



Science Arts & Métiers (SAM)

is an open access repository that collects the work of Arts et Métiers Institute of Technology researchers and makes it freely available over the web where possible.

This is an author-deposited version published in: <https://sam.ensam.eu>
Handle ID: <http://hdl.handle.net/10985/16035>

To cite this version :

Gabriel SEISSON, Gabriel PRUDHOMME, Pierre Antoine FRUGIER, David HÉBERT, Emilien LESCOUTE, Arnaud SOLIER, Laurent VIDEAU, Patrick MERCIER, Michel BOUSTIE, Laurent BERTHE - Dynamic fragmentation of graphite under laser-driven shocks: Identification of four damage regimes - International Journal of Impact Engineering - Vol. volume 91, p.Pages 68-79 - 2016

Any correspondence concerning this service should be sent to the repository

Administrator : scienceouverte@ensam.eu



Dynamic fragmentation of graphite under laser-driven shocks: Identification of four damage regimes

G. Seisson ^{a,*}, G. Prudhomme ^a, P.-A. Frugier ^a, D. Hébert ^b, E. Lescoute ^a, A. Sollier ^a, L. Videau ^a, P. Mercier ^a, M. Boustie ^c, L. Berthe ^d

^a CEA DIF, Bruyères-le-Châtel, 91297 Arpajon Cedex, France

^b CEA CESTA, 15 avenue des Sablières CS60001, 33116 Le Barp Cedex, France

^c Institut P' – UPR3346 CNRS-ENSMA-Université de Poitiers, 1 avenue Clément Ader, 86961 Futuroscope Cedex, France

^d Laboratoire PIMM – UPR8006 CNRS-Arts et Métiers ParisTech, 151 boulevard de l'Hôpital, 75013 Paris, France

A B S T R A C T

This study presents the results of a large experimental campaign conducted on the Luli2000 laser facility. Thin targets of a commercial grade of porous graphite were submitted to high-power laser-driven shocks leading to their fragmentation. Many diagnostics were used such as high-speed time- and space-resolved imaging systems (shadowgraphy and photography), laser velocimetry (PDV and VISAR), debris collection and post-mortem X-ray tomography. They provided the loading levels into the targets, the spall strength of the material, the shape and size of debris and the localization of the subsurface cracks. The crossed data reduction of all the records showed their reliability and allowed to get a better insight into the damage phenomena at play in graphite. Thereby, four damage regimes, ranked according to their severity and loading level, were identified. It confirms that laser shocks are very complementary to classical impact tests (plates and spheres) since they ally two-dimensional loadings to the possibility of using both, in-situ and post-mortem diagnostics. Finally, the campaign shall be able to provide large and consistent data to develop and adjust reliable models for shock wave propagation and damage into porous graphite.

Keywords:

Carbon
Damage
PDV
VISAR
Strength

1. Introduction

From the beginning of their development, high-power laser facilities have always been considered as potential calibrated-shock generators [1]. Indeed, the interaction between the laser and the front face of a solid target generates a plasma whose expansion creates a shock wave into the matter that may lead to its failure. Thus, similarities with plate impact experiments [2–5] or hypervelocity impacts [6,7] have been pointed out. Many efforts have been done to understand and predict the mechanical effects of the laser-matter interaction through the development of empirical laws [8–11] and specific hydrocodes [12,13]. As a consequence, high-power lasers are now commonly used in a large scope of shock studies [14–21].

The present authors have recently studied the dynamic behavior of porous graphite under high or hypervelocity impacts of metallic plates and spheres [22–27]. On the one hand, for plate impact experiments, all the phenomena are one-dimensional. Data, exclusively particle velocities (free-surface or interface), are collected during

the experiment and samples cannot be recovered for further post-mortem analysis. On the other hand, hypervelocity impacts of spheres generate two-dimensional phenomena and allow sample recovering for fine post-mortem analysis such as micrography and tomography. However, in-situ dynamic observations are less reachable because of time and space uncertainties about the impact.

Hence, the purpose of this paper is to show how a better insight into the two-dimensional damage phenomena of porous graphite can be obtained with well-calibrated and repeatable laser-driven shocks using crossed data reduction from various in-situ and post-mortem diagnostics. In Section 2, we present the experimental set-up. Then, in Section 3, we discuss the free-surface velocity records in order to estimate the loading levels and the spall strength of our graphite. And finally, in Section 4, we confront, correlate and discuss all the experimental results in order to better understand the damage mechanisms, leading to the identification of four different damage regimes.

2. Experimental set-up

Shock experiments have been conducted with a high-power laser facility onto thin graphite targets leading to their fragmentation and/or perforation. Various diagnostics have been used in order to

* Corresponding author. CEA DIF, Bruyères-le-Châtel, 91297 Arpajon Cedex, France. Tel.: +331 69 26 40 00.

E-mail address: gabriel.seisson@cea.fr (G. Seisson).

measure the laser spot and pulse, to capture time- and space-resolved images of the fragmentation and to record the particle velocities. In the same time, reference shots have been done onto well-known materials such as aluminum and tantalum.

2.1. Facility and diagnostics

Luli2000 is a high-power laser facility of the *Laboratoire pour l'Utilisation des Lasers Intenses* (LULI) based at the *École Polytechnique* (Palaiseau, France) [28]. This laser generates square temporal pulses tunable from 0.5 to 5 ns and can reach energies up to 1 kJ at the wavelength of 1064 nm.

Fig. 1 gives a simplified scheme of the experimental set-up. During this campaign, the laser was used at the wavelength of 532 nm with energies between 35 and 700 J, of which about 90% were delivered in 5 ns as shown in Fig. 2(a). The targets were placed at the center of the experimental chamber under high-vacuum where two different beams (called SB and NB, i.e. South beam and North beam) were alternatively focused. They formed a negligible angle of 5.5 degrees with the horizontal x -axis. They shared the same laser source but had their own amplification chain which allowed larger quantity of shots per day. The focal spot of each beam was spatially shaped just before the experiment chamber by means of phase plates that made the beams axisymmetrical and pseudo-Gaussian (see Fig. 2(b) and 2(c)).

The particle velocities of the rear face of the targets were measured by VISAR [29] which has a good temporal resolution. However, its need of a strong return signal can be an issue when the measured surface gets highly deformed and loses its reflectivity. Hence, we also used photonic Doppler velocimetry (PDV) [30–32] that has a lower temporal resolution but is capable to record multiple velocities despite weak return signals (around a few percents of the original one). Two PDV probes with 1-mm-diameter beams were placed in the x - y plan, each forming an angle with the x -axis (α_1 and α_2 respectively). They were pointed to the back face of the targets measuring its velocity and then the velocity of the ejected fragments.

For some shots, VISAR was replaced by an open cube filled with varagel, a gel derived from paraffin with a density close to the water one. Placed at a few centimeters from the back face, this collector captured debris without damaging them in order to measure and analyze them by means of tomography [33].

The time- and space-resolved laser shadowgraphy recorded fragments ejected from the targets back face [34]. A 527-nm continuous laser enlightened two amplified cameras that took pictures of the shadow of the ejecta according to the x - z plan. Each camera made two images at different times with an exposure time of 5 ns. The exact instant of the capture was known thanks to a synchronization system between the laser facility and all the diagnostics.

High-speed photography was obtained by pulsed-laser illumination [35]: two 10-ns pulses of second harmonic YAG laser

