



Science Arts & Métiers (SAM)

is an open access repository that collects the work of Arts et Métiers Institute of Technology researchers and makes it freely available over the web where possible.

This is an author-deposited version published in: <https://sam.ensam.eu>
Handle ID: <http://hdl.handle.net/10985/18235>

To cite this version :

Khalil AOUADI, Brahim TLILI, Corinne NOUVEAU, Aurélien BESNARD, Moez CHAFRA - Characterization of CrN/CrAlN/Cr₂O₃ Multilayers Coatings Synthesized by DC Reactive Magnetron Sputtering - In: CMSM: International Conference Design and Modeling of Mechanical Systems, Tunisie, 2019-03 - Design and Modeling of Mechanical Systems - IV. CMSM 2019, Lecture Notes in Mechanical Engineering - 2020

Any correspondence concerning this service should be sent to the repository

Administrator : scienceouverte@ensam.eu



Characterization of CrN/CrAlN/Cr₂O₃ Multilayers Coatings Synthesized by DC Reactive Magnetron Sputtering

K. Aouadi¹(✉), B. Tlili², C. Nouveau¹, A. Besnard¹, and M. Chafra³

¹ LaBoMaP, Arts et Métiers ParisTech, Rue Porte de Paris, Cluny 71250, France
aouadikhalil@hotmail.com,

{corinne.NOUVEAU,aurelien.BESNARD}@ensam.eu

² Université de Tunis, El-Manar Ecole Nationale d'Ingénieurs de Tunis,
LR-11-ES19, Laboratoire de Mécanique Appliquée et Ingénierie (LR-MAI),
1002 Tunis, Tunisia

tlilii_brahim@yahoo.fr

³ Laboratoire de Systèmes et de Mécanique Appliquée,
2078 La Marsa, Tunis, Tunisie
chafra_moez@yahoo.fr

Abstract. The CrN/CrAlN/Cr₂O₃ multilayer coatings were deposited by reactive magnetron sputtering DC on 90CrMoV8 stainless steel under various oxygen flow rates. The structure and crystalline phases are characterized by the x-ray diffractometer. Through SEM, a dense and coherent is revealed in CrN/CrAlN/Cr₂O₃ multilayer coatings. The friction and wear behaviors obtained with the ball-on-disc test show that all multilayer films exhibit a good wear resistance, especially the one with an oxygen flow rate of 10 sccm. Nevertheless, in sea water the film without a top layer of Cr₂O₃ have the lowest coefficient of friction. This behavior is attributed to the interfacial strengthening and the existence of the upper passivation layer Cr₂O₃. Adding to that, the film obtained under an oxygen flow rate of 10 sccm show the lowest grain size and the maximum hardness and elastic modulus could respectively, 45 and 417 GPa.

Keywords: Multilayer coatings · Microstructure · Hardness · Wear

1 Introduction

Oxide thin films coatings are widely used in different applications. They are known by their good oxidation resistance, good corrosion resistance, good wear resistance and good thermal properties [1, 6, 13]. However, when applied as individual coatings, oxides films haven't good properties.

To enhance the hardness of by developing super-lattice [8], some researchers studied an oxide/oxide structure. Nevertheless, in some cases, hardness has not been improved specially for Al₂O₃/ZrO₂ super-lattice [23]. This is explained either by the fact that the shear modulus of the two oxides is similar, or by the formation of an amorphous phase. In fact, Chang et al. [6] deposited an electrolytic ZrO₂/Al₂O₃ double layer coating by varying temperature. They note that the maximum hardness is about

