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# Effect of Nano-Peening Surface Texturing on Self-Cleaning Function

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## ABSTRACT:

Surface texturation at micro- and meso-scales plays an important role in applications where cosmetic, aesthetic and self-cleaning functionalities are specified. This research paper deals with a multiscale surface, in which texturing and texture have a larger influence because they are scaled differently. The experimental approach highlights the important effect of texture and texturing on the anti-fingerprinting performance rated in term of surface wettability. We examine first, in detail, the wetting response of surfaces textured on aluminum alloy 6063 plates using nano-peening with various processing parameters. Roughness was measured by atomic force microscopy (AFM) and interferometry. Surface wettability was quantified using the sessile drop method. The calculation takes into account the wetting behavior of the textured surfaces at different scales. Correlations were made between the surface roughness and its functionality.

## 1. INTRODUCTION

Nano peening processes are applied to materials for manufacturing functional surfaces. The process consists in impacting the surface of a component by multiple high velocity shots that induce plastic deformation on the surface layer and subsequently affecting the surface properties such as its wettability [1]. The self-cleaning and Anti-Fingerprint (AF) functions are often demanded today for engineered surfaces. These surfaces are amphiphobic surfaces that possess

non-wetting behavior simultaneously against water (hydrophobicity) and fats (oleophobicity) [2]. Amphiphobic properties are achievable by specific chemical composition and topography design, such as lowering surface free energies [3][4][5] and designing functional surface textures [6][7][8].

From a thermodynamic point of view, the solid-liquid system, free of any chemical reaction, tends to minimize its free energy via physical interactions and bonding formation [9]. Lowering the solid surface energy enhances the hydrophobicity. However a specific roughness is required for achieving superhydrophobic surfaces [10][11][12][13][14][15][16][17][18][19]. A designed roughness affects the surface wettability by changing the solid-liquid contact line geometry or the quantity of air trapped in the asperities underneath the liquid drop (air-solid composite surface) [9][20]. Hierarchical surfaces with nano, micro, and macro multi-scale structures are in particular relevant for achieving liquid repellent properties [21][22]. The surface structure [23][24] and roughness [25][26][27] are important for producing non-wetting behaviors. The evaluation of the fingerprint properties is usually restricted to the surface wettability against water, hexadecane, oleic acid [2] and artificial fingerprint liquid [28].

Sand blasting [29][30], surface mechanical attrition treatment (SMAT) [1], and shot peening [31] are currently used for modifying the wettability of metal surfaces by controlled generation of specific roughness and texture profiles. A rough and hydrophilic surface is created by deforming the surface by particle impacts. Nevertheless, the correlation between the process parameters and the induced wetting properties remains not well defined.

The present work investigated the anti-fingerprint properties of aluminum surfaces manufactured using various nano-peening process parameters. These parameters being confidential, the surfaces were characterized by roughness measurements and electronic microscopy observations. Their wettability was measured with the sessile drop method using two known liquids and compared to the polished aluminum as prior to peening performance.

## 2. THEORETICAL BACKGROUND

### 2.1. Roughness Characterization

The deformed nano-peened surfaces can be described quantitatively using the common roughness criteria [32]. The heights  $Y_i$  of the profile at each position  $(x,y)$  are calculated relatively to the nominal shape of the surface. The arithmetic mean deviation of the assessed profil  $S_a$  is the most used parameter:

$$S_a = \frac{1}{N} (\sum_{i=1}^N |Y_i|) \quad (\text{Eq.1})$$

However, a single roughness value may not be enough informative to describe the topography of a surface. Thus additional parameters should be used.

In order to study the symmetry and peakedness of the profiles, two parameters of skewness ( $S_{sk}$ ) and kurtosis ( $S_{ku}$ ) have been defined. Skewness is a measure of the symmetry of the curve describing the height distribution. A profile with a majority of valleys has negative skewness. A symmetrical height distribution with as many peaks as valleys has zero skewness. The numerical formula used to calculate is as follow:

$$S_{sk} = \frac{1}{NS_q^3} (\sum_{i=1}^N Y_i^3) \quad (\text{Eq.2})$$

, where  $S_q$  is the root mean square (RMS) of a profile composed of  $N$  points of height  $Y_i$ .

$$S_q = \sqrt{\frac{1}{N} (\sum_{i=1}^N Y_i^2)} \quad (\text{Eq.3})$$

Kurtosis parameter  $S_{ku}$  represents the peakedness of a profile. A surface with a narrow height distribution has a kurtosis value greater than 3, while a surface that has a well spread out height distribution has a kurtosis value of less than 3. A surface with a Gaussian height distribution has a kurtosis value of 3. The kurtosis parameter is calculated by:

$$S_{ku} = \frac{1}{NR_q^4} (\sum_{i=1}^N Y_i^4) \quad (\text{Eq.4})$$

Finally the roughness parameter  $S_{dr}$  characterizing the developed interfacial area ratio is estimated as the ratio of the real ( $A_{real}$ ) to projected ( $A_{proj}$ ) surface areas:

$$S_{dr} = \frac{A_{real}}{A_{proj}} - 1 \quad (\text{Eq.5})$$

Surface irregularities induced by nano-peening process are formed by intersections of the craters generated by each single impact. Although the shot impacts are random during the process, observations have revealed that for high surface coverage, the shot impacts are distributed on the treated surface in a relatively regular manner. Accordingly the mentioned standard roughness parameters are appropriate to characterize the surface topography of nano-peened specimens.

## 2.2. Wettability Measurement

The wettability of a surface by a liquid in a gaseous environment results in part from the interactions between the gas, liquid and solid surface energies. Among the numerous methods existing to characterized wettability [33][34], the sessile drop method is well adapted to the characterization of the wetting properties of solid surfaces by known liquids. Measurements of liquid advancing or receding angles are acquired by imaging a liquid drop placed on a flat, unwetted solid surface. Historically analyzed using the Laplace equation and the Bashforth-Adams tables [33], the norm AFNOR EN 828 [35] proposes the use of various known liquids to deduce the solid surface energy. The analysis is founded on the Young-Dupré equation for a perfectly flat homogeneous solid surface wetted by a liquid drop. The measured contact angle  $\theta$  results from the three interfacial energies in mechanical equilibrium:

$$\sigma_{SV} = \sigma_{LS} + \sigma_{LV} \cos \theta \quad (\text{Eq.6})$$

, where  $\sigma_{SV}$  et  $\sigma_{LS}$  are the solid-vapor and liquid-vapor superficial tensions, respectively. A practical disadvantage of Young's equation is that it contain only two readily measurable quantities : the contact angle  $\theta$  and the liquid vapor surface tension  $\sigma_{LV}$ .