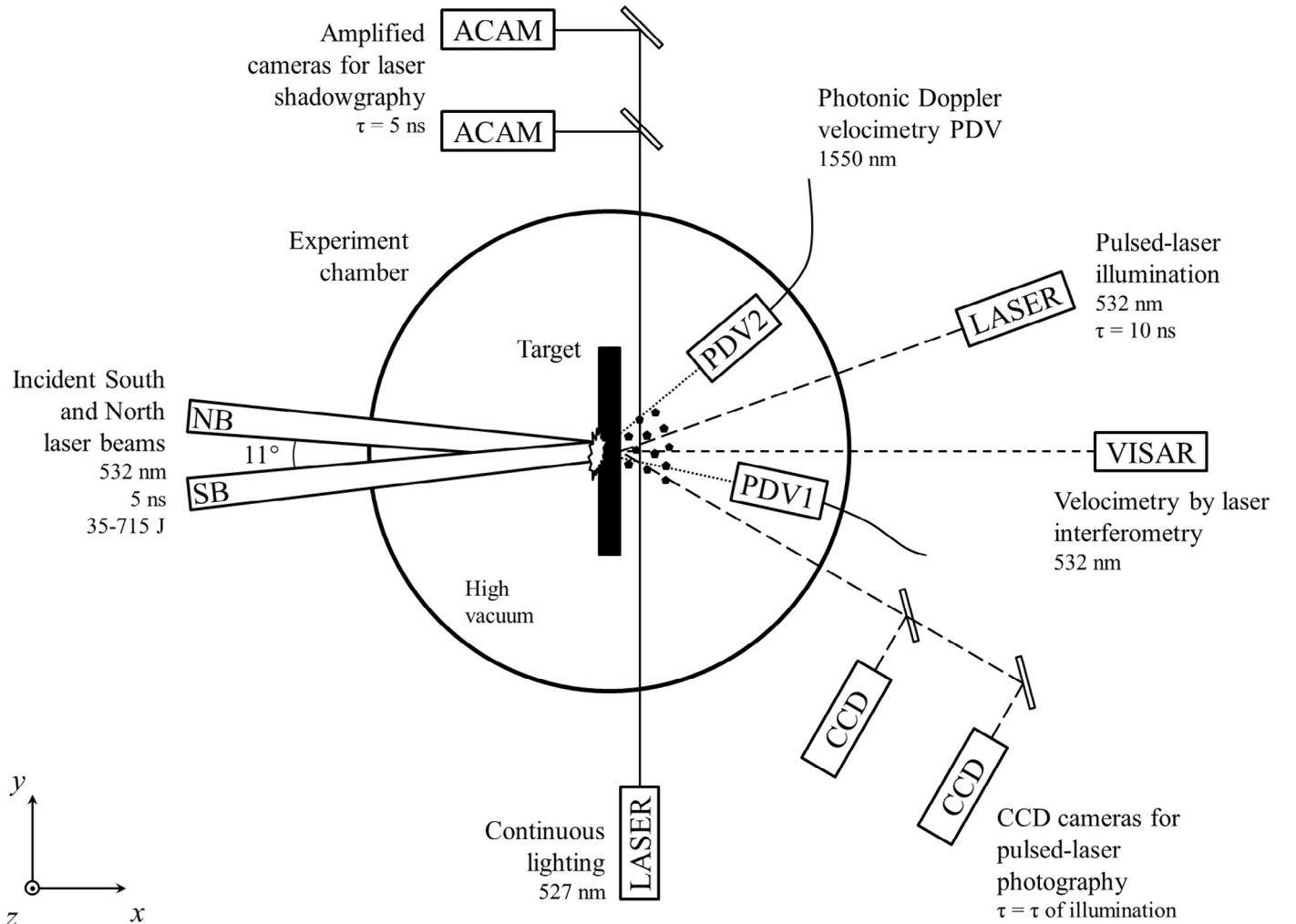


Fig. 1. Simplified scheme of the experimental set-up. Two different types of diagnostic have been used: laser velocimetry, and time-resolved laser imaging.

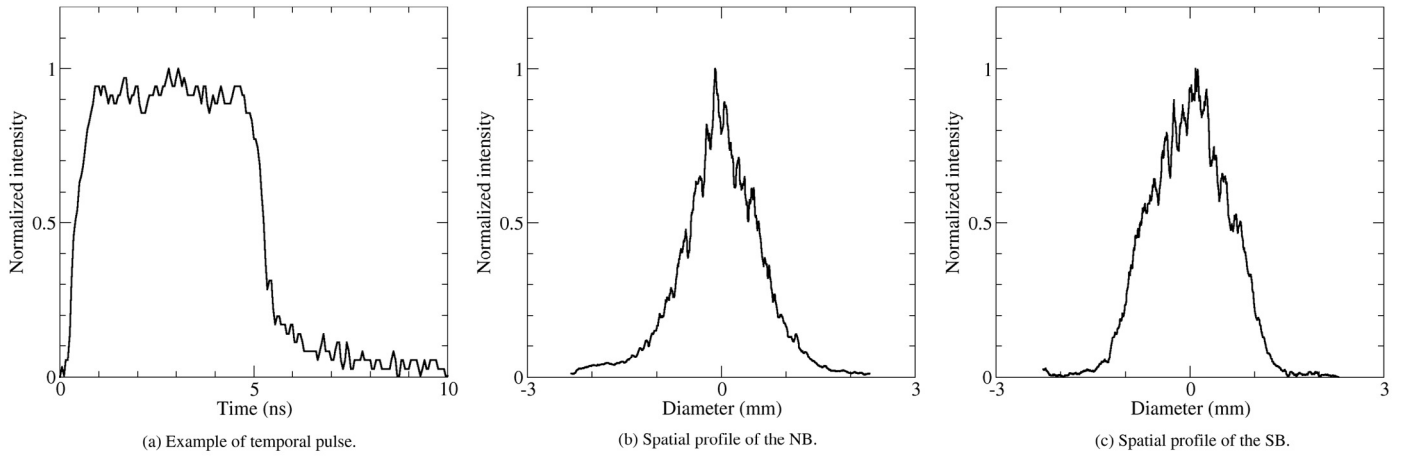


Fig. 2. Temporal and spatial characteristics of the laser pulses of South and North beams. For the record, the temporal profile has been measured by a photodiode for every shot. Very stable, the spatial profiles have been gauged at regular intervals with a CCD camera.

lightened the scene, hence freezing the movement of the rear surface. The apparatus delivered two high-resolution frames, even when fragment velocities exceeded several hundreds of meters per second. Light was fed through bundles of multimode optical fibers providing flexibility in its positioning and, as a side effect, operating a significant smoothing of both objective and subjective speckles. Its residual contrast was estimated at only 14%. Each frame was captured by a CCD camera with sampling 2048×2048 pixels and 500 ns framing for spurious light rejection; an interferometric filter could also be implemented to further reject unwanted light signals (plasma, PDV probes, etc.).

2.2. Targets and shot configurations

The shots of the campaign are summarized in Table 1 giving the characteristics of the targets as well as the laser and diagnostic parameters. As mentioned above, reference shots were performed onto 6061-T6 aluminum and tantalum targets whose respective thicknesses were 250 and 125 μm . But most of the shots were done onto 18-mm square plates of EDM3 graphite whose thickness varied from 0.75 to 2.5 mm.

EDM3 is a macroscopically isotropic commercial grade of graphite made by POCO [36,37] and has been extensively investigated by the present authors [22,38] in the context of understanding the dynamic behavior of matrices from carbon-carbon composites. It is about 22% porous with a density of 1.754 g/cm^3 . A binarised optical micrograph of a healthy sample of EDM3 (after cutting and polishing) is displayed in Fig. 3. It shows that the side of the cubic Representative Volume Element (RVE) is of the order of 50 μm , i.e. from 15 to 50 times less than the target thickness and around 40 times less than the laser spot diameter. The main features of EDM3 that may be useful to the reader and to the discussions are recalled in Table 2.

Finally, the back face of the targets were covered of a 1- μm aluminum layer in order to better reflect laser diagnostics.

3. Velocimetry analysis

In this section, we present and analyze the VISAR and the PDV records in order to evaluate the difference between South and North beams, the spall strength of EDM3 and the mechanical loading endured by the targets.

Table 1
Summary of the shots on aliminum, tantalum and EDM3 graphite. Only α_2 is given since $\alpha_1 = 13^\circ$ never changed. The laser energy is the one that has been measured and not the one that has been adjusted by calibration (cf. Section 3.1). The reference time is set to be the arrival time of the high-power laser onto the front face of the target.

Shot number	Target		Laser		Velocimetry		Shadowgraphy (μs)				Photography (μs)		Debris collector
	Material	Thick (μm)	Beam	Energy (J)	VISAR	α_2	IMG1	IMG2	IMG3	IMG4	IMG1	IMG2	
3	Al	250	S	116	×	15°	1.5	2	3	4	0.46	0.54	–
4	Al	250	N	572	–	15°	0.6	1	1.4	1.8	–	0.48	–
5	EDM3	2500	S	215	×	15°	5	16	30	50	10.44	16.44	–
6	EDM3	2500	N	715	×	15°	5	16	30	50	10.44	16.44	–
7	EDM3	750	S	121	×	15°	5	16	30	50	10.44	–	–
8	EDM3	750	N	652	×	15°	4	7	10	13	3.36	9.36	–
9	EDM3	1000	N	636	×	42°	3	5	8	10	2.36	8.36	–
10	EDM3	1000	S	235	×	42°	3	8	15	20	4.36	10.34	–
11	EDM3	1500	N	608	×	42°	4	10	15	20	4.36	10.34	–
12	EDM3	1500	S	189	×	42°	10	20	30	50	–	–	–
13	EDM3	2000	N	564	×	42°	10	30	50	100	10.34	30.34	–
14	EDM3	750	S	35	×	42°	5	10	30	50	10.34	30.34	–
15	EDM3	750	S	259	–	42°	5	16	30	50	10.34	30.44	×
16	EDM3	750	N	167	×	42°	5	10	20	30	10.34	30.34	–
17	EDM3	750	S	547	×	42°	2	4	8	10	2.4	8.4	–
18	EDM3	1000	N	342	×	42°	3	9	15	20	3.4	9.4	–
20	Ta	125	N	644	×	42°	1	2	4	7	1.44	7.36	–
26	EDM3	1000	N	415	–	42°	–	–	–	–	–	9.4	×
27	EDM3	1000	S	467	–	42°	–	–	–	–	3.4	9.4	×

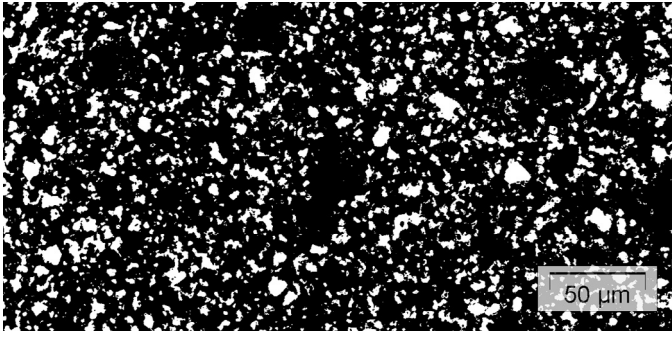


Fig. 3. Binarized optical micrograph of a healthy sample of EDM3 after cutting and polishing. Material matrix appears in black whereas voids are in white. The Representative Volume Element (RVE) is about $50 \times 50 \times 50 \mu\text{m}$.

