.

The modeling of robot and process are presented in Section II. The design of our new observer is described in Section III. In Section IV results of experiments with robot KUKA KR500

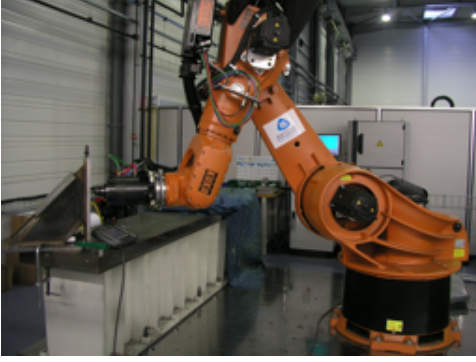


Fig. 1. Robot KUKA KR500 MT-2 (by courtesy of Institut de Soudure)

TABLE I. MDH PARAMETERS OF ROBOT KUKA KR500 MT-2.

j	μ_j	σ_j	α_j	d_j	θ_j	r_j
1	1	0	π	0	q_1	$-L_{1z}$
2	1	0	$\pi/2$	L_{1x}	q_2	0
3	1	0	0	L_2	$\pi/2 + q_3$	0
4	1	0	$-\pi/2$	D_4	q_4	$-L_{34}$
5	1	0	$\pi/2$	0	q_5	0
6	1	0	$-\pi/2$	0	$-\pi/2 + q_6$	$-L_5$
7	0	2	0	0	0	$-L_{tz}$

MT-2 are provided. These results showed good performances of the proposed observer. Finally, conclusions and directions for future work are discussed in Section V .

II. MODELING OF FLEXIBLE JOINT ROBOT AND FSW PROCESS

The robot concerned in this study is a serial chain manipulator (see Fig. 1), main numerical values used for the proposed observer are given in the Appendix. The control problem of this kind of manipulator for precise manufacturing is a challenging task: the manipulator is an elastic multibody, multivariable and strongly coupled system. Its highly non-linear dynamics state change rapidly while manipulator moves in its workspace.

A. Modeling of a 6 DOF flexible manipulator

The Modified Denavit-Hartenberg (MDH) notation is frequently used to model robots including the robot concerned in this research work [13]. The MDH parameters for this manipulator are listed in Table I and are used for the modeling of robot with the help of software *SYMORO+* [14] [15]. All the joints of this manipulator are revolute joints, except the seventh axis that represents the spindle fixed on link 6. The flexible joint robot model suggested by Spong [16] is used in this research work under the assumption that the robot has flexible joints and rigid links.

This robot has a gravity compensation system with a gas accumulator on the second axis to compensate the effects due to gravity of the robot, the expression of this compensator is not presented here, but is used in simulation in section IV-B. According to [17], a flexible joint robot can be modeled as follows:

$$D(q)\ddot{q} = \Gamma - H(q, \dot{q}) - F_{robot}(\dot{q}) - J^T(q)F \quad (1)$$

$$I_a\ddot{\theta} = \Gamma_m - N_v^T\Gamma - F_{motor}(\dot{\theta}) \quad (2)$$

with the expression of link friction:

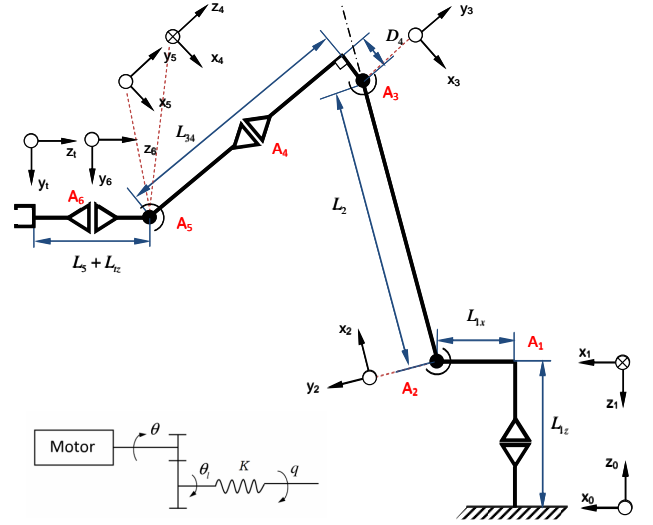


Fig. 2. Robot and flexible gearbox model in 2D.