Several semi-empirical approaches have been developed to calculate the solid surface tension. The most popular is the approach developed by Owens and Wendt [35]. They extended Fowkes' concept of surface tension components by dividing the total surface energy into two components, a dispersion force component and a hydrogen bonding component. The latter component consists of both hydrogen bonding and dipole-dipole interactions. Implementing the polar (subscript  $P$ ) and dispersed (subscript  $D$ ) components of the surface tensions  $\sigma_{SV}$  and  $\sigma_{LS}$  into Eq. 6 leads to [35]:

$$\frac{(1+\cos\theta)\cdot\sigma_{LV}}{2\sqrt{\sigma_{LV}^D}} = \sqrt{\sigma_{SV}^P} \cdot \sqrt{\frac{\sigma_{LV}^P}{\sigma_{LV}^D}} + \sqrt{\sigma_{SV}^D} \quad (\text{Eq.7})$$

, where  $\theta$  is the contact angle for a given liquid drop. Linear best-fitting of  $\frac{(1+\cos\theta)\cdot\sigma_{LV}}{2\sqrt{\sigma_{LV}^D}}$  versus

$\sqrt{\frac{\sigma_{LV}^P}{\sigma_{LV}^D}}$  estimates the polar  $\sigma_{SV}^P$  (slope) and dispersed  $\sigma_{SV}^D$  (residue) components. In this approach, the contact angles of at least two liquids with known surface energy components, such as deionized water and glycerol, are required in order to calculate the dispersive and polar components of the solid surface energy.

### 2.3. Wettability of Rough Surfaces

The wettability of a solid surface is partly controlled by its roughness, as indicated in reviews on the subject [36][37][9][38][39]. A theoretical model proposed by Wenzel describes the contact angle  $\theta^*$  on a wetted solid surface with a roughness parameter  $S_{dr}$  [40]:

$$\cos \theta^* = S_{dr} \cdot \cos \theta \quad (\text{Eq.8})$$

, where  $\theta$  is the contact angle on a flat homogeneous surface of a solid with same composition. As  $S_{dr}$  is always positive, the surface roughness increases hydrophobicity and hydrophilicity of hydrophobic and hydrophilic surfaces, respectively, by increasing the liquid-solid contact area [31]. Apparent contact angles for full liquid intrusion into the pattern cavities are calculated using the Wenzel model:

$$\cos\theta^* = 1 + \phi_S(\cos\theta - 1) \quad (\text{Eq.9})$$

In opposite, the Cassie-Baxter model describes the wetting of rough surfaces with entrapped air below the drop, i.e. unwetted vales [41]. The Cassie-to-Wenzel wetting transition has been observed by enforcing the liquid into the solid asperities [42]. The Cassie-Baxter equation estimates the apparent contact angle  $\theta^*$  of a wetting liquid on a composite air-solid surface composed by a fraction  $f_1$  and  $f_2$  of contact surface ( $f_1+f_2=1$ ) with contact angles of  $\theta_1$  and  $\theta_2$ , respectively [41]:

$$\cos\theta^* = f_1 \cos\theta_1 + f_2 \cos\theta_2 \quad (\text{Eq.10})$$

Implementing into Eq.10 the solid fraction area  $\phi_S$  and air trapped fraction  $1 - \phi_S$  underneath the droplet, and the contact angles  $\theta$  on a flat homogeneous solid surface and  $\pi$  on air [43], the Cassie-Baxter equation is modified as:

$$\cos\theta^* = -1 + \phi_S(\cos\theta + 1) \quad (\text{Eq.11})$$

The Wenzel-to-Cassie-Baxter transition is related in part to topographic limits for a liquid to penetrate into the asperities.

### 3. EXPERIMENTAL METHODS

#### 3.1. Material

Samples were prepared from aluminum alloy 6063 plate (AlMg0.7Si) with dimensions of 50 x 50 x 0.7 mm<sup>3</sup>. All samples were polished prior to the nano-peening treatment to obtain smooth surfaces with a hydrophobic property. The as-polished sample is referred to as *S0*. Various

peening parameters were used to obtain 15 different nano-peened surfaces. Surfaces can be classified according to Table 1.

**Table 1:** process parameters for peening process.

Sample	Al plate preparation	Peening Pressure	Shot Material	Shot Surface Finishing	Shot Size
S0	polished	-	-	-	-
SA-1	polished	Low	ceramic	SF1	Small
SA-2	polished	Medium	ceramic	SF1	Small
SA-3	polished	High	ceramic	SF1	Small
SB-1	polished	Low	ceramic	SF2	Large
SB-2	polished	Medium	ceramic	SF2	Large
SB-3	polished	High	ceramic	SF2	Large
SC-1	Not polished	Low	metallic	SF1	Small
SC-2	Not polished	Medium	metallic	SF1	Small
SC-3	Not polished	High	metallic	SF1	Small
SD-1	polished	Low	metallic	SF1	Small
SD-2	polished	Medium	metallic	SF1	Small
SD-3	polished	High	metallic	SF1	Small
SE-1	polished	Low	metallic	SF2	Medium
SE-2	polished	Medium	metallic	SF2	Medium
SE-3	polished	High	metallic	SF2	Medium

### 3.2. Electronic Microscopy Observation Procedure

Observation of surfaces was performed using the JEOL 7001F LV microscope equipped with SEM and EDS. Observations (SEM) and composition analysis (EDS) were performed in  $2 \cdot 10^{-3}$  Pa vacuum at 15.0 kV accelerating voltage and 10.0 mm working distance

### 3.3. Roughness Measurement Procedure

A three-dimensional analysis was undertaken to assess the surface roughness induced by nano-peening. A white light interferometer, WYKO 3300 NT (WLI), sampled a representative surface

topography area of 640x480 points with the same step scale of 1.94  $\mu\text{m}$  in the -x and -y directions (the surface size is therefore 1.2 mm x 0.93 mm). The form component is removed from the acquired 3D data using least square method based on a cubic spline function [44]. In addition, AFM measurements were performed over a 100 x 100  $\mu\text{m}^2$  surface with a 512x512 points resolution.