Table 2

Main characteristics of the EDM3 graphite according to references 22 and 38. The Young modulus was extracted from tensile and compression tests and confirmed by ultrasonic analysis that also gave the sound velocities.

Density ρ_0 (kg/m ³)	Porous	1754
	Compact	2265
Failure stress σ_r (MPa)	Tension	70
	Compression	140
Failure strain ϵ_r (%)	Tension	1
	Compression	8
Young modulus E (GPa)		11–12
Bulk sound velocity C_0 (m/s)		2212
Fracture toughness K_{Ic} (MPa $\cdot\sqrt{\text{m}}$)		0.8–1.2
Porosity γ_0 (%)		22

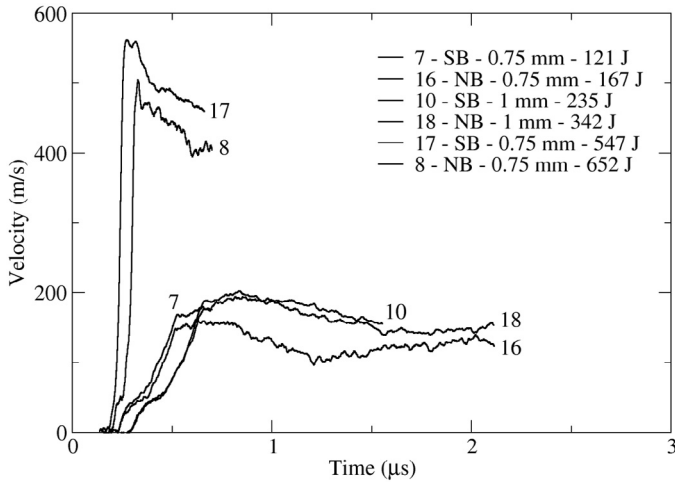


Fig. 4. Free surface velocities for three couples of similar shots performed with different beams. It clearly points out the difference between NB and SB. For clarity, noise has been reduced.

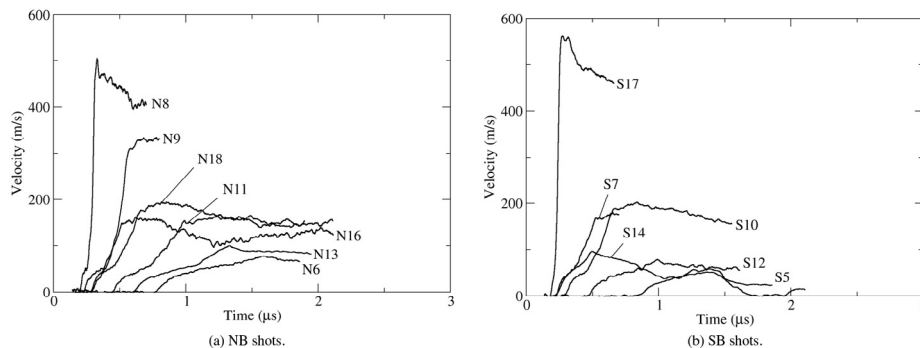


Fig. 5. VISAR records of shots onto EDM3 graphite. Noise has been reduced.

3.1. North beam vs. South beam

Before presenting all the VISAR records, the difference between NB and SB has to be pointed out. The shots conducted on both beams must be considered as two distinct series. This is demonstrated by Fig. 4 that presents VISAR signals for three couples of shots with identical thicknesses. For each couple, the energy of NB is slightly higher than the one of the SB but this is not the case of the free surface velocity. For example, the energy of shot #8 is 20% higher than shot #17 but its velocity is 15% lower. For clarity and consistency we specify in the following the laser beam used for each shot adding the letter S or N before the shot number, e.g. S17 and N8.

The most obvious reason of such a discrepancy between NB and SB in spite of similar energies is the shape of their respective focal spots that are rather different. A significant part of the announced energy can be spent in the wings of the Gaussian spot at very low intensities but over a large area. Thus, it is necessary to know the exact amount of energy contained in the useful part of the spot, i.e. the central part where the intensity is high enough to generate a shock wave into the target. Therefore, reference shots onto well-known materials that are aluminum and tantalum have been performed. A calibration process consisting in computations of laser-matter interaction and shock wave propagation (not presented here) revealed that the useful part of the focal spot contains 45% of the measured energy for NB and 80% for SB which is consistent with the VISAR records plotted in Fig. 4.

3.2. Loading levels

Fig. 5 gathers the VISAR records obtained for the shots onto EDM3. Note that the time uncertainty is of ± 2 ns. The set of shots covered a large field of loading since the free surface velocities range from 50 to 560 m/s.

Using the acoustic approximation, one can roughly evaluate the maximum pressure P_m of the shock wave breaking out of the target back face by means of the following expression:

$$P_m = \frac{1}{2} \rho_0 C_0 U_m \quad (1)$$

where ρ_0 and C_0 are the initial density and the bulk sound velocity of the target material and U_m is the maximum free surface velocity. The pressure P_m of each shot on graphite is given in Table 3, ranging from 0.1 to 1.1 GPa. But this must be considered with caution, because if the acoustic approximation is quite well adapted to dense materials where the sound velocity does not vary so much with the pressure, this is not the case for porous materials such as EDM3 where the sound velocity decreases first and then increases because of the compaction phenomenon. However, it gives good orders of magnitude.

Table 3

The maximum pressure seen by the back face P_m is estimated from the maximum free surface velocity U_m and from equation 1. For shots without VISAR (starred numbers), U_m is extracted from PDV signals. The ablation pressure P_{ab} is calculated thanks to the maximum calibrated laser intensity I_m and to equation 2.

Shot number	05	06	07	08	09	10	11	12	13	14	15*	16	17	18	26*	27*
Laser beam	S	N	S	N	N	S	N	S	N	S	S	N	S	N	N	S
Thickness (mm)	2.5	2.5	0.75	0.75	1	1	1.5	1.5	2	0.75	0.75	0.75	0.75	1	1	1
U_m (m/s)	51	77	169	511	332	201	163	78	99	97	272	162	564	194	190	320
P_m (MPa)	99	149	327	991	644	390	316	151	192	188	528	314	1094	376	369	621
I_m (TW/cm ²)	1.57	3.94	0.89	3.59	3.50	1.72	3.35	1.38	3.11	0.26	1.89	0.92	4.00	1.88	2.29	3.42
P_{ab} (GPa)	43.5	90.6	27.4	84.2	82.5	46.7	79.6	39.2	74.9	10.2	50.4	28.3	91.7	50.2	58.6	80.8

It is interesting to compare P_m to the ablation pressure generated on the front face by the plasma expansion. In the case of aluminum, the Grün formula [9] gives good results:

$$P_{ab} = 1440 \left(0.8 \frac{I_m}{10^5} \right)^{0.8} \quad (2)$$

with P_{ab} the ablation pressure in GPa and I_m the maximum laser intensity expressed in GW/cm². There is no such empirical law for graphite but we have shown that the Grün formula gives good order of magnitude for graphite at intensities around 1 TW/cm² [25]. The intensity used here is an equivalent one calculated after the calibration process in the case of a homogeneous top-hat spot whose diameter has been adjusted to conserve the power. Table 3 gives the ablation pressure of each shot deduced from equation 2.

The immense difference (two orders of magnitude) between P_{ab} and P_m must be noticed. It shows a strong attenuation of the shock wave during its propagation through the graphite target. This phenomenon is linked to the target thickness, to the very short laser pulse and to the fact that the velocities of the release waves in porous materials are much higher than the shock wave one.

3.3. Spall strength

Fig. 6 shows the back face of shot S27 captured by the laser imaging at 3.4 μ s after the laser pulse beginning. The Gaussian shape of the beam leads to a strong bulge of the surface degrading its reflectivity. It certainly happened right after the shock break-out instant that can explain the fact that VISAR signal is lost before any pull-back. Thus, VISAR is very useful for recording the shock front but for spall phenomenon, PDV must take over.