$$F_{robot}(\dot{q}) = B_s\dot{q} + F_s(\text{sign}(\dot{q})) \quad (3)$$

and the expression of the friction at motors axes:

$$F_{motor}(\dot{\theta}) = B_m\dot{\theta} + F_m(\text{sign}(\dot{\theta})) \quad (4)$$

where $J^T(q)$ is the Jacobian matrix of the tool frame, F is the vector of efforts applied by robot on external environment, Γ_m is the vector of motor torques, Γ is the vector of gearbox torque, vectors $q = [q_1 q_2 q_3 q_4 q_5 q_6]^T$, \dot{q} and \ddot{q} represent angular positions, velocities and accelerations, respectively. Vectors $\theta = [\theta_1 \theta_2 \theta_3 \theta_4 \theta_5 \theta_6]^T$, $\dot{\theta}$ and $\ddot{\theta}$ denote the vector of angular positions, velocities and accelerations of motor axes, respectively. Here $N_v = N^{-1}$ is the gear transmissions ratio matrix, and N is a matrix of dimension 6×6 . For the robot KUKA KR500 MT-2, N is not a diagonal matrix, there is also a coupling among axes 4, 5 and 6. The non-null elements are presented in Appendix. $D(q)$ is the symmetric, uniformly positive definite and bounded inertia matrix of the robot. I_a is the inertia matrix of the motor. $H(q, \dot{q})$ represents the contribution due to centrifugal, Coriolis and gravitational forces and the gas accumulator of axis two. B_m and B_s are the viscous friction coefficient matrices of the motor and joint axes respectively. F_m and F_s are the matrices of Coulomb friction of the motor and joint axes.

Robots have two main sources of flexibilities: the flexibilities of body/arms, and those located at joints (which include those of motors and transmissions). In this study, links of robot are considered as rigid, only the flexibilities localized at gearboxes are taken into account and represented by a rigidity matrix K :

$$\Gamma = K(N_v\theta - q) \quad (5)$$

where $\theta_l = N_v\theta$ is the vector of angular positions after gear reduction (see Fig. 2).

B. Modeling of FSW process

FSW is commonly known as a solid state welding process, which gives the possibility to weld almost all types of aluminum alloys, even for some alloys that classified as non-weldable materials by fusion welding [18]. The advantage of

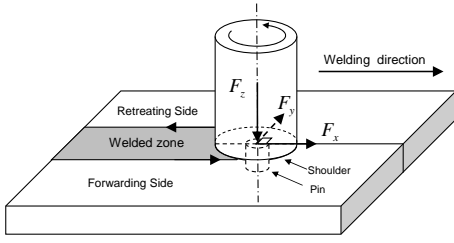


Fig. 3. Friction Stir Welding Model.

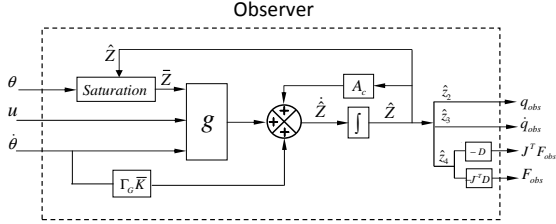


Fig. 4. Diagram of the observer

this process is to avoid those problems encountered in classical welding by melting the metals. It is for this reason that FSW process has been implemented, primarily in transportation industry where aluminum is used to reduce the weight of mechanical structures [2], [19]. Up to now, this process has been carried out by some specially developed machine-tools, which are expensive and have smaller workspace compared with robot manipulators.

III. OBSERVER DESIGN

FSW needs reliable force control and tracking performance under a significant axial force. This problem can be solved if the state of the links (q, \dot{q}) and external forces are known. Unfortunately, only state and current of motor axes and axial force (F_z) are measured by our robot. Therefore, an observer is proposed in this section to solve this problem.

Disturbance observer is a widely used technique in control for improving the performance of disturbance rejection [10]. The unknown input observer (UIO) method is one of the most well-known approach to estimate states [20]. The proposed observer is based on a non-linear observer introduced in [11], which reconstructs articular positions and velocities of links with the ones measured from motor axes. This observer is then modified in order to get also an estimation of efforts by adding more state variables function of forces. In this paper, the observer proposed in [12] has been improved to obtain a better performance in estimating external forces, the block diagram is presented Fig. 4, and it is then implemented into a KUKA robot for experimental validation.