### 3.4. Wettability Testing Procedure

Contact angles were measured in the Morphoscan apparatus from Michalex Tribometrix using the sessile drop method according to the norm AFNOR EN 828 [35]. Three surface cleaning conditions performed just prior to the measurements were investigated: cleaning with ethanol only (C1), ultrasonic cleaning in ethanol followed by air blow drying (C2), and ultrasonic cleaning in ethanol followed by air blow drying after ageing 6 months in ambient air (C3). Drops were deposited in an environment of  $22 \pm 1$  °C temperature and  $54 \pm 2$  % relative humidity.

Two liquids, deionized water and glycerol, were used with characteristics given in Table 2. Inside a temperature-controlled chamber, a CCD video camera imaged deposited sessile drops on the solid surface using a syringe of inside diameter of 4.6 mm equipped with a needle of 0.8 mm outside diameter were used to control the amount of liquid deposited on the surface. 6  $\mu\text{L}$  droplets were deposited on nano-peened surfaces. The capillary length  $K$  (Table 1) is given by [40]:

$$K = \sqrt{\frac{\gamma}{\rho g}} \quad (12)$$

, where  $\gamma$  is liquid superficial tension,  $\rho$  liquid density,  $g$  gravitational acceleration. The droplets had radii of  $1.5 \pm 0.5$  mm, smaller than the capillary length (Table 2), so that gravity can be considered negligible.

The static droplet shape on sample's surface was recorded ten seconds after the drop deposition as a 720x480 pixels image. Advancing contact angles were measured to an accuracy of  $\pm 0.5^\circ$  using a home-developed program (Figure 1). Ten droplets of each liquid were deposited at different

locations on the surface of each sample to obtain a mean value of the contact angles. Left and right angles were used to determine the reported surface energy.

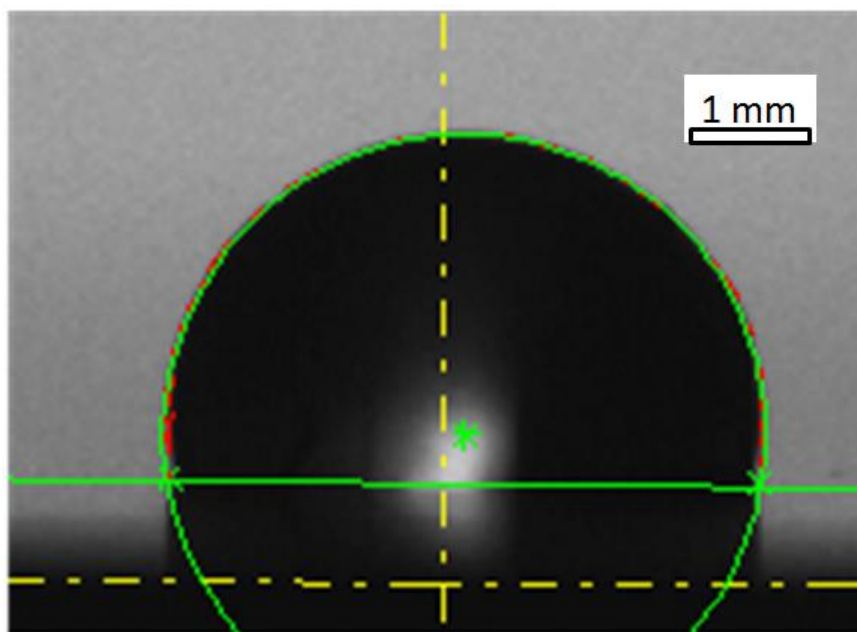


Figure 1: photograph of drop with superimposed profile used for contact angle calculation

Table 2: surface tensions of liquids used [35].

Liquid	Superficial Tension $\gamma$ mN·m <sup>-1</sup>	Dispersed Component $\gamma^d$ mN·m <sup>-1</sup>	Polar Component $\gamma^p$ mN·m <sup>-1</sup>	Density (kg/m <sup>3</sup> )	Capillary Length (m)
deionised water	72.80	21.80	51.00	1000	0.0027
glycerol	63.40	37.00	26.40	1260	0.0023

### 3.5. Multi scale surface roughness characterization of peened surfaces

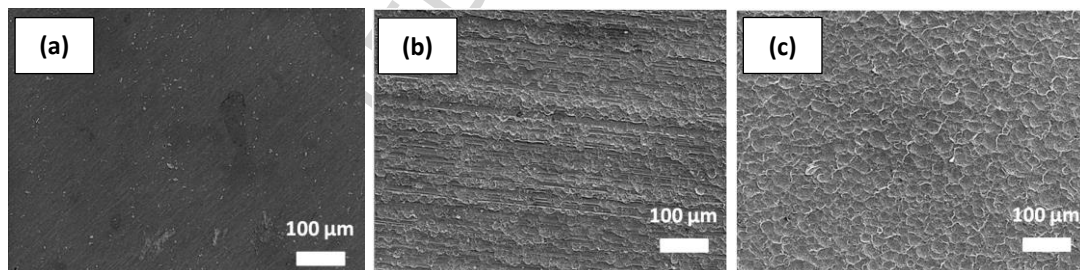
The multi-scale characterization of engineering surfaces describes the surface features and irregularities at various wavelengths that compose the surface. The surface roughness profiles were split into frequency components from  $10^{-3}$  to  $1$  mm<sup>-1</sup> using the continuous wavelets decomposition approach [45]. This decomposition can be considered as a mathematical microscope, where the resolutions are the basic functions obtained from a single wavelet or mother wavelet  $\psi(x)$  by dilation (or compression) and translation. The result of the

decomposition makes it possible to identify the various scales of the topographic signal after a 2D inverse wavelet transformation. The characterization methodology consists then of determining the developed interfacial area ratio parameter  $S_{dr}$  derived from ISO25178 standard at each individual scale from the scales of waviness to roughness [46]. Then, a multiscale spectrum  $MS_{dr}$  of the topographic profile is obtained.