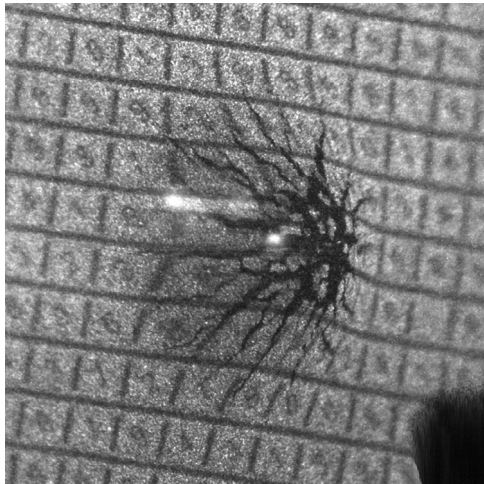


Fig. 6. Tilted view of the back face of shot S27, 3.4 μ s after the laser pulse. The surface is strongly deformed under the effect of the shock. The black area in the right-hand-side bottom corner is due to the sensor damage. White trails are a residue of the PDV pumping laser.

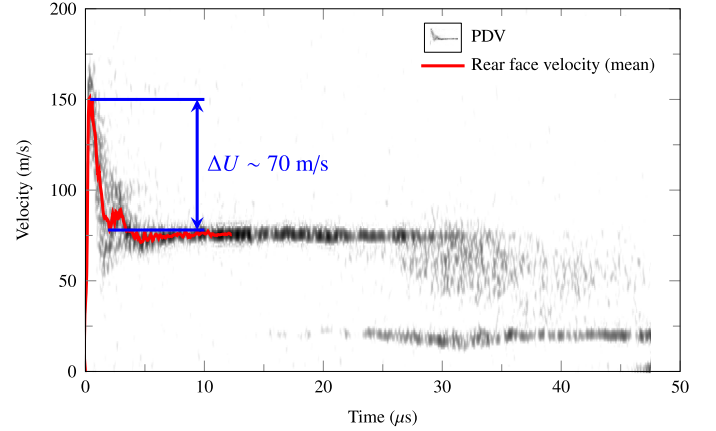


Fig. 7. Spectrogram S7-PDV1. The second constant velocity signal around 20 m/s after 20 μ s is hardly understandable without the help of the imaging systems. Velocities are corrected by the cosine of α_1 .

Remind that the PDV probes use a collimated beam whose diameter is above 1 mm. It means they record all the velocities over a surface equal to the beam area. As a result, we get a spectrum of velocities whose maximum values are theoretically related to the center of the stressed area. Nevertheless, a correction is needed in order to take into account the angles α_i dividing the velocities by their respective cosine (in the hypothesis of colinearity between the x -axis and the surface and/or debris motion).

The spectrogram of S7-PDV1 plotted in Fig. 7 confirms the maximum free surface velocity of 170 m/s recorded by VISAR, which is the case ($\pm 10\%$) for every shots with both PDV and VISAR. Then, after 4 μ s, it clearly shows a spall flight with a constant velocity signal around 75–80 m/s.

Averaging the velocities before 10 μ s gives a unique velocity signal where a pull-back is clearly visible with a $\Delta U \sim 70$ m/s. One can estimate the spall strength by:

$$\sigma_{sp} = -\frac{1}{2} \rho_0 C_0 \Delta U \quad (3)$$

It gives $\sigma_{sp} = -135$ MPa a value sensibly higher than the static tensile strength of -70 MPa given in Table 2. However, given the porosity of EDM3, the acoustic approximation must be considered with caution. Anyway, the existence of a planar spall is uncertain because of the Gaussian shape of the focal spot that complexifies the phenomenon. In fact, after 20 μ s, the signal lose its intensity and a new trail progressively begins around 20–25 m/s. The joint use of PDV and imaging systems will help to understand this phenomenon.

4. Correlation of the experimental results

Many in-situ diagnostics have been simultaneously used during the campaign. Each of them gives partial information about the shock propagation into the target or about its fragmentation. They were

completed by post-mortem tomographies of the recovered targets and debris, informing about damage. The purpose of the following is to correlate all these results in order to better understand the damage phenomenology of graphite under laser-induced shock.

4.1. Representative shots

A first data reduction allowed us to visually identify four different damage regimes to which almost all the shots can be linked to. Each of the four shots discussed in this section is representative of a particular damage regime.

4.1.1. Shot S7 – 0.75 mm – 0.89 TW/cm²

Fig. 8 gives the results of the two time-resolved imaging systems used during shot S7. Surprisingly, they evidence two spall levels: the one that is ejected first looks like an Asian conical hat and is constituted of multiple debris; it is followed by a unique spall shaped like a cymbal or a saucer recessed of the first stage of debris. The distance between those two stages is increasing with time which indicates the first one is moving faster.

We drew the position and the size of the PDV1 beam onto the shadowgraphy images. In reality, probes were placed in the x - y plan instead of the x - z plan as suggested here but this is not much inaccurate because of the axisymmetry of the experiment. In this manner, one sees that the Asian hat goes first through the PDV beam. Then, between 16 and 50 μ s, the cymbal progressively intercepts the beam. Thus, the velocity signal around 75–80 m/s seen on Fig. 9 should correspond to the first spall level whereas the one around 20–25 m/s should belong to the second stage. It is easily verifiable thanks to the time- and space-resolved shadowgraphy which enables to know the average speed of an object V_{av} between two images, using the simple formula:

$$V_{av} = \frac{x_2 - x_1}{\Delta t} \quad (4)$$

According to Fig. 8(a), it leads to 88 m/s for the first level and 28 m/s for the second one. The order of magnitude is rather good even if a slight discrepancy exists. It probably comes from the fact that the two methods do not consider the velocity of the same points, those possibly varying despite the almost axisymmetry of the experiment.

4.1.2. Shot S15 – 0.75 mm – 1.89 TW/cm²

The same analysis is feasible for totally different shots such as shot S15, conducted at higher energy and whose results are given in Fig. 9. With shadowgraphy, one identifies three successive debris levels whose velocities are around 250 m/s for the first one (L1), 140 m/s (L2) and 85 m/s (L3). They are represented on the spectrogram of PDV1 by means of three horizontal lines. The identification of the slower level is the easiest because it is the one that stays the longest in the PDV beam (from 10 μ s).

4.1.3. Shot S17 – 0.75 mm – 4 TW/cm²

Until now, we followed the assumption that the motion of the ejecta was exclusively along the x -axis and thus, the velocity measured by PDV1 could simply be corrected by the cosine of α_1 . It was rather accurate for shots S7 and S15, but it is less obvious in the case of shot S17 conducted at even higher energy whose results are outlined in Fig. 10.

Beyond the first instants, one cannot know the exact velocity along the x -axis because the debris cloud takes the shape of an expanding sphere, also moving along this axis. Hence, the record is only a projection of the particle velocity along the probe axis. This is an incomplete measure whose bias depends not only on the time but also on the observed particle. When the PDV beam skims over the sphere periphery, it records in the same time particle velocities with strongly different directions. That is why no angle correction has been done on the PDV spectrogram of Fig. 10(a). Nonetheless, at late instants one observes a constant velocity signal around 100 m/s that according to shadowgraphy seems to be the one of the cone following the sphere.

4.1.4. Shot N13 – 2 mm – 3.11 TW/cm²

The reading of shot N13 is much more simple as shown in Fig. 11. Except small central debris due to overintensities of the focal spot observable in Fig. 2(b), imaging systems evidence the creation and the flight of a single spall at very low velocity in the order of 15 m/s. This fact is confirmed by the sole constant velocity signal appeared on PDV1. Moreover, one notes that the pull-back observed on the spectrogram ($\Delta U \sim 70$ m/s) corroborates the one recorded for shot S7 (see Section 3.3).

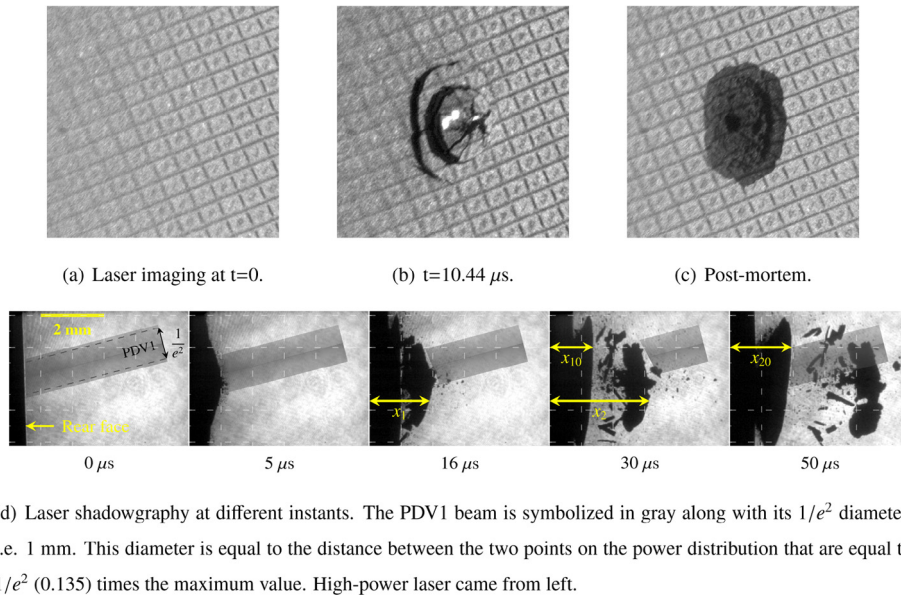


Fig. 8. Shot S7 – 0.75 mm – 0.89 TW/cm². Results of the laser imaging systems at different instants after the high-power laser pulse.