If the state variables x_i is defined as $x_1 = q = [q_1 \ q_2 \ q_3 \ q_4 \ q_5 \ q_6]^T$, $x_2 = \dot{q} = [\dot{q}_1 \ \dot{q}_2 \ \dot{q}_3 \ \dot{q}_4 \ \dot{q}_5 \ \dot{q}_6]^T$, $x_3 = \theta = [\theta_1 \ \theta_2 \ \theta_3 \ \theta_4 \ \theta_5 \ \theta_6]^T$, $x_4 = \dot{\theta} = [\dot{\theta}_1 \ \dot{\theta}_2 \ \dot{\theta}_3 \ \dot{\theta}_4 \ \dot{\theta}_5 \ \dot{\theta}_6]^T$, then following state space model can be obtained:

$$\begin{cases} \dot{x}_1 = x_2 \\ \dot{x}_2 = \ddot{q} \\ = D(q)^{-1}[\Gamma - H(q, \dot{q}) - F_{robot}(\dot{q}) - J^T(q)F] \\ \dot{x}_3 = x_4 \\ \dot{x}_4 = \ddot{\theta} = I_a^{-1}[\Gamma_m - N^T \Gamma - F_{motor}(\dot{\theta})] \end{cases} \quad (6)$$

Then, measured variables are now denoted as y , the following change of coordinates is considered:

$$\begin{cases} z_1 = [I_a^{-1} N^T K]^{-1} x_4 = K^{-1} N^T I_a x_4 \\ z_2 = x_1 = q \\ z_3 = x_2 = \dot{q} \\ z_4 = -D^{-1}(z_2) J^T(z_2) F \\ y_1 = x_3 = \theta \\ y_2 = x_4 = \dot{\theta} \end{cases} \quad (7)$$

Moreover, if $u = \Gamma_m$ then:

$$\begin{cases} \dot{z}_1 = z_2 + K^{-1} N^T [u - F_{motor}(y_2)] - N_v y_1 \\ \dot{z}_2 = z_3 \\ \dot{z}_3 = \ddot{q} = z_4 + \psi(z_2, z_3, y_1) \\ \dot{z}_4 = -\frac{d}{dt}[D^{-1}(z_2) J^T(z_2) F] \end{cases} \quad (8)$$

where ψ is equal to:

$$\psi = D(z_2)^{-1} [K(N_v y_1 - z_2) - H(z_2, z_3) - F_{robot}(z_3)] \quad (9)$$

If A and C are defined as following (I is the 6 order identity matrix and 0 is the 6×6 zero matrix):

$$A = \begin{pmatrix} 0 & I & 0 & 0 \\ 0 & 0 & I & 0 \\ 0 & 0 & 0 & I \\ 0 & 0 & 0 & 0 \end{pmatrix} \text{ and } C = (I \ 0 \ 0 \ 0) \quad (10)$$

then:

$$\dot{z} = Az + g(z, y, u) + d(z, F, \dot{F}) \quad (11)$$

with

$$g = \begin{cases} K^{-1} N^T [u - F_{motor}(y_2)] - N_v y_1 \\ 0 \\ \psi(z_2, z_3, y_1) \\ 0 \end{cases} \quad (12)$$

and $d(z, F, \dot{F}) = [0 \ 0 \ 0 \ -\frac{d}{dt}[D^{-1}(z_2) J^T(z_2) F]]^T$.

This non-linear observer is an improved version of the one described in [12]. The measured input y_1 and y_2 are now θ and $\dot{\theta}$, z_4 are here represent an additional acceleration which enables the additional acceleration ψ not to be a function of unknown disturbance external forces. Define now the following high gains matrix, with G a constant ≥ 1 :

$$\Gamma_G = \begin{pmatrix} GI & 0 & 0 & 0 \\ 0 & G^2 I & 0 & 0 \\ 0 & 0 & G^3 I & 0 \\ 0 & 0 & 0 & G^4 I \end{pmatrix} \quad (13)$$

and matrix L such as $(A - LC)$ has all its eigenvalues in the left half of the complex plane, then a new observer is proposed as follow:

$$\dot{\hat{z}} = (A - \Gamma_G LC) \hat{z} + g(\hat{z}, y, u) + \Gamma_G \bar{K} y_2 \quad (14)$$