## 4. RESULTS

### 4.1. SEM Observation

Surfaces of  $800 \times 600 \mu\text{m}$  were imaged by SEM for each sample. The initial surface  $S_0$  is smooth from the previous polishing treatment. Figure 2 shows the surface structure of AA6063 after nano-peening using various peening pressures. *Low*-pressure peened specimens (i.e. indexed “1”) showed residual scratches generated by the polishing process prior to peening. On the opposite, *High*-pressure peened specimens indexed “3” strongly modified the surfaces with deep grooves and imprints of the peening balls. A greater nanopeneering pressure yields to more craters on the treated surface. AFM imaging of surface topographies are summarized in the Appendix.



**Figure 2:** SEM observation of surface (a) prior peening ( $S_0$ ) and nano-peened with (b) low (SB-1) and (c) high (SB-3) pressures

### 4.2. Surface roughness

The surface roughness measurements performed by AFM are detailed in Table 3. The reconstructed surfaces from the AFM data are shown in Appendix (Figure A1). The roughness

parameter  $S_a$  which is defined as the average roughness evaluated over the complete 3D measured surface, is significantly increased by the nano-peening treatment. The initial  $S0$  had very low  $S_a$  roughness ( $0.02 \mu\text{m}$ ) in agreement with an as-polished sample. The peening process increased the  $S_a$  roughness values from  $0.020$  up to  $0.874 \mu\text{m}$  with greater values for samples peened with the highest pressure *High*, in agreement with the more deformed surfaces imaged by SEM (recall Figure 1). However,  $S_a$  values decrease at greater peening pressures for the SE specimens. The possible lowering of the roughness at excessive peening has been observed previously on other superficial deforming processes [1][32]. Such trend may be justified by the fact that the first shots impact the target when its surface is entirely smooth. As a consequence local changes cause important roughness increase, while changes induced by further nano-peening would not be evident as those resulting from the first collisions.

In case of skewness and kurtosis parameters, it is observed that both parameters are more or less independent of peening pressures. Most  $S_{sk}$  values are positive, in agreement with the residual spherical imprints of the shots, except for SB-1 and SB-2 possibly due to piling-up of the superficial material during shot impact. Finally most of the nano-peened substrates present a Gaussian distribution of peaks and valleys ( $S_{ku}\approx 3$ ) except SA-2 with a  $S_{ku}$  value near 13.8 because of several high peaks of residual materials.

The parameter  $S_{dr}$  indicated the percentage of additional surface area provided by the texture over a perfectly flat and smooth surface of a same cross-section. The combination of different texture amplitudes and spacings comprising the texture influences the additional surface area provided by the texture. Nano-peened surfaces offer from 4 to 21% additional surface area than the corresponding base material  $S0$ . Increasing the shot pressure from *Low* to *High* increases the surface roughness parameters even though the reason for the high  $S_{dr}$  value for SC-1 at *Low* peening pressure remains unclear. An increase in surface area of hydrophilic materials may enhance the degree of surface wetting by fluids [40].

**Table 3:** 3D roughness parameters

Specimen	S0	SA-1	SA-2	SA-3	SB-1	SB-2	SB-3	SC-1	SC-2	SC-3	SD-1	SD-2	SD-3	SE-1	SE-2	SE-3
<b>Sa (<math>\mu\text{m}</math>)</b>	0.020	0.366	0.623	0.679	0.579	0.848	0.94	0.459	0.538	0.664	0.389	0.509	0.64	0.6	0.874	0.713
<b>Sq (<math>\mu\text{m}</math>)</b>	0.0277	0.454	0.857	0.871	0.779	1.1	1.18	0.588	0.675	0.843	0.484	0.631	0.809	0.774	1.17	0.908
<b>Ssk</b>	-0.951	0.266	1.79	0.48	-0.347	-0.0352	0.529	0.441	0.427	0.289	0.144	0.0879	0.614	0.242	0.494	0.456
<b>Sku</b>	8.17	3.03	13.8	3.49	5.03	3.35	3.51	3.47	3.19	3.45	2.79	2.75	3.37	3.57	4.09	3.21
<b>Sdr</b>	0.0026	0.0449	0.0966	0.0742	0.0777	0.1018	0.1482	0.1331	0.0775	0.1158	0.05	0.1035	0.1541	0.1534	0.2057	0.2171

### 4.3. Surface energy

Surface energy was investigated for the three cleaning conditions C1 to C3. Contact angles measured by the sessile drop method are shown in Figure 3. Contact angles had a standard deviation of  $\pm 3^\circ$  over 20 measurements. Angles are modified with cleaning method, ageing, and peening conditions. The calculated surface tensions (according to Eq. 7) of the *S0* reference sample were 21.9, 32.5 and 55.4  $\text{mN}\cdot\text{m}^{-1}$  for the cleaning conditions C1, C2, and C3, respectively. The ultrasonic cleaning in C2 may have eliminated some dirt entrapped in asperities and left on surfaces after C1 cleaning. The ageing effect may reflect the growth of the oxide layer that alters the aluminum surfaces.

The nano-peening process slightly enhanced the surface wettability as indicated by the little increase of apparent solid surface energy in all treated specimens for C2 cleaning condition. The hydrophilic property of the initial surface *S0* with a water contact angle of  $71^\circ$  is thus improved by the nano-peening treatment.