7.2 GP under a temperature of 300 °C. Likewise, they observed that $\text{ZrO}_2/\text{Al}_2\text{O}_3$ multilayer coating has a very good corrosion behavior with a corrosion resistance which is 10 times higher than that of uncoated steel. Recently nitride/oxide super-lattice with high hardness has been successfully developed. Studies have shown that these thin films have a good hardness which can reach 45 GPa. However, these super-lattices have relatively low deposition times. Many researchers have been made to increase the deposition time of these super-lattices using reactive magnetron sputtering technique. Yue et al. [25] developed VN/SiO_2 multilayers with SiO_2 thicknesses ranging from 0.45 to 1.70 nm. They showed that when the thickness of SiO_2 is less than 1 nm, multilayer films crystallized according to the VN matrix and the two layers exhibit epitaxial growth. The hardness of this coating increases to 34 GPa. Li et al. [15] developed $\text{TiAlN}/\text{SiO}_2$ films by reactive magnetron sputtering. They found that hardness reaches his maximum (37 GPa) when the thickness of SiO_2 is about 0.6 nm. However, the variation of the thickness of the VN layer has no effect on the mechanical and structural properties.

Chromium oxide, Cr_2O_3 , is an oxide which has been used as a protective coating of cutting tools due to its outstanding wear and corrosion resistance. It's known by its high hardness and melting temperature, good resistance to wear and high oxidation temperature [5]. In order to improve the properties of chromium oxides, several researchers have studied the effect of increasing the oxygen content. Luo et al. [19] developed chromium oxides by RF magnetron sputtering by varying oxygen flow. They showed that as oxygen flow increases from 2.3 to 3.22 sccm, the hardness increases rapidly from 8 to 30 GPa. Hones et al. [10] deposited Cr_2O_3 films by RF magnetron sputtering. They showed that the grain size of chromium oxides increases linearly with the deposition temperature. However, with the increase of the oxygen level, the grain size increases initially and then remains constant for a percentage of 20% at. Similarly, they showed that the hardness significantly depends on the O_2 content since it reaches a maximum value of 31 GPa for an oxygen content between 15 and 25 at.%. Nevertheless, for an O_2 content of 30% at. The hardness is very low (2.5 GPa). Liu et al. [17] developed Cr_2O_3 films by plasma glow discharge with different oxygen flow rates (5, 10, 15 and 20 sccm) over a chromium nitride film as a top layer. They studied the corrosion resistance in an aqueous 3.5% NaCl solution. They observed that the application of a thin layer of Cr_2O_3 on the stainless steel greatly improves its corrosion resistance. Ho et al. [9] deposited Cr_2O_3 films on a CrN layer as a top layer. The adhesion test shows the appearance of cracks which is probably due to the improved hardness of Cr_2O_3 . The addition of a top layer of Cr_2O_3 also lowered the coefficient of friction.

In this work we present results multilayers films $\text{CrN}/\text{CrAlN}/\text{Cr}_2\text{O}_3$ were synthesized through using DC magnetron sputtering technique. The effect of oxygen rate on the properties of the top layer Cr_2O_3 is studied. In this study, the chemical composition, microstructure, mechanical, and tribological properties of the multilayer coatings $\text{CrN}/\text{CrAlN}/\text{Cr}_2\text{O}_3$ coatings were investigated.

2 Experimental Procedures

The CrN/CrAlN/Cr₂O₃ multilayer coatings were deposited by DC reactive magnetron sputtering (KENOSISTEC-KS40V).

Before deposition, substrates were in situ etched under argon plasma at -700 V for 10 min to ensure a better adhesion of the coatings. The base pressure prior to sputtering was lower than 2.10^{-5} Pa and heated at 300 °C. During deposition, the working pressure was 0.5 Pa.

For the deposition process, chromium and aluminum target with purity of 99.95% was used. To deposited CrN and CrAlN monolayers The Cr and Al target power was set respectively at 1500 W and 1000 W and flow rates of Ar and N₂ were 68.8 and 33.3 sccm, respectively. For the Cr₂O₃ thin films, the Cr target power was set at 1500 W. The flow rate of O was determined with the hysteresis experimental. After this experimental process, the flow rate of oxygen chosen is 0 , 10 and 20 sccm. A substrate bias voltage of -500 V is applied to all coatings during deposition. Before deposited CrN/CrAlN/Cr₂O₃ multilayer film, a thin layer about 120 nm Of Cr is deposited to ensure the adhesion of the coating.