where $\bar{K} = LK^{-1} N^T I_a$ and:

$$\begin{cases} \bar{z}_2 = y_1 - \frac{y_1 - \hat{z}_2}{\|y_1 - \hat{z}_2\|} N_s \text{sat}\left(\frac{\|y_1 - \hat{z}_2\|}{N_s}\right) \\ \bar{z}_3 = \frac{\hat{z}_3}{\|\hat{z}_3\|} M_s \text{sat}\left(\frac{\|\hat{z}_3\|}{M_s}\right) \\ \bar{z}_4 = \frac{\hat{z}_4}{\|\hat{z}_4\|} A_s \text{sat}\left(\frac{\|\hat{z}_4\|}{A_s}\right) \end{cases} \quad (15)$$

with the saturation function:

$$\text{sat}(x) = \begin{cases} x & \text{if } |x| \leq 1 \\ 1 & \text{if } |x| > 1 \end{cases} \quad (16)$$

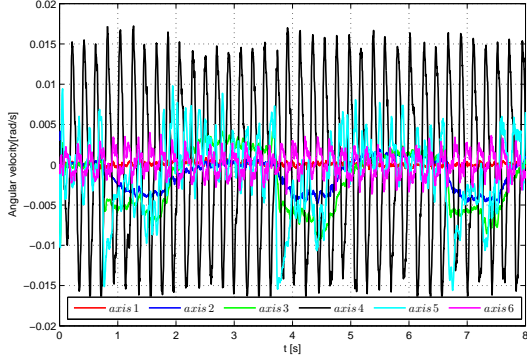


Fig. 5. Estimate error of angular velocity.

and M_s , N_s , F_M , F_d , J_M , D_M and A_s are known positive physical constant bounds:

$$\left\{ \begin{array}{l} \|x_2\| < M_s \\ \|x_1 - x_3\| < N_s \\ \|F\| < F_M \\ \|\dot{F}\| < F_d \\ \|J^T(z_2)\| < J_M \\ \|D^{-1}(z_2)\| < D_M \\ A_s = D_M J_M F_M \end{array} \right. \quad (17)$$

Fig. 4 shows the diagram of the proposed observer where $A_c = A - \Gamma_C LC$. For only one axis, $L = [L_1 \ L_2 \ L_3 \ L_4]^T$ and:

$$\det[\lambda I - (A - LC)] = \lambda^4 + L_1 \lambda^3 + L_2 \lambda^2 + L_3 \lambda + L_4 \quad (18)$$

where λ is an eigenvalue of matrix $A - LC$. A possible choice for L is then: $L_1 = 4a$, $L_2 = 6a^2$, $L_3 = 4a^3$ and $L_4 = a^4$. In this case, matrix $A - LC$ has four stable eigenvalues in $\lambda = -a$, where a is a positive real fixing the dynamics of the proposed observer.

The estimation error $e = z - \hat{z}$ satisfies the following differential equation:

$$\dot{e} = A_c e + g(z, y, u) - g(\hat{z}, y, u) + d(z, F, \dot{F}) \quad (19)$$

Because of the form of disturbance $d(z, F, \dot{F})$ the following stability theorem can be proven for the proposed observer:

Theorem 1: There exists a constant G^0 such that error $e(t)$ is bounded for any gain $G > G^0$.

The proof is similar to one described in [12], as $\|\frac{d}{dt}[D^{-1}(z_2)J^T(z_2)F]\|^T$ is bounded since \dot{z}_2 , F , \dot{F} are bounded (see equation (17)) and $\frac{\partial D^{-1}(z_2)}{\partial z_2}$ and $\frac{\partial J^T(z_2)}{\partial z_2}$ are also bounded as they are only functions of sines and cosines.