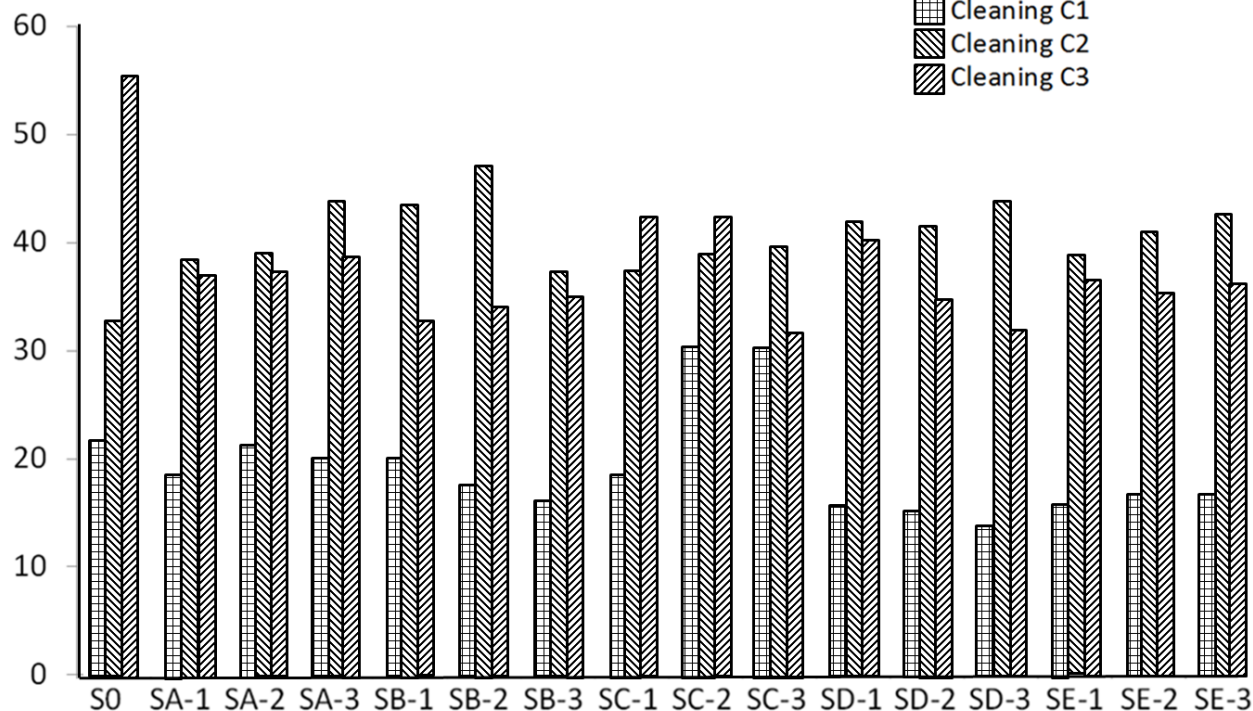
Solid Surface Energy ( $\text{mN}\cdot\text{m}^{-1}$ )

Figure 3: Solid surface energies calculated from contact angles measured by sessile drop method

The effect of cleaning is observable on our samples. Only rinsing with acetone does not clean sufficiently, in agreement with other works [47][48]. The drop of the contact angles when cleaning in ultrasonic baths suggest that residual impurities such as lubricant and dust require ultrasonic energy to detach from the valleys in which they are entrapped. Indeed, hydrophobic property results from the absence of any permanent or induced electrical dipole of the molecule and lack of ability to form hydrogen bonds [9] suggesting that lubricants remained trapped into the surface micro-valleys without ultrasonic baths. The largest increase in apparent surface energy was for SB-2, SE-1, SE-2, and SE-3 samples that had the highest roughness (recall table 3) and thus the highest ability for lubricant entrapment.

Ageing had an influence on the physical properties of its surface. It may possibly be due to the humidity adsorption and the oxide layer thickening. The effect on ageing is ambiguous with either improvement or deterioration of the wettability depending on the surface manufacturing history

and the deposited liquid. The overall trend is a drop in the dispersive component of the surface tension. For aged specimens we were possibly measuring the spreading ability on aluminum oxide rather than bare aluminum metal.

The last parameter influencing the wettability of peened surface is the peening process parameters themselves. The surface peening induced an average variation of  $15^\circ$  for the contact angles. Calculations of air trapped fraction under the drops (Table 4) revealed that the Cassie-Baxter wetting state is predominant leading up to 32% of air beneath the drops. Note that the negative value for glycerol on B2 suggests that the wetting mode is better modeled by a Wenzel state. Nano-peening process parameters can therefore be chosen to maximize the air trapped fraction and subsequently optimize the self-cleaning and AF functionalities.

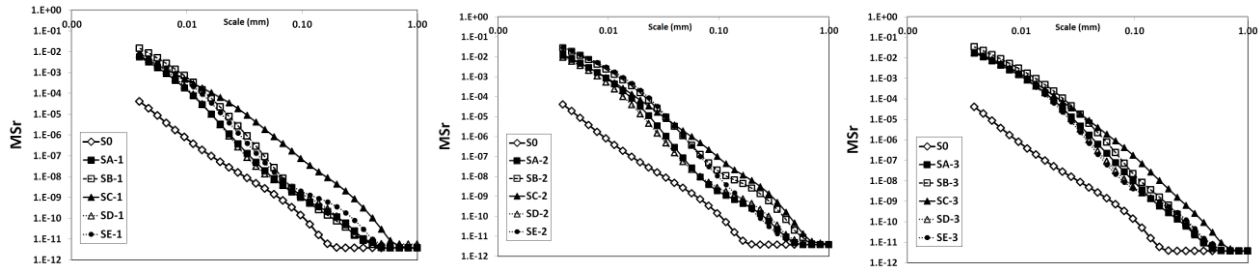
**Table 4:** Air trapped fraction  $1 - \phi_s$  calculated from Eq. 11 for deionised water and glycerol drops

Specimen	S0	SA-1	SA-2	SA-3	SB-1	SB-2	SB-3	SC-1	SC-2	SC-3	SD-1	SD-2	SD-3	SE-1	SE-2	SE-3
deionised water	0.00	0.18	0.23	0.34	0.39	0.30	0.17	0.13	0.20	0.15	0.31	0.31	0.30	0.24	0.27	0.32
Glycerol	0.00	0.03	0.23	0.11	0.19	-0.03	0.09	0.21	0.27	0.28	0.30	0.13	0.05	0.19	0.10	0.15