The microstructure and surface morphology of the multilayer coatings were observed by SEM field emission (JEOL JSM 7610F). The friction coefficient is determined by rotative ball-on-disk tests. The applied fixed load was 5 N and the sliding speed was 3 cm/s. The counterpart used is an alumina ball (Al₂O₃) 6 mm of diameter. The distance slide by the ball is about 200 m. The wear volume of different coatings was calculated from 3D optical profilometer (VEECO, Wyko NT-1100) profiles. The wear volume was calculated from profilometer profiles. To be more precise, eight sections of depth in the wear track are chosen. The film surfaces topography was analyzed by atomic force microscope (AFM) (type XE Park 70) using the tapping mode. An area of $25 \mu\text{m}^2$ (5×5) was scanned. Additional analyses with the Gwyddion software were performed to determine the RMS roughness of the multilayer coatings. The coating hardness was determined by nanoindentation tests using a MTS XP Nano indenter equipped with a Vickers indenter and using the Rahmoun's model [22]. The adhesion tests were carried out by means of a micro-scratch tester (Scratch Tester Millennium 200) equipped with Rockwell spherical diamond indenter. To calculate an average adhesion value, each test is repeated three times. Figure 1 illustrates a descriptive scheme of multilayer film.

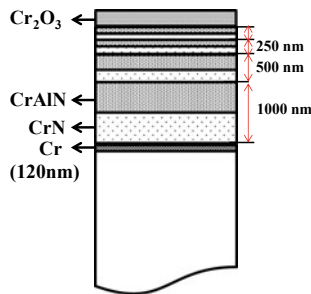


Fig. 1 Scheme of the multilayer systems

3 Results and Discussion

3.1 Microstructure and Morphology

The observation of the SEM images of the cross-section and surface morphology of the multilayer coatings CrN/CrAlN/Cr₂O₃ was carried out using a high-resolution FEG SEM. Figure 2 shows the cross-section of the multilayer films without and with a top layer of Cr₂O₃.

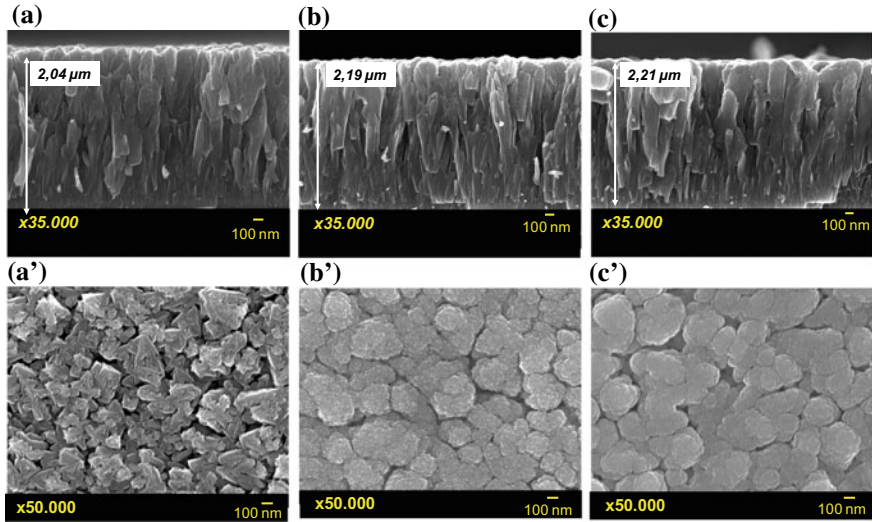


Fig. 2 Cross-sectional SEM image and surface morphology of multilayer films with a top layer of Cr₂O₃ at oxygen rate: (a, a') 0 sccm (b, b') 10 sccm (c, c') 20 sccm

All coatings represent a columnar and dense structure. The observations of the images of the surface morphology of the different multilayer coatings (Fig. 1a'–c') show that the application of a top layer of oxide leads to a variation of the shape of the columns. The film without a top layer of oxide present pyramid-like surface features. The presence of nano-pores between the columns is very visible. According to the Mahieu's model structure zones [20], this structure corresponds to the I_c zone. By adding an oxide layer with a small amount of O₂ (10 sccm), a rounded and assembled columnar tops appear and form a cauliflower-like structure. Always, according to the Mahieu's model, this structure corresponds to the zone II. This area is denser and more homogeneous than I_c area. We notice that the number of nano-pores decreases compared to the multilayer coating without top layer. By increasing the oxygen flow rate to 20 sccm, the surface is always smooth with very small columns which seem less granular than those obtained with an oxygen flow rate of 10 sccm.