IV. EXPERIMENTAL VALIDATION

A. Test 1: Validation of proposed observer during diving phase of FSW process

On the first step, the observer is validated only with measured data. FSW process can be divided into three phases: diving, welding and removing the tool. During experiment, the robot is programmed to press on a work-piece, then the tool will enter the material step by step with a force (F_z) equalling

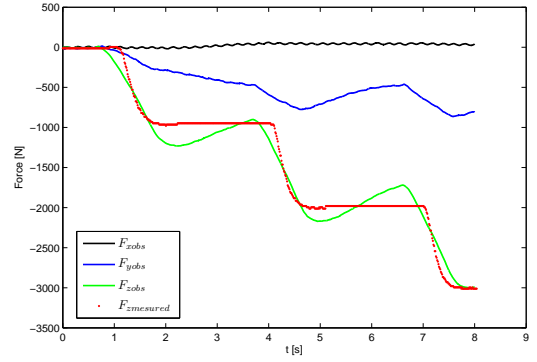


Fig. 6. Comparison between measured force and estimated force.

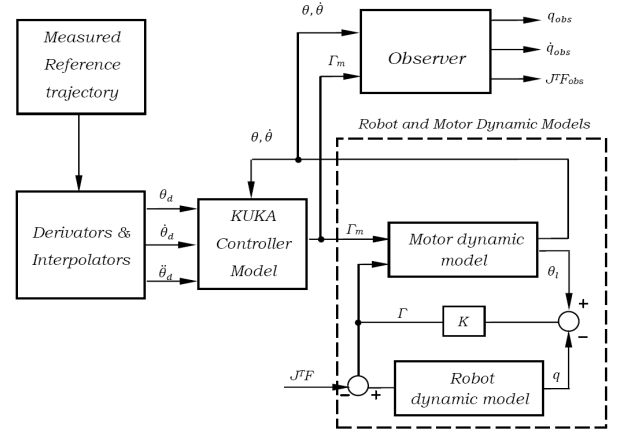


Fig. 7. Block diagram for validation of force building in the case of a complex trajectory of robot KUKA KR500 MT-2.

1000 N, 2000 N and 3000 N, just like the diving phase of FSW process as shown in Fig. 1. Meanwhile, state of rotor (θ , $\dot{\theta}$), current of each motor (I) and the axial force $F_{z_{measured}}$ are measured with the Scope and function monitor FTCtrlMonitor of the robot controller. After that, the state and current are used off line as input of the observer. The observer should reconstruct the state of link (q_{obs} , \dot{q}_{obs}) and the external forces ($F_{x_{obs}}$, $F_{y_{obs}}$, $F_{z_{obs}}$), as shown in Fig. 4. In this test, we have chosen tuning parameters of the observer $G = 1$, $a = 25$ for the first three axes and $a = 50$ for the other axes. Moreover, the lateral forces in direction x and y are also estimated, which improves operation performance as it is these lateral forces that prevent the robot to weld a straight line during FSW process.

Fig. 5 shows the error of reconstructed angular speeds ($\dot{q}_{obs} - \dot{\theta}_l$), as $\dot{\theta}_l$ is angular velocities after reduction gearbox. As mentioned before, the tool is in contact with work-piece at the beginning. During this experiment, only the axes of motor can have a little movement while applying a force in z direction, links of robot should rarely move. Fig. 6 presents the estimated forces and the measured force $F_{z_{measured}}$ on direction z of the tool frame, since the robot only has axial force sensor. The $F_{z_{obs}}$ matches well with the $F_{z_{measured}}$, and the observer has also reconstructed other forces $F_{x_{obs}}$ and $F_{y_{obs}}$. Here, $F_{y_{obs}}$ might be caused by friction.

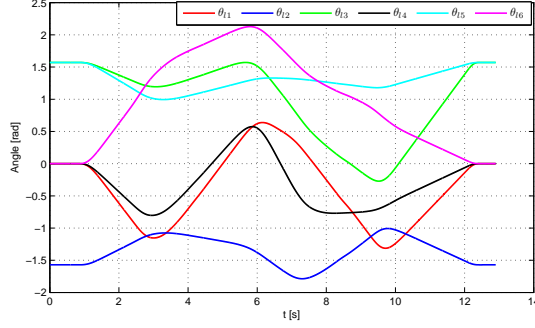


Fig. 8. Robot KUKA KR500 MT-2 measured reference angle displacements.

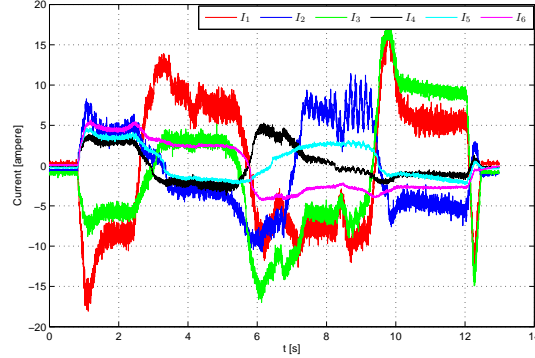


Fig. 9. Robot KUKA KR500 MT-2 measured currents.