#### 4.4. Multi-scale characterization

The multiscale spectrum  $MS_{dr}$  were determined for the initial (S0) and all peened surfaces (SA, SB, SC, SD and SE). Figure 4 shows the Log-Log plot of these  $MS_{dr}$  spectrums for the three considered peening pressures *Low*, *Medium*, and *High*. For all the peening process parameters investigated,  $MS_{dr}$  curves exhibited practically a linear behavior under a scale limit of  $400 \mu\text{m}$ . For the initial smooth polished surface S0, this linear behavior occupies lower scale range. The scale limit was lower and did not exceed  $170 \mu\text{m}$ . In fact, the nano-peening process induced a practically uniform vertical shift of the initial  $MS_{dr}$  spectrum which indicated a roughness generation after peening

process. It can be remarked also, in particular for the low peening pressure, that *SC* peened surfaces were the most shifted ones.



**Figure 4:** Multiscale spectrum of surface developed area function of analyzing scale for the three peening pressures.

The linear relation between the multiscale parameter and the analysis scale was representative of a fractal surface where the slope of the  $MSdr$  was a scale-independent parameter. The gap between the final slope and initial one was therefore a pertinent parameter to analyze the multiscale impact of the peening process.

Figure 5 shows a small variation of the  $MSdr$  spectrum for samples *SC* in opposite to all the others samples. This highlights that, for *SC* surfaces, all the scales in the 5 to 400  $\mu\text{m}$  range are impacted by the peening process with the same manner. Furthermore, *SA-1* and *SB-2* peened surfaces with peening pressures *Low* and *Medium*, respectively, exhibited the less scale-dependent modifications.

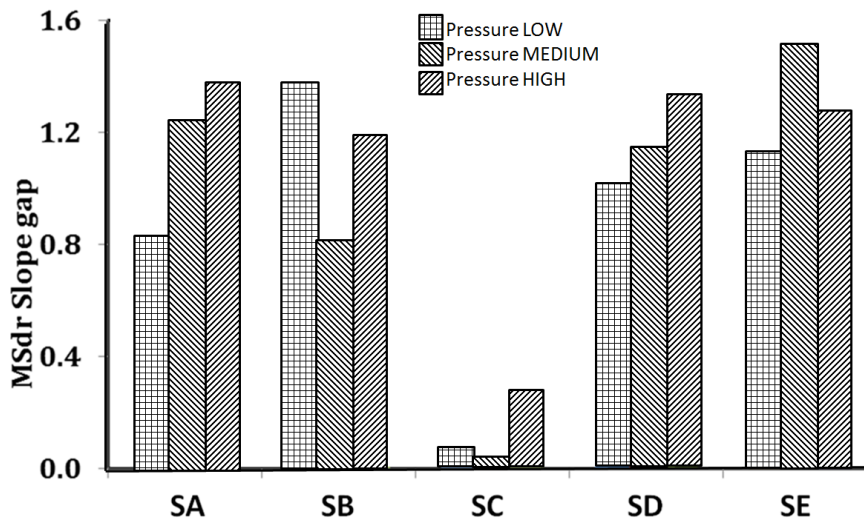


Figure 5: Gap of the MSdr spectrum slope for different peening process configurations

## 5. DISCUSSION

The aim of the present work was to investigate how variations in nano-peening process parameters and cleaning conditions may affect the wettability of AA6063 substrates. The present experimental results combined with literature data should promote a better understanding of the underlying wetting mechanisms associated with nano-peened surfaces.

Correlations between the peening process parameters and the wetting behavior of textured surfaces have been established. The enhancement of hydrophilicity by plastic deformation under ball impacts on metallic surfaces was observed in other works [1] [29][30] [31]. The nano-peening process slightly enhances the surface wettability of AA6063 alloy as indicated by the increase in solid surface energy, suggesting a preferential Wenzel mode of wetting.

The droplet contact angle on a rough surface is given by considering the ratio between the actual solid surfaces over its projection on a relatively flat surface ( $S_{dr}$ ). The roughness ratio ( $S_{dr}$ ) of a rough surface is always greater than 1, since the pairs of peak and valley in nano-peened surface enlarges the surface area. The apparent contact angle of water on nano-peened samples

decreased from 74.1° (flat surface) down to 62.2° for peened surfaces with specific peening parameters. As the surface of AA6063 prior to nano-peening is classified as hydrophilic, the apparent droplet contact angles from nano-peening fall into lower values than that prior to treatment, in agreement with macro-peening works [1] [31]. The reduction of the contact angle correlated inversely to the surface roughness. Nano-peening enhanced only slightly the wetting capability of AA6063 without achieving highly hydrophilic properties. Nevertheless the paper reveals the possibility of nano-peening to be used for modifying the wetting properties optimizing them by precise control of nano-peening process parameters.

Multi-scale approaches demonstrated the significant effect on the wetting properties of the surface texturing scale, apparently near  $10^{-1}$  and  $10^{-2}$  mm wavelengths. The results suggest that the surface textures improve the liquid attractivity by the substrates, possibly inherent to a preferential Wenzel than Cassie-Baxter wetting mode with creation of capillary forces. The textures are two-scale morphologies as indicated by the multi-scale analyses. When introducing cleaning parameters into the system, it is evident that ultrasonic is required to eliminate dirt present in the depth of the valleys. Moreover, ageing has a pronounced effect on both water and glycerol wettability, suggesting that the thickening of the oxide layer affects the overall wetting behavior of the peened surfaces.

Regarding the ageing and cleaning effects, the sessile drop method has been successful in highlighting the importance of the surface conditioning history. Our present surface energy measurements are compared to the data from other works (Table 4). Our results agree with the observed increase in surface tension when ultrasonic cleaning and ageing the aluminum samples.