The atomic force microscopy (AFM) images surface of multilayer films are presented in Fig. 2.

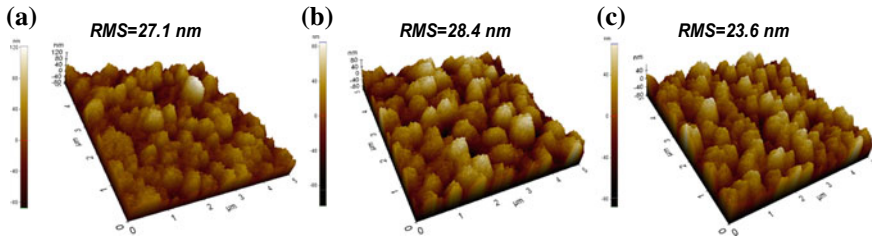


Fig. 3 Three-dimensional AFM of multilayer films with a top layer of Cr_2O_3 deposited on silicon substrate at oxygen rate: **a** 0 sccm **b** 10 sccm **c** 20 sccm

AFM images show that all multilayer films are homogeneous, dense and weakly porous. The morphology of these coatings appears to be a set of continuous mounds.

The roughness of coatings is also shown in Fig. 3. The films with a top layer of Cr_2O_3 obtained with an oxygen flow rate of 20 sccm, has the lowest roughness (23.6 nm). Generally, the growth of Cr_2O_3 films is determined by the diffusion current of Cr^{3+} ions and the oxygen rate adsorption. Also, with the increase in oxygen flow rate, the O_2 adsorption rate can moderate the Cr diffusion current and leads to the formation of a denser Cr_2O_3 layer and more smooth [17].

3.2 Mechanical Properties

The hardness and Young modulus of the multilayers films as a function of the oxygen flow rate are shown in Fig. 4.

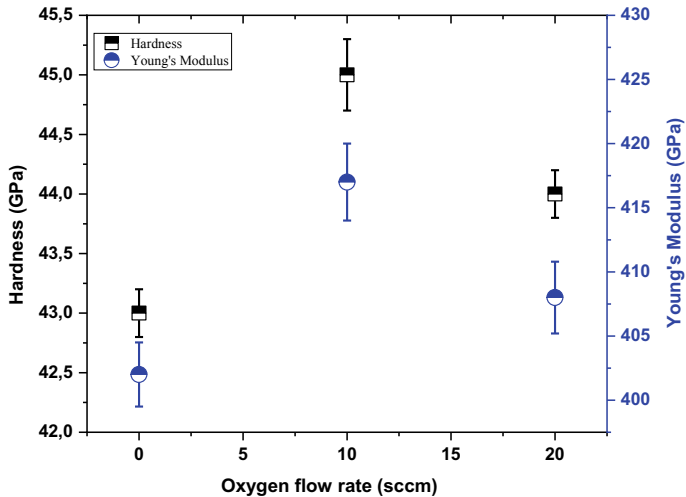


Fig. 4 Hardness and Young's modulus of multilayer films $\text{CrN/CrAlN/Cr}_2\text{O}_3$