B. Test 2: Validation of observer in the case of a complete trajectory

On the second step, the robot is programmed to move along a large trajectory in its workspace. Fig. 8 and Fig. 9 present the measured angular displacements and currents on each motor axis. Then, the desired displacement, speed and acceleration measurements fed a simulation model of robot KUKA KR500 MT-2 disturbed by an external force, as shown in Fig. 7. From $t = 4s$, an external force of $F_z = 1000$ N is added to the robot system model. The reconstructed state of links (q_{obs} , \dot{q}_{obs}) and external forces (F_{xobs} , F_{yobs} , F_{zobs}) are compared with the measured state of motor axes (θ_l , $\dot{\theta}_l$) and the added forces to verify and validate the proposed observer. The results show a good performance in angular position, velocity and external force estimations as shown in Fig. 11 with a precision of $10^{-7}rad$ for positions and $10^{-5}rad/s$ for velocities. Fig. 10 shows the torque due to the added external force on each axis, which can reach about 1400 Nm on axis 2. If we defined $\chi = J^T F - (J^T F)_{obs}$, then the relative mean square error can be calculated by:

$$RMSE = \chi_{rms} / (J^T F)_{rms} \quad (20)$$

where χ_{rms} and $(J^T F)_{rms}$ are the root mean square value of χ and $J^T F$ respectively. The $RMSE$ of axes 2, 3 and 5 are equal to: $RMSE_2 = 0.79\%$, $RMSE_3 = 0.83\%$, $RMSE_5 = 0.37\%$.

The identified inertia parameters have good precisions, but here, in order to analyse the sensitivity of the proposed observer, two simulations have been carried out with an additional error of $\pm 10\%$ of inertia parameters (see Fig. 12

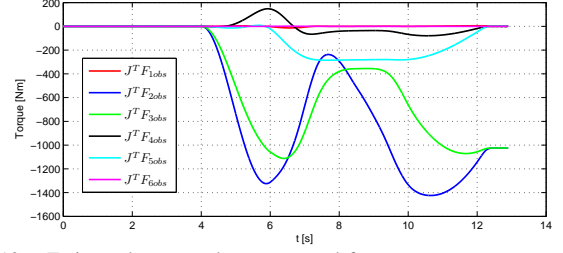


Fig. 10. Estimated torques due to external force.

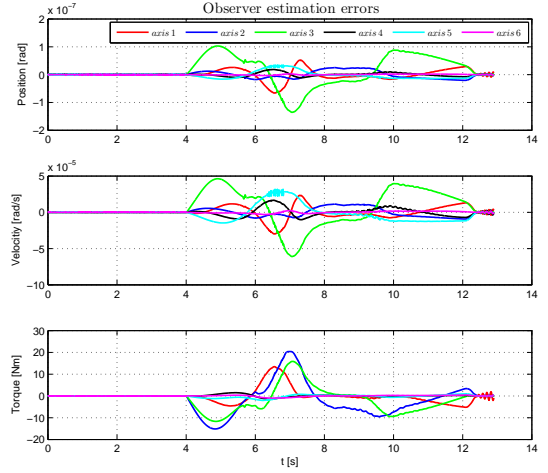


Fig. 11. Observer error of angular positions $q - \hat{q}$, velocities $\dot{q} - \hat{\dot{q}}$ and torques $J^T F - (J^T F)_{obs}$

and Fig. 13). The estimations appear to be stable and quite accurate in spite of the error of inertia.

V. CONCLUSIONS

In this paper, a non-linear disturbance observer is proposed for flexible-joint industrial robots and a stability theorem has been introduced to prove the boundedness of observer estimation errors. A flexible model of the concerned KUKA robot has been developed, with precise identification parameters. A series of experimental validation tests demonstrates that the proposed observer is fast enough to estimate the system state with required accuracy and sensitivity, and better performance than the one proposed in [12]. Even under noises of measurement, this observer still provides satisfactory results in both state and external force estimations.