The contact angle of a water droplet on aluminum has been observed to increase from  $34\pm 3$  degrees in the non-oxidized state up to  $55\pm 5$  degrees for oxidized aluminum surfaces after weeks of exposure to ambient air, but the trend was inverted with a drop in contact angle with time for nano-peened specimens. The aluminum oxide layer thickness and the adsorbed water have an effect on the sample wettability in agreement with other works (Table 5). It has been shown that the degree plastic deformation induced by nano-peening at the surface influences the thickness of

the oxide film on steels [49]. A similar phenomenon may possibly be at the origin of the difference in ageing behavior between the as-polished *S0* surface and the nano-peened surfaces, with a smoothing of the peening-induced irregular geometry by thickening of the oxide layer. The observed drop in contact angle with ageing time for peened AA6063 is in agreement with the wettability behavior observed on other peened metals [31]. Therefore, from static droplet shape measurements, it may be suggested that the initial contact angle on freshly peened surfaces is mainly controlled by the surface geometry while the change in contact angle with ageing is dependent upon the type and thickness of the oxide film formed on the peened surfaces.

**Table 5:** Surface tensions of aluminum substrates

Alloy	Cleaning method	$\gamma$ mN·m <sup>-1</sup>	$\gamma^p$ mN·m <sup>-1</sup>	$\gamma^D$ mN·m <sup>-1</sup>	Ref
6063 – Sample <i>S0</i>	Acetone	21.9	21.1	0.8	Present work
6063 – Sample <i>S0</i>	Ultrasonic with acetone	32.5	13.1	19.4	Present work
6063 – Sample <i>S0</i>	Aged + ultrasonic with acetone	55.4	52.8	2.6	Present work
Al foil	-	45.3	17.3	28.0	[47]
AlSi1MgMn	None	27.0	1.2	25.8	[48]
AlSi1MgMn	Rinsed in ethanol in ultrasonic bath	38.0	7.6	30.4	[48]
AlSi1MgMn	Rinsed in ethanol in ultrasonic bath, then rinsed in acetone in ultrasonic bath	43.9	9.3	34.6	[48]
AlSi1MgMn	Rinsed in alkaline detergent in ultrasonic bath, then rinsed with deionized water	56.3	18.9	37.4	[48]

The roughness effect on wettability is ambiguous depending on the wetting state, i.e. Wenzel or Cassie-Baxter. If the reference material is the polished substrate *S0*, the Wenzel state will be revealed by an increase in wettability while the Cassie-Baxter state will be observed by a reduced wettability induced by entrapped air below the liquid drop [9]. Literature has shown that the SMAT (Surface Mechanical Attrition Treatment) process improved wettability for stainless steel surfaces [1]. Nevertheless our results showed that this is not always the case. The unaged samples mostly revealed a Wenzel wetting behavior except for B2 wetted by glycerol. On the contrary the aged specimens mainly showed a Cassie-Baxter behavior, possibly induced by a heterogeneous growth of Al<sub>2</sub>O<sub>3</sub> oxide layer. Even though the kinetics growth are smaller than 0.1 nm·min<sup>-1</sup> at 373 K [50][51], the amorphous oxide film attains after several months a limiting uniform thickness of a few nm [52] which may contain nanopores [53][54]. This air-oxide bi-

compound layer may be the reason for a change from Wenzel to Cassie-Baxter behavior after ageing. The wettability is therefore modified by a two-level topography with micro- and nano-sized asperities [9]. Indeed, air trapping under a liquid occurs for a valley depth  $a$  and roughness period  $\lambda$  [40]:

$$\lambda < \frac{2\pi a}{\tan(\theta_E)}$$

, where  $\theta_E$  is the contact angle of the liquid on a perfectly flat surface. Considering  $\theta_E = 55^\circ$  (recall Fig 4) and  $a = S_a = 0.5 \mu m$  (recall Table 3), the wavelength of the roughness must be smaller than  $2.2 \mu m$ . Since the shots diameters are approximately  $5 \mu m$  and the nano-porosity on an aluminum oxide film of  $10^{-2}$ - $10^{-1} \mu m$  [53][54], this may possibly explain why the Cassie-Baxter wetting state is not observed on freshly peened but rather on aged peened substrates. The design of the peened surfaces should aim at obtaining the non-wetting behaviors of hierarchical textures [21]. The roughness of the peened surface must prevent the spreading of the liquid drops. A gradient of texture such as hierarchical structures [55][8] is therefore desirable for non-wetting properties such as self-cleaning and AF properties.

Overall the effectiveness of shot peening on controlling wettability and achieving self-cleaning and AF properties is interesting. Efficient processes are today already used for providing self-cleaning properties to substrates as indicated in reviews on the subject [21]. Coatings such as  $Cu(CH_3(CH_2)_{14}COO)_2$  are applicable on many substrates but have limited lifetime because there are sensitive to wear and scratch issues. Multiscale topographies can also be manufactured by FIB and are very efficient in anti-fingerprint functionalities but are costly to manufacture and limited to small surfaces. Even though it is less efficient than coatings and FIB manufacturing, nanopeening processes have been proven through this work to enable the wettability of surfaces by modifying the superficial topographic signature. Advantages of using nano-peening include its resistant to scratches (if selected the appropriate substrate), the improving AF characteristics with ageing, and the ability to manufacture surfaces at very large scales. Future work will be focusing on optimizing the nanopeening process specifically for AF and self-cleaning applications.