Figure 4 show that the addition of a top layer of Cr_2O_3 obtained with 10 sccm of oxygen flow rate causes an increase in hardness and Young's modulus and it reaches values of 45 and 417 GPa. However, for the coatings without top layer the hardness is about 43 GPa and the Young's modulus is 402 GPa. This improvement can be attributed to the increase in the number of interfaces between the film of Cr_2O_3 and the CrN/CrAlN coating. Indeed, the interfaces are considered as barriers to dislocation which prohibit the growth of columnar grains through the layers. Blocking dislocations due to column-to-column discontinuity contributes to improved hardness [21]. Also, increasing hardness may be attributed to the existing of hard oxide coating as a barrier to plastic deformation [2]. Likewise, good hardness of the coatings with top layer is due to the morphology of these films. In fact, the multilayer coating without top layer presents pores, however these pores disappear in films with Cr_2O_3 top layer (Fig. 2) [7]. Indeed, pores are known by their detrimental effect on hardness. Also, the strain effect and hall-Petch strengthening can explain the increasing of the hardness [14]. By increasing the oxygen flow rate to 20 sccm, hardness decrease to 44 GPa. Similar results have been shown by Barshilia et al. [3]. This decrease can be attributed to the decrease in hardness of the Cr_2O_3 layer. In fact, Luo et al. [18] developed Cr_2O_3 films by magnetron sputtering. They varied the flow of oxygen from 2 to 2.3 sccm and showed that the hardness of chromium oxide decreases with this increase of the oxygen rate from 14 to 7 GPa. Barshilia et al. [4] attribute the decreasing of hardness to the voids appears during the growing films which influence the mechanical properties.

Figure 5 shows the Lc_1 and Lc_2 critical loads of the $\text{CrN/CrAlN/Cr}_2\text{O}_3$ multilayers films as a function of the oxygen flow rate.

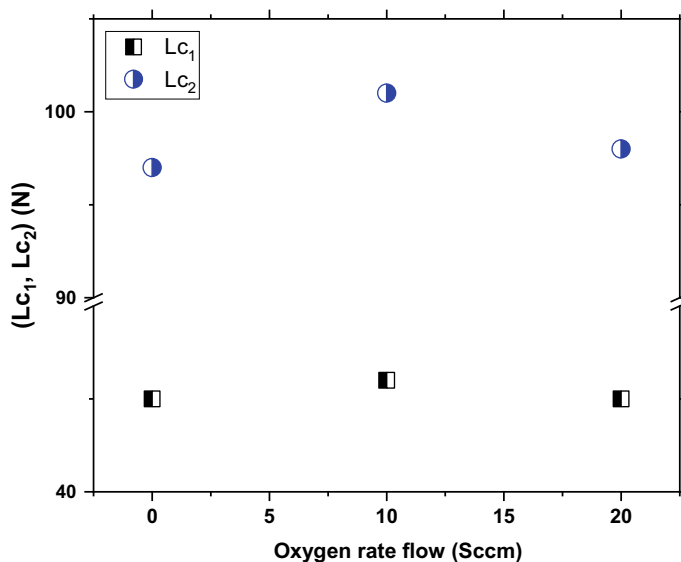


Fig. 5 Critical load of $\text{CrN/CrAlN/Cr}_2\text{O}_3$ multilayer coatings

From Fig. 5 we have noticed that the addition of a top layer of oxide (Cr_2O_3) to the CrN/CrAlN multilayers hasn't any effect on the force corresponds to the development of cracks (Lc_1). For Lc_2 , it increases when a layer of Cr_2O_3 is deposited as a top layer on the multilayer film and reaches a value of 102 N, which is a more than respectable result for layers that should be used in mechanical applications. This improvement in adhesion is attributed to the increase in the number of interfaces [11]. Indeed, the interfaces can delay the propagation of cracks. In addition, the deposition of a small thickness of a layer Cr_2O_3 can form a coherent interface with CrAlN films resulting in a significant increase of adhesion. This improvement can also be due to the improvement of the microstructure. Indeed, when comparing Fig. 2a' with Fig. 2b', c', it can be shown that there exist less pores. For the CrN/CrAlN/ Cr_2O_3 multilayer film obtained with a flow rate of oxygen of 20 sccm Lc_2 slightly decrease. This may be due to the decrease of hardness (Fig. 4). Indeed, many researchers have reported that the critical load increases linearly with the hardness of coatings [12, 24] and this confirm our results.

3.3 Coefficient of Friction

Figure 6 shows the coefficient of friction (COF) of the CrN films after sliding against Al_2O_3 balls (normal load of 5 N) as a function of oxygen flow rate.