More precisely, in FSW diving phase, the estimated axial force matches well with the measured force. This method can also be applied to other robots and processes. For instance, in our laboratory, numerous experiments have been implemented to identify all the necessary parameters of KUKA KR500 MT-2. With more precise robot identification, the performance of observer can also be improved. Using both state of the rotor axes and the estimated state of robot links in the control of flexible robots can lead to more stable and robust feedback control as shown in [12], [17]. Moreover, the reconstructed external forces can reduce the error on the work-piece. Next step consists now to implement some experiments on-line with industrial robots, and use the estimated lateral force to suppress lateral deviation observed in FSW process.

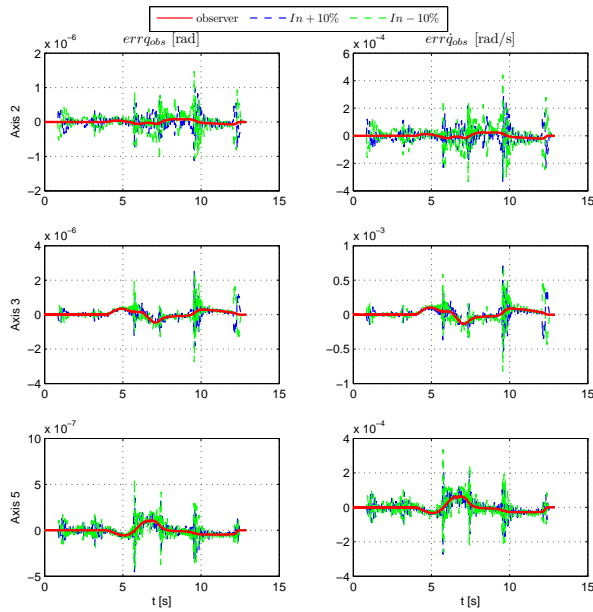


Fig. 12. Comparison of estimation error of \hat{q} and $\hat{\dot{q}}$ with $\pm 10\%$ error of Inertia parameters.

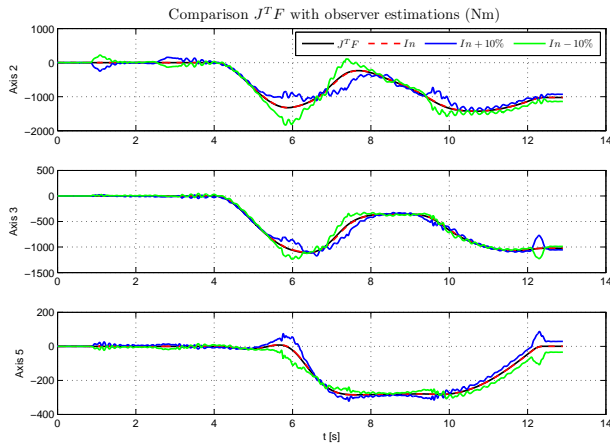


Fig. 13. Comparison of $J^T F$ estimation error with $\pm 10\%$ error of Inertia parameters.

APPENDIX

ACKNOWLEDGMENT

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REFERENCES

- [1] S. Zimmer, L. Langlois, J. Laye, and R. Bigot, "Experimental investigation of the influence of the fsw plunge processing parameters on the maximum generated force and torque," *Int. Journal of Advanced Manufacturing Technology*, vol. 47, no. 1-4, pp. 201–215, 2010.
- [2] R. S. Mishra and Z. Y. Ma, "Friction stir welding and processing," *Materials Science and Engineering, Reports*, vol. 50, pp. 1–78, 2005.
- [3] G. Besançon, *Nonlinear Observers and Applications*, 1st ed., G. Besançon, Ed. Berlin Heidelberg: Springer, 2007.