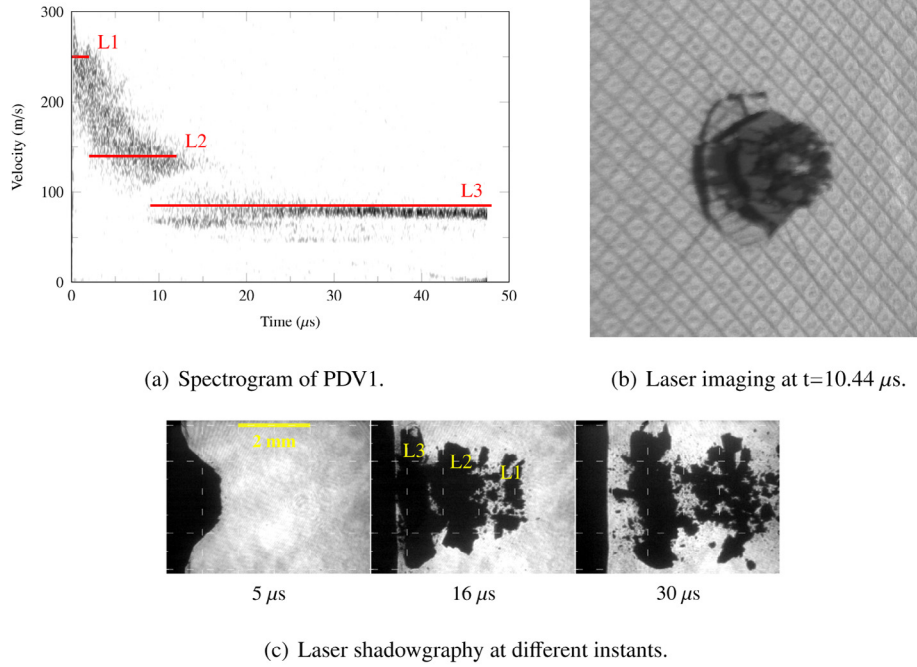


Fig. 9. Shot S15 – 0.75 mm – 1.89 TW/cm². Laser imaging and shadowgraphy at different instants and debris velocity recorded by PDV.

4.2. Damage regimes

As said previously, shots N13, S7, S15 and S17 were not randomly selected. They are representative of four different damage regimes identified, proceeding from the data reduction of the campaign. Name them D1 to D4 according to their physical aspect and severity:

- Regime D1:** formation of a single conical spall;
- Regime D2:** apparition of a double spall with a multi-fragmented first stage and a one-piece second one;

- Regime D3:** multiple fragmentation of the target into few debris levels;
- Regime D4:** explosion of the target with a sphere-shaped cloud constituted of numerous debris of small size.

4.2.1. Identification and origins

The data reduction of the other shots allows to identify those linked to one or the other regime based on the damage aspect as ranked in [Table 4](#). Because damage necessarily depends on loading

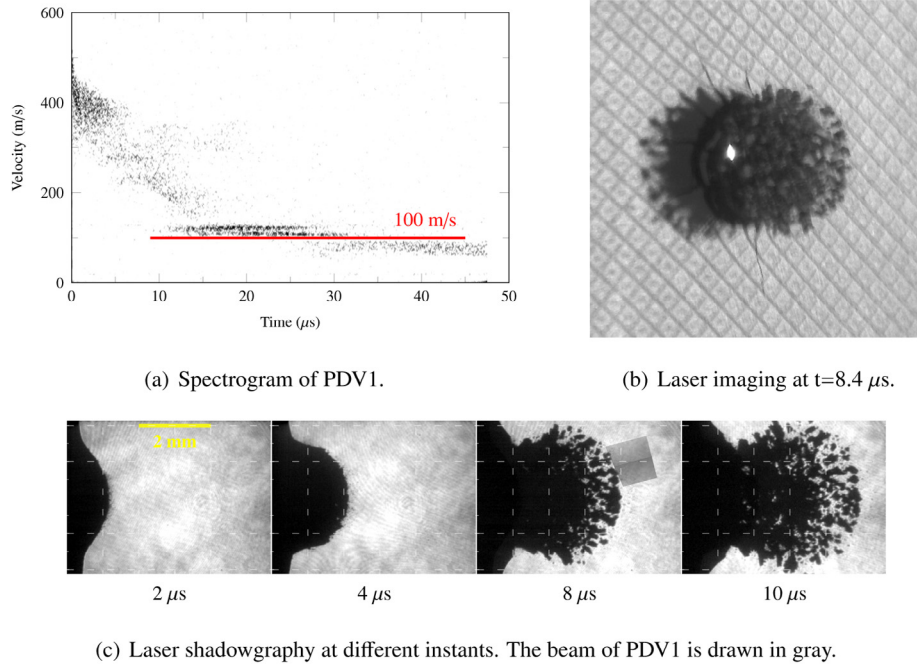
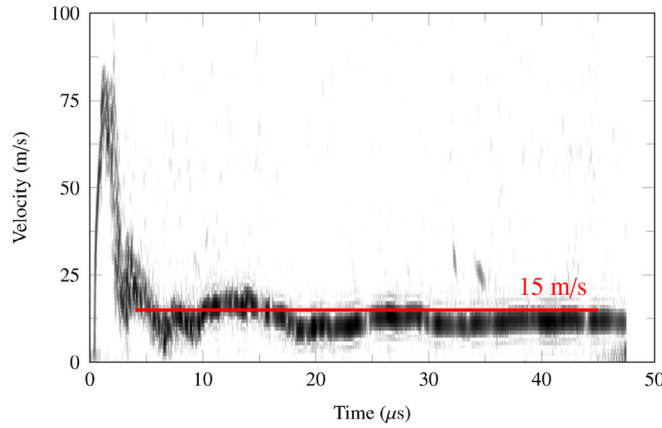
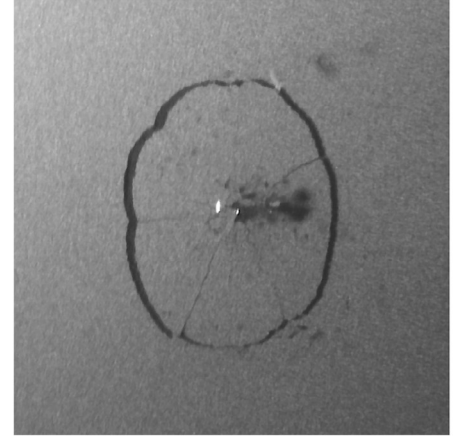


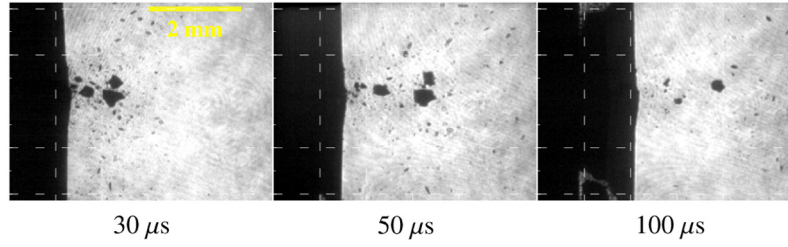
Fig. 10. Shot S17 – 0.75 mm – 4 TW/cm². Laser imaging and shadowgraphy at different instants and debris velocity recorded by PDV. Velocity has not been corrected by the cosine of α_1 .



(a) Spectrogram of PDV1.



(b) Laser imaging at $t=30.34 \mu s$.



(c) Laser shadowgraphy at different instants.

Fig. 11. Shot N13 – 2 mm – 3.11 TW/cm^2 . Laser imaging and shadowgraphy at different instants and debris velocity recorded by PDV.

conditions, the maximum intensity, the maximum pressure seen by the back face and the maximum free surface velocity are recalled.

Shots S5, N6, S10, S12, S14 and N16 are not ranked, either because there is no apparent damage or because the latter does not look like the one of any other shot. It clearly appears that the belonging of a shot to a regime is not directly related to the laser intensity, i.e. to the ablation pressure. For example, in D2 the laser intensities are varying from simple to double; and the unique intensity of D1 (N13 – 3.11 TW/cm^2) is higher than the lowest one of D3 (S15 – 1.89 TW/cm^2). Nevertheless, the back face velocities are very close to each other for shots from a same regime. This phenomenon is illustrated by Fig. 12 that gives an overview of the four regimes for each beam. In the case of NB, the ablation pressure is constant and the target thickness is varying whereas it is the opposite for SB. The only common point between the shots of one regime is the free surface velocity, hence the loading level seen by the sample rear face. Note that the existence of different and identical thicknesses in a same regime (cf. regimes D2, D3 and D4 in Table 4) indicates the statistical homogeneity of all the targets in spite of

the fact that the thinnest one represents only 15 times the RVE (see Section 2.2).

We thereby obtained thresholds for the four damage regimes according to the stress endured by the target back face (see Table 4). However, they were estimated by means of the acoustic approximation, which cannot be totally trusted in the case of porous materials, and they should be refined thanks to further reliable simulations.