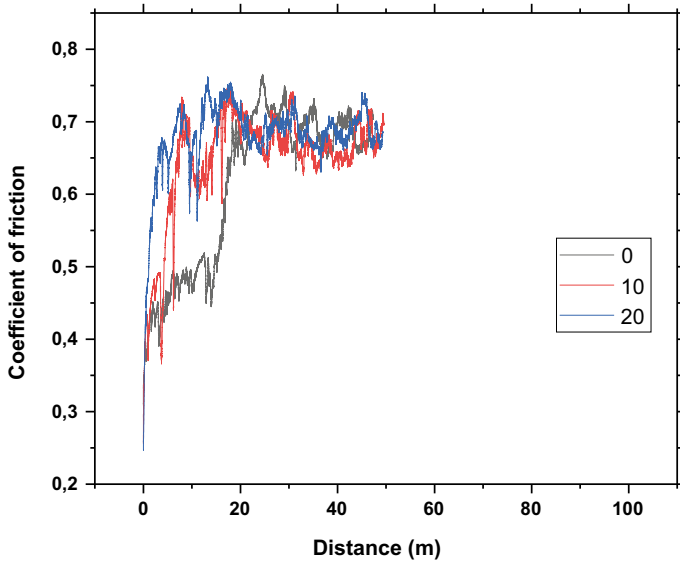


Fig. 6 Coefficient of friction of CrN/CrAlN/ Cr_2O_3 multilayer coatings

From Fig. 6 we note that the addition of a layer of Cr_2O_3 hasn't any influence on the friction behavior. The coefficient of friction of the various multilayers is about 0.69. Ho et al. [9] have shown that the deposition of a Cr_2O_3 layer on a CrN layer has reduced its coefficient of friction from 0.4 to 0.26. This is not the case for our films.

This may be due to the thinness of our oxide top layer. In addition, the friction of the ball on the surface of the film can increase the amount of oxide due to the local increase in temperature. This new oxide can weaken the bond strength between the top layer of Cr_2O_3 and the layers below. In fact, if the oxygen atoms (O) are sufficiently incorporated in the upper layer, it becomes more fragile and has cracks for a critical quantity of oxygen [16].

4 Conclusion

The main objective of the present work was to investigate the effect of a top layer of chromium oxide (Cr_2O_3) in the properties the multilayer $\text{CrN/CrAlN/Cr}_2\text{O}_3$. All films were deposited by DC reactive magnetron sputtering and the influence of the oxygen flow rate was studied. The cross section SEM image shows that all coatings present a columnar structure. For the surface morphology, multilayer without top layer exhibits pyramid-like surface features. Whereas, films with a layer of Cr_2O_3 represent a form of a cauliflower-like structure. Also, the application of a top layer improves mechanical properties. In fact, by adding a layer of Cr_2O_3 , the hardness and the adhesion increase. For tribological properties, we noted that, the application of a top layer hasn't any influence. This may be attributed to the small thickness of the layer of Cr_2O_3 .