TABLE II. NUMERICAL VALUES OF ROBOT KUKA KR500 MT-2

$N(i, j)$	Link length	(m)	Rigidity	(Nm/rad)	
N_{11}	469.375	L_{1x}	1.045	K_1	$6.61 \cdot 10^6$
N_{22}	469.375	L_{1z}	0.500	K_2	$7.16 \cdot 10^6$
N_{33}	-504.770	L_2	1.300	K_3	$3.08 \cdot 10^6$
N_{44}	-260.619	L_{34}	1.025	K_4	$0.56 \cdot 10^6$
N_{55}	-251.977	D_4	-0.055	K_5	$0.66 \cdot 10^6$
N_{66}	164.570	L_5	0.290	K_6	$0.47 \cdot 10^6$
N_{54}	-1.0964	L_{tz}	0.350		
N_{64}	-1.5836	L_{ty}	0		
N_{65}	1.5311				

- [4] S. E. Talole, J. P. Kolhe, and S. B. Phadke, "Extended-state-observer-based control of flexible-joint system with experimental validation," *IEEE Transactions on Industrial Electronics*, vol. 57, no. 4, pp. 1411–1419, 2010.
- [5] A. De Luca, D. Schröder, and M. Thümmel, "An acceleration-based state observer for robot manipulators with elastic joints," in *IEEE International Conference on Robotics and Automation*, Roma, Italy, April 2007, pp. 3817–3823.
- [6] R. Henriksson, M. Norrlöf, S. Moberg, E. Wernholt, and T. B. Schön, "Experimental comparison of observers for tool position estimation of industrial robots," in *Proceedings of the IEEE Conference on Decision and Control*, 2009, pp. 8065–8070.
- [7] C. Kravaris, V. Sotiropoulos, C. Georgiou, N. Kazantzis, M. Q. Xiao, and A. J. Krener, "Nonlinear observer design for state and disturbance estimation," *Systems Control Letters*, vol. 56, no. 11-12, pp. 730–735, 2007.
- [8] T. A. Davis, Y. C. Shin, and B. Yao, "Observer-based adaptive robust control of friction stir welding axial force," *IEEE/ASME Transactions on Mechatronics*, vol. 16, no. 6, pp. 1032–1039, 2011.
- [9] B. Yao and L. Xu, "Observer-based adaptive robust control of a class of nonlinear systems with dynamic uncertainties," *International Journal of Robust and Nonlinear Control*, vol. 11, no. 4, pp. 335–356, 2001.
- [10] S. K. Park and S. H. Lee, "Disturbance observer based robust control for industrial robots with flexible joints," in *International Conference on Control, Automation and Systems 2007*. Seoul, Korea: ICCAS '07, December 2007, pp. 584 – 589.
- [11] M. Jankovic, "Observer based control for elastic joint robots," *IEEE Trans. on Robotics and Automation*, vol. 11, no. 4, pp. 618–623, 1995.
- [12] J. Qin, F. Léonard, and G. Abba, "Non-linear observer-based control of flexible-joint manipulators used in machine processing," in *Proceedings of The ASME 2012 11th Biennial Conference on Engineering Systems Design and Analysis*, no. 82048, Nantes, France, July 2012.
- [13] W. Khalil and E. Dombre, *Modeling, Identification and Control of Robots*, K. P. S. Paper, Ed. Oxford: Elsevier Ltd, 2004.
- [14] *SYMORO+ Symbolic Modeling of Robots, User's Guide*.
- [15] W. Khalil and D. Creusot, "Symoro+: A system for the symbolic modelling of robots," *Robotica*, vol. 15, pp. 153–161, 1997.
- [16] M. W. Spong, "Modeling and control of elastic joint robots," *Journal of Dynamic Systems, Measurement, and Control*, vol. 109, no. 4, pp. 310–318, 1987.
- [17] M. W. Spong, S. Hutchinson, and M. Vidyasagar, *Robot Modeling and Control*, M. Spong, S. Hutchinson, and M. Vidyasagar, Eds. Berlin Heidelberg: John Wiley and Sons, Inc., 2005.
- [18] R. Nandan, T. DebRoy, and H. Bhadeshia, "Recent advances in friction-stir welding - process, weldment structure and properties," *Progress in Materials Science*, vol. 53, no. 6, pp. 980–1023, 2008.
- [19] X. Zhao, P. Kalya, R. G. Landers, and K. Krishnamurthy, "Empirical dynamic modeling of friction stir welding processes," *Journal of Manufacturing Science and Engineering, Transactions of the ASME*, vol. 131, no. 2, pp. 1–9, 2009.
- [20] X. Yue, D. Vilathgamuwa, and K.-J. Tseng, "Robust adaptive control of a three-axis motion simulator with state observers," *IEEE/ASME Transactions on Mechatronics*, vol. 10, no. 4, pp. 437–448, 2005.