4.2.2. Other shots analysis

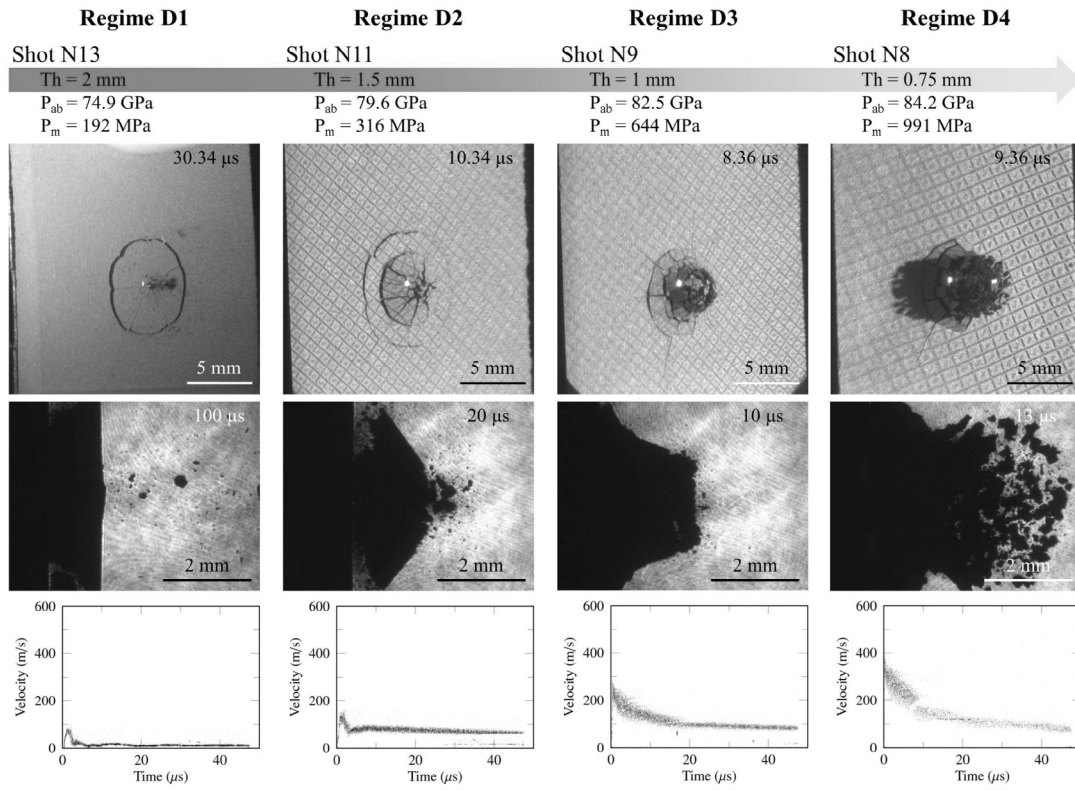
Apparently, six shots do not match with the four-damage-regime ranking because their fragmentation does not look like any other. However, some of them have free surfaces velocities close to those of ranked shots. Post-mortem tomographies have been performed in order to detect eventual subsurface damage capable to clarify our analysis.

According to U_m , S10 and N16 should belong to D2 but imaging given in Fig. 13 does not show any typical double spall corresponding to this regime. Nevertheless, the tomographic slices on the same

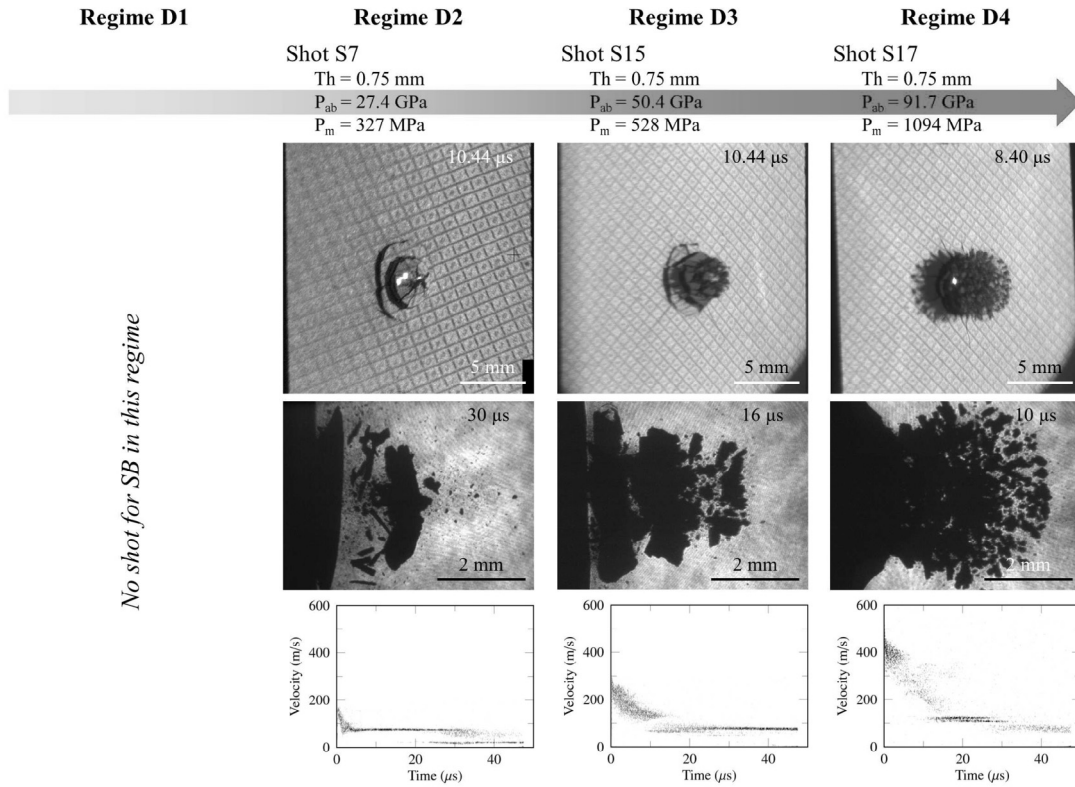
Table 4

Ranking of the shots according to the damage regime they belong to, thanks to imaging systems results. Six shots are not classifiable a priori: S5, N6, S10, S12, S14 and N16.

Regime	D1					D3			D4	
Shot	N13	S7	N11	N18	N26	N9	S15	S27	N8	S17
Thick. (mm)	2	0.75	1.5	1	1	1	0.75	1	0.75	0.75
I_m (TW/cm^2)	3.11	0.89	3.35	1.88	2.29	3.50	1.89	3.42	3.59	4.00
U_m (m/s)	99	169	163	194	190	332	272	320	511	564
P_m (MPa)	192	327	316	376	369	644	528	621	991	1094



(a) North beam. Ablation pressure P_{ab} is constant whereas target thickness is decreasing.



(b) South beam. Target thickness is constant whereas P_{ab} is increasing.

Fig. 12. Evidence of the four damage regimes. The reference time is set to be the arrival time of the high-power laser onto the front face of the target.

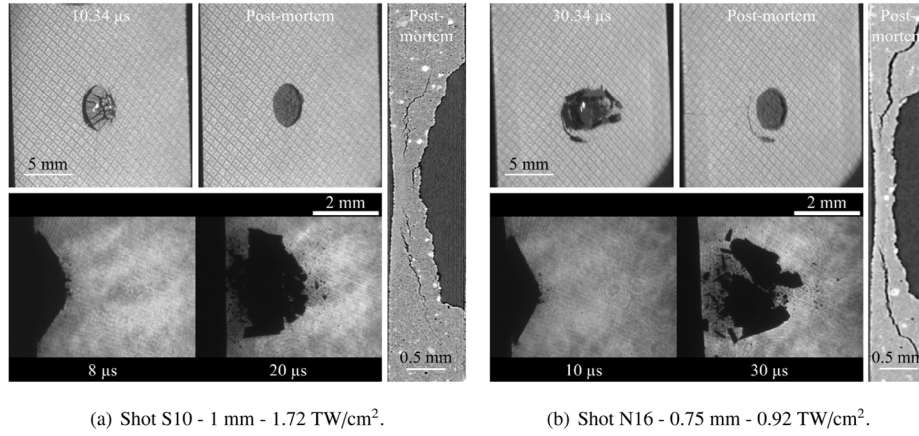


Fig. 13. Shots S10 and N16 belong to the threshold between regimes D1 and D2. Imaging systems do not show double spall but post-mortem tomographies reveal a second spall almost formed under the back surface. Left-hand side of tomographies: front face. Right-hand side: rear face. The white dots on tomographies are inclusions of vanadium and titanium from the graphite manufacturing process.

figure reveals subsurface cracks that have not completely or not at all reached the back face. Their shape suggests that a second spall was appearing but did not detach itself. Therefore, those two shots are at the threshold between D1 and D2, between a single and a double spall.

Given the velocities of shots S5, N6, S12 and S14, they could be logically linked to regime D1 but no damage was visible with the imaging systems. Fig. 14 presents tomographies of these targets.