## 6. CONCLUSION

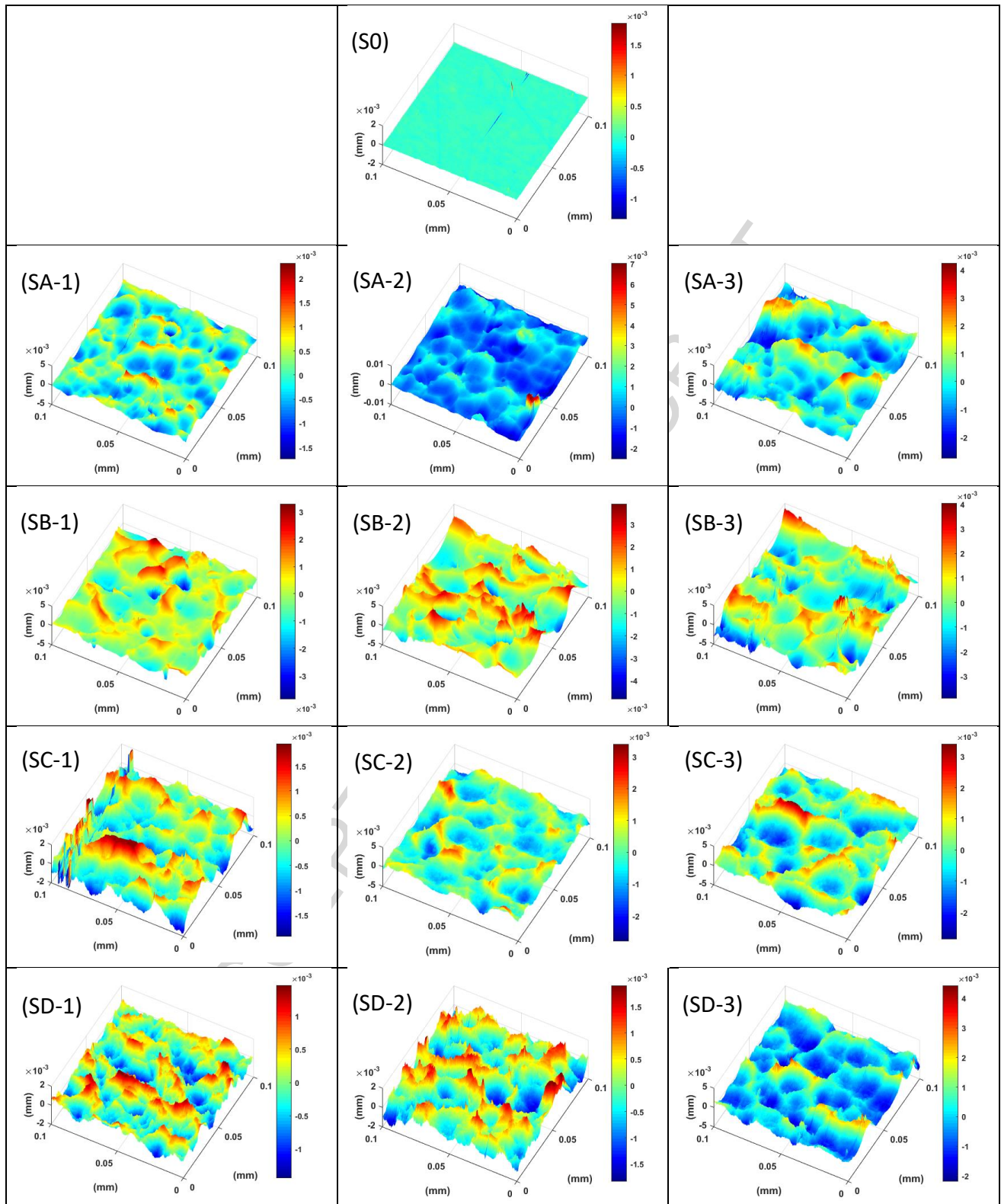
This study focused on the effect of the nano-peening-induced surface textures on their functionality. The impacts of nano-peening balls create craters which consequently enhance the roughness of the steel surface. The generated roughness is process parameter-dependent. First, the cleanliness of aluminum substrates for obtaining reliable wettability measurements was proven to require ultrasonic baths for eliminating dust and lubricants entrapped in the superficial micro-valleys. Once properly cleaned, changing the peening process parameters modify the superficial texture leading to a variation up to 15 degrees in the wettability angles. Nano-peening slightly enhances the wetting capability on AA6063 and yields to a texture with more hydrophilic property.

Ageing was also proven to influence greatly the wetting properties of nano-peened surfaces. The thickening of a porous oxide layer may possibly have modified the multiscale texture of the nano-peened surfaces. Besides, depending on the shot material and pressure, a variety of surface texture was generated with a multiscale-type of roughness. The texture aspect ratio of the nano-peened surface was varied with different gradient of the roughness profile leading to a multiscale observable change in surface energy and contact angle. Future work will focus on determining the peening process parameters and ageing conditions to achieve functional textures.

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## 8. APPENDIX



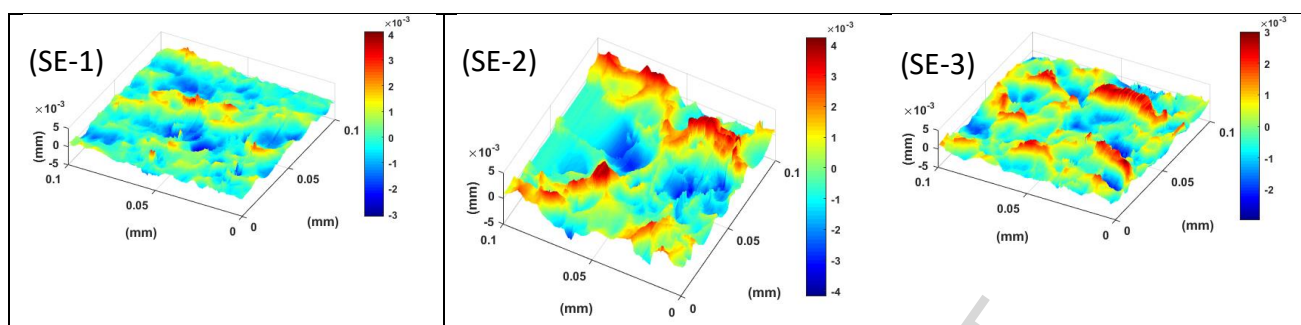


Figure A1: AFM imaging of initial and peened specimens.

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## Research Highlights

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1. Nano-peening process is usable to control the functionality of surfaces, such as self-cleaning and anti-fingerprint functions
2. Nano-peened surface energy is strongly dependent upon the process parameters used to generate these surfaces.
3. Nano-peening influences the ageing behavior of surfaces, and especially their wetting behavior after several months.
4. Mutli-scale approach identified two ranges of scale wavelengths that have been modified by nano-peening.

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