The laser shock of shot S5 produced an important crater on the target front face but did not generate cracks nor crack initiations in the direction of the back face as shown in Fig. 14(a). S5 does not belong to any damage regime. Moreover, its free surface velocity is sensibly lower than the observed one for D1, i.e. 51 m/s instead of around 100 m/s.

The tomography of shot S14 evidences a conical crack underlined in yellow in Fig. 14(d). If it had propagated up to the rear face, a conical spall would have been formed and ejected. Hence, S14 is probably at the threshold between no damage and regime D1.

It is harder to interpret shots N6 and S12. In both cases, tomographies reveal conical cracks facing the back surface. There are few hypotheses. First, if cracks had reached the back face, double or triple spall would have occurred and these two shots could not be ranked

in regime D1. Second, if only the crack that is the closest to the front face had reached the back face, there would be a single spall. This is likely since it would lead to the perforation of both targets which has been noted for N13 (the unique confirmed shot of D1). Moreover, as the spall of this shot has not been recovered, we cannot know if it held in other crack initiations. In that case, N6 and S12 ranked somewhere between no damage and D2. Third and last, the creation of a large crater on the front face of the two shots may have strongly influenced the crack initiation and propagation in the deeper volumes. Damage regimes would thus not only be linked to the rear surface velocity but also to the target thickness, since large craters are formed onto the thickest ones.

4.3. Damage characterization

4.3.1. Targets

Tomographies presented in Figs. 13 and 14 show that, when it exists, the subsurface damage into the targets mainly takes the form of long conical cracks. It is the case of all shots up to the regime D2 included. Sadly, for shots of regimes D3 and D4, the belated strong flexions caused by the laser loading broke the targets into unrecovered multiple parts.

Shot S12 is of particular interest as it allows to learn how front face craters are formed thanks to Fig. 14(c). A crack propagates from the depth to the surface apparently leading to the ejection of a not or barely fragmented block of matter despite the fact that the front face endured pressures around 40 GPa.

All these post-mortem observations should be very helpful for a precise adjustment of the thresholds of further numerical failure models.

Finally, note that, even though the graphite–diamond phase transition pressure (18–28 GPa according to the SESAME 7832 table) has been widely exceeded for almost all the shots, no diamond phase has been observed on the tomography.

4.3.2. Debris

For shots N26 (D2) and S27 (D3), debris have been recovered thanks to varagel collectors. Tomographies have been performed in order to analyze their population. Fig. 15 plots for both shots the cumulated debris volume according to the particle volume. The two targets have the same thickness, i.e. 1 mm. To allow the comparison, we neglect the potential shape effect of the laser beam on the ejected particles volume.

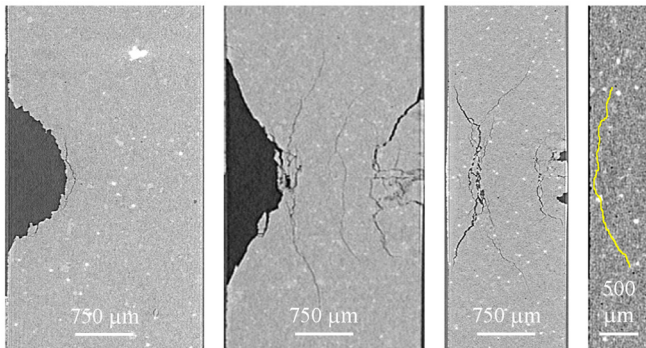


Fig. 14. Tomographies of shots S5, N6, S12, and S14. The target fronts are left. The white dots are inclusions of vanadium and titanium from the graphite manufacturing process. For clarity, crack of S14 has been underlined in yellow.

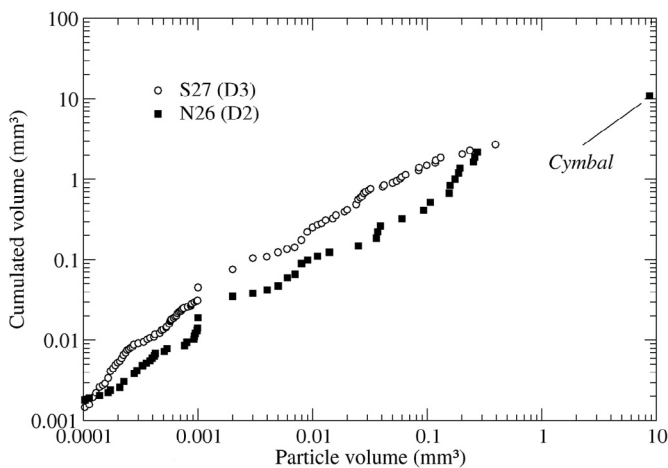


Fig. 15. Cumulated debris volume according to particle volume. The volume of ejected matter is greater for the lowest damage regime (D2). Particles are smaller for the highest regime (D3).

Unlike we could have anticipated, the volume of the ejected matter during the lowest shot (N26) is almost four times greater than for the highest shot (S27). The difference entirely comes from the cymbal-like debris observed in regime D2 since it accounts for three quarters of total volume of the debris. Once excluded, volumes become equivalent.

Differences in terms of debris population have to be noticed. Particles of volume between 0.0001 and 0.001 mm³ are more numerous for shot S27 (D3) than for shot N26 (D2) since the slope of the first one is steeper. The slopes are then equivalent for particles between 0.001 and 0.1 mm³ which indicates a similarity between the debris populations. Finally, beyond 0.1 mm³, the slope of shot N26 is the steepest which reveals its debris of this size are more numerous than for S27. These measures are consistent with our visual observations that show the size of debris is decreasing when the loading level increases. According to Grady's theory [39], it confirms that the strain rate is higher in D3 than in D2.

5. Summary and future work

Previous studies showed the shortcomings of classical impact tests (plates and spheres) in helping to understand the two-dimensional damage phenomena of a commercial grade of porous graphite. This paper has demonstrated that a better insight can be obtained using well-calibrated and repeatable laser-driven shocks along with various in-situ and post-mortem diagnostics:

- Spall strength has been estimated thanks to PDV data;
- Precise VISAR records allowed to value the stress level seen by the rear face of the targets;
- High-speed imaging systems provided a dynamic visualization of damage and fragments and helped to understand unfamiliar long-time PDV spectrograms;
- Time- and space-resolved shadowgraphy confirmed velocity measurements;
- Fragment analysis and subsurface crack localization became available thanks to post-mortem tomography;
- Identification and comprehension of four damage regimes was possible because of a large crossed data reduction.

Given all the collected data, associated numerical works are currently being conducted and will be the subject of a further publication. Free-surface and fragment velocity, back-face deformations, crack

localizations and fragment sizes, in conjunction with the space and time characterization of the laser pulse, will help to develop and adjust reliable models for shock wave propagation and damage into graphite. Then, the stress thresholds of the four damage regimes could be refined. Finally, similar experimental and numerical approaches could be conducted for other materials.

Acknowledgments

The authors would like to thank Yannick Pannier (Institut P' – UPR3346) for his help conducting the tomographies and all the LULI staff members for their technical and administrative support during the campaign. The access to the Luli2000 facility was granted by the French Lasers and Plasmas Institute (ILP – FR2707).

References

- [1] DeMichelis C. Laser interaction with solids – a bibliographical review. *IEEE J Quant Electron* 1970;6(10):630–41.
- [2] Veeres LR, Solem JC. Studies of laser-driven shock waves in aluminum. *Phys Rev Lett* 1978;40:1391–4. doi:10.1103/PhysRevLett.40.1391. <http://link.aps.org/doi/10.1103/PhysRevLett.40.1391>.
- [3] Ng A, Parfeniuk D, DaSilva L. Hugoniot measurements for laser-generated shock waves in aluminum. *Phys Rev Lett* 1985;54:2604–7. doi:10.1103/PhysRevLett.54.2604. <http://link.aps.org/doi/10.1103/PhysRevLett.54.2604>.
- [4] Eliezer S, Gilath I, Bar-Noy T. Laser-induced spall in metals: experiment and simulation. *J Appl Phys* 1990;67(2):715–24. <http://dx.doi.org/10.1063/1.345777>, <http://scitation.aip.org/content/aip/journal/jap/67/2/10.1063/1.345777>.
- [5] Boustie M, Cottet F. Experimental and numerical study of laser induced spallation into aluminum and copper targets. *J Appl Phys* 1991;69(11):7533–8. <http://dx.doi.org/10.1063/1.347570>, <http://scitation.aip.org/content/aip/journal/jap/69/11/10.1063/1.347570>.
- [6] Pirri AN. Theory for laser simulation of hypervelocity impact. *Phys Fluids* 1977;20(2):221–8. doi:10.1063/1.861859. <http://link.aip.org/link/?PFL/20/221/1>.
- [7] Nebolsine PE. Laser simulation of hypervelocity impact. In: *AIAA 14th Aerospace Sciences Meeting*; 1976.
- [8] Phipps CR, Turner TP, Harrison RF, York GW, Osborne WZ, Anderson GK, et al. Impulse coupling to targets in vacuum by KrF, HF, and CO₂ single-pulse lasers. *J Appl Phys* 1988;64(3):1083–96. doi:10.1063/1.341867.
- [9] Grün J, Decoste R, Ripin BH, Gardner J. Characteristics of ablation plasma from planar, laser-driven targets. *Appl Phys Lett* 1981;39(7):545–7. <http://dx.doi.org/10.1063/1.92788>, <http://scitation.aip.org/content/aip/journal/apl/39/7/10.1063/1.92788>.
- [10] Fabbro R, Fournier J, Ballard P, Devaux D, Virmont J. Physical study of laser-produced plasma in confined geometry. *J Appl Phys* 1990;68(2):775–84. doi:10.1063/1.346783. <http://link.aip.org/link/?JAP/68/775/1>.
- [11] Berthe L, Fabbro R, Peyre P, Tollier L, Bartnicki E. Shock waves from a water-confined laser-generated plasma. *J Appl Phys* 1997;82(6):2826–32. doi:10.1063/1.366113. <http://link.aip.org/link/?JAP/82/2826/1>.
- [12] Buresi E, Coutant J, Dautray R, Decroissette M, Duborgel B, Guillauneux P, et al. Laser program development at CEL-V: overview of recent experimental results. *Laser Part Beams* 1986;4:531–44. doi:10.1017/S0263034600002214. <http://journals.cambridge.org/article/S0263034600002214>.
- [13] Ramis R, Meyer-ter-Vehn J, Ramírez J. MULTI2D – a computer code for two-dimensional radiation hydrodynamics. *Comput Phys Commun* 2009;180(6):977–94. <http://dx.doi.org/10.1016/j.cpc.2008.12.033>, <http://www.sciencedirect.com/science/article/pii/S0010465508004505>.
- [14] Batani D, Strati F, Stabile H, Tomasini M, Lucchini G, Ravasio A, et al. Hugoniot data for carbon at megabar pressures. *Phys Rev Lett* 2004;92:1–4. doi:10.1103/PhysRevLett.92.065503. <http://link.aps.org/doi/10.1103/PhysRevLett.92.065503>.
- [15] Laporte D. Analyse de la réponse d'assemblages collés sous des sollicitations en dynamique rapide. Essais et modélisations [Ph.D. thesis]. École Nationale Supérieure de Mécanique et d'Aérotechnique de Poitiers; 2011.
- [16] Loison D, de Rességuier T, Dragon A, Mercier P, Benier J, Deloison G, et al. Skew photonic Doppler velocimetry to investigate the expansion of a cloud of droplets created by micro-spalling of laser shock-melted metal foils. *J Appl Phys* 2012;112:1–8.
- [17] Bolis C. Étude numérique et expérimentale de la séparation par chocs brefs d'interface de revêtements multicouches. Application au test d'adhérence par chocs laser [Ph.D. thesis]. Université de Poitiers; 2004.
- [18] Ecault R, Boustie M, Touchard F, Pons F, Berthe L, Chocinski-Arnault L, et al. A study of composite material damage induced by laser shock waves. *Compos Part A Appl Sci Manuf* 2013;53(0):54–64. <http://dx.doi.org/10.1016/j.compositesa.2013.05.015>, <http://www.sciencedirect.com/science/article/pii/S1359835X13001589>.
- [19] Cuq-Lelandais JP. Étude du comportement dynamique de matériaux sous choc laser sub-picoseconde [Ph.D. thesis]. École Nationale Supérieure de Mécanique et d'Aérotechnique de Poitiers; 2010.

- [20] Holmquist TJ, Wereszczak AA. Laser-induced spall in silicon carbide. In: 23rd International Symposium on Ballistics; 2007.
- [21] Holmquist TJ, Wereszczak AA. The internal tensile strength of a borosilicate glass determined from laser shock experiments and computational analysis. *Int J Appl Glass Sci* 2014;5(4):345–52. doi:10.1111/ijag.12097. <<http://dx.doi.org/10.1111/ijag.12097>>.
- [22] Hébert D, Seisson G, Bertron I, Chevalier JM, Thessieux C, Quessada JH, et al. Plate impact experiments and simulation on porous graphite. *J Phys Conf Ser* 2014;500(18):1–6. <<http://stacks.iop.org/1742-6596/500/i=18/a=182016>>.
- [23] Hébert D, Seisson G, Bertron I, Hallo L, Chevalier JM, Thessieux C, et al. Simulations of hypervelocity impacts into graphite. *Procedia Eng* 2015;103:159–64. <<http://dx.doi.org/10.1016/j.proeng.2015.04.022>>, <<http://www.sciencedirect.com/science/article/pii/S1877705815006967>>; Proceedings of the 2015 Hypervelocity Impact Symposium (HVIS 2015).
- [24] Seisson G, Hébert D, Bertron I, Chevalier JM, Lescoute E, Videau L, et al. Dynamic behavior of a porous brittle material: experiments and modeling. In: Sorensen B, Chhabildas L, editors. *Procedia Eng* 2013;58:715–23. <<http://dx.doi.org/10.1016/j.proeng.2013.05.083>>; Proceedings of the 12th Hypervelocity Impact Symposium.
- [25] Seisson G, Hébert D, Bertron I, Chevalier JM, Hallo L, Lescoute E, et al. Dynamic cratering of graphite: experimental results and simulations. *Int J Impact Eng* 2014;63(0):18–28. <<http://dx.doi.org/10.1016/j.ijimpeng.2013.08.001>>, <<http://www.sciencedirect.com/science/article/pii/S0734743X13001565>>.
- [26] Seisson G, Hébert D, Hallo L, Chevalier JM, Guillet F, Berthe L, et al. Penetration and cratering experiments of graphite by 0.5-mm diameter steel spheres at various impact velocities. *Int J Impact Eng* 2014;70(0):14–20. <<http://dx.doi.org/10.1016/j.ijimpeng.2014.03.004>>, <<http://www.sciencedirect.com/science/article/pii/S0734743X14000724>>.
- [27] Jodar B, Seisson G, Hébert D, Bertron I, Boustie M, Berthe L. Enhancement of a dynamic porous model considering compression–release hysteresis behavior: application to graphite. *Int J Impact Eng* 2015;Submitted.
- [28] Luli. Luli200. <www.luli.polytechnique.fr/accueil/les-installations/luli2000>; 2014 [accessed 09.15].
- [29] Barker LM, Hollenbach RE. Laser interferometer for measuring high velocities of any reflecting surface. *J Appl Phys* 1972;43(11):4669–75. <<http://dx.doi.org/10.1063/1.1660986>>, <<http://scitation.aip.org/content/aip/journal/jap/43/11/10.1063/1.1660986>>.
- [30] Strand OT, Goosman DR, Martinez C, Whitworth TL, Kuhlow WW. Compact system for high-speed velocimetry using heterodyne techniques. *Rev Sci Instrum* 2006;77(8):1–8. doi:10.1063/1.2336749.
- [31] Mercier P, Bénier J, Frugier PA, Sollier A, Le Gloahec Rabec M, Lescoute E, et al. PDV measurements of ns and fs laser driven shock experiments on solid targets. *AIP Conf Proc* 2009;1195(1):581–4. <<http://dx.doi.org/10.1063/1.3295205>>, <<http://scitation.aip.org/content/aip/proceeding/aipcp/10.1063/1.3295205>>.
- [32] Hébert D, Hallo L, Voisin L, Desanlis T, Galtié A, Birel B, et al. A KDP equation of state for laser-induced damage applications. *J Appl Phys* 2011;109(12):123527. <<http://dx.doi.org/10.1063/1.3600210>>, <<http://scitation.aip.org/content/aip/journal/jap/109/12/10.1063/1.3600210>>.
- [33] Loison D, de Rességuier T, Dragon A. Ballistic properties of debris produced by laser shock-induced micro-spallation of tin samples. *J Phys Conf Ser* 2014;500(11):1–6. <<http://stacks.iop.org/1742-6596/500/i=11/a=112041>>.
- [34] Lescoute E, De Rességuier T, Chevalier JM, Boustie M, Berthe L, Cuq-Lelandaïs JP. Transverse shadowgraphy and new recovery technique to investigate dynamic fragmentation of laser shock-loaded metals. *AIP Conf Proc* 2009;1195(1):1043–6. <<http://dx.doi.org/10.1063/1.3294979>>, <<http://scitation.aip.org/content/aip/proceeding/aipcp/10.1063/1.3294979>>.
- [35] Frugier PA. Quantification 3D d'une surface dynamique par lumière laser structurée en impulsion nanoseconde. Application à la physique des chocs, du millimètre au décimètre [Ph.D. thesis]. Université Paris Sud; 2015.
- [36] Poco. Poco website. <www.poco.com>; 2014 [accessed 12.15].
- [37] Sheppard RG, Morgan D, Mathes DM, Bray DJ, editors. Properties and characteristics of graphite for the EDM industry. 5th ed. Poco Graphite, Inc.; 2002.
- [38] Seisson G. Étude expérimentale et théorique de l'endommagement du graphite sous sollicitation dynamique – Application aux impacts hypervéloces [Ph.D. thesis]. École Nationale Supérieure de Mécanique et d'Aérotechnique; 2014.
- [39] Grady DE. Local inertial effects in dynamic fragmentation. *J Appl Phys* 1982;53:322–5.