References

1. Alirezaei S, Monirvaghefi SM, Salehi M, Saatchi A (2007) Wear behavior of Ni–P and Ni–P– Al_2O_3 electroless coatings. *Wear* 262:978–985. <https://doi.org/10.1016/j.wear.2006.10.013>
2. Alirezaei S, Monirvaghefi SM, Salehi M, Saatchi A (2004) Effect of alumina content on surface morphology and hardness of Ni– $\text{P-Al}_2\text{O}_3(\alpha)$ electroless composite coatings. *Surf Coat Technol* 184:170–175. <https://doi.org/10.1016/j.surfcoat.2003.11.013>
3. Barshilia HC, Surya Prakash M, Poojari A, Rajam KS (2004) Corrosion behavior of nanolayered TiN y NbN multilayer coatings prepared by reactive direct current magnetron sputtering process. *Thin Solid Film* 460:133–142. <https://doi.org/10.1016/j.tsf.2004.01.096>
4. Barshilia HC, Rajam KS (2008) Growth and characterization of chromium oxide coatings prepared by pulsed-direct current reactive unbalanced magnetron sputtering. *Appl Surf Sci* 255:2925–2931. <https://doi.org/10.1016/j.apsusc.2008.08.057>
5. Celik E, Tekmen C, Ozdemir I, Cetinel H, Karakas Y, Okumus SC (2003) Effects on performance of Cr_2O_3 layers produced on Mo/cast-iron materials. *Surf Coat Technol* 175:1074–1081. [https://doi.org/10.1016/S0257-8972\(03\)00361-X](https://doi.org/10.1016/S0257-8972(03)00361-X)
6. Chang C, Yen SK (2004) Characterization of electrolytic $\text{ZrO}_2/\text{Al}_2\text{O}_3$ double layer coatings on AISI 440C stainless steel. *Surf Coat Technol* 182:242–250. [https://doi.org/10.1016/S0257-8972\(03\)00862-4](https://doi.org/10.1016/S0257-8972(03)00862-4)
7. Gaillard Y, Rico VJ, Jimenez-Pique E, Gonzalez-Elipse A (2009) Nanoindentation of TiO_2 thin films with different microstructures. *J Phys D Appl Phys* 42:145305–145314. <https://doi.org/10.1088/0022-3727/42/14/145305>
8. Helmersson U, Todorova S, Barnett SA et al (1987) Growth of single-crystal TiN/VN strained-layer superlattices with extremely high mechanical hardness. *J Appl Phys* 48:1–5. <https://doi.org/10.1063/1.339770>

9. Ho Wei-Yu, Huang D-H, Huang L-T, Hsu C-H, Wang D-Y (2004) Study of characteristics of $\text{Cr}_2\text{O}_3/\text{CrN}$ duplex coatings for aluminum die casting applications. *Surf Coat Technol* 178:172–177. <https://doi.org/10.1016/j.surfcoat.2003.06.017>
10. Hones P, Diserens M, Lévy F (1999) Characterization of sputter-deposited chromium oxide thin films. *Surf Coat Technol* 121:277–283. [https://doi.org/10.1016/S0257-8972\(99\)00384-9](https://doi.org/10.1016/S0257-8972(99)00384-9)
11. Huang S, Chen S, Kuo Y et al (2011) Mechanical and tribological properties evaluation of cathodic arc deposited CrN/ZrN multilayer coatings. *Surf Coat Technol* 206:1744–1752. <https://doi.org/10.1016/j.surfcoat.2011.10.029>
12. Ichimura H, Rodrigob A (2000) The correlation of scratch adhesion with composite hardness for TiN coatings. *Surf Coat Technol* 126:152–158. [https://doi.org/10.1016/S0257-8972\(00\)00541-7](https://doi.org/10.1016/S0257-8972(00)00541-7)
13. Kim H, Koh Y, Kim H (2000) Densification and mechanical properties of B_4C with Al_2O_3 as a sintering aid. *J Am Ceram Soc* 65:2863–2865. <https://doi.org/10.1111/j.1151-2916.2000.tb01647.x>
14. Kong M, Wu X, Huang B, Li G (2009) Epitaxial growth and superhardness effect of TiN/AlON nanomultilayers synthesized by reactive magnetron sputtering technology. *J Alloy Compd* 485:435–438. <https://doi.org/10.1016/j.jallcom.2009.05.133>
15. Li W, Liu P, Wang J et al (2011) Microstructure and mechanical properties of TiAlN/SiO₂ nanomultilayers synthesized by reactive magnetron sputtering. *Mater Lett* 65:636–638. <https://doi.org/10.1016/j.matlet.2010.11.073>
16. Lin C, Tsai Y, Duh J (2010) Effect of grain size on mechanical properties in CrAlN/SiNx multilayer coatings. *Thin Solid Films* 518:7312–7315. <https://doi.org/10.1016/j.tsf.2010.04.100>
17. Liu H, Tao J, Xu J, Chen Z, Gao Q (2009) Corrosion and tribological behaviors of chromium oxide coatings prepared by the glow-discharge plasma technique. *Surf Coat Technol* 204:28–36. <https://doi.org/10.1016/j.surfcoat.2009.06.020>
18. Luo F, Gao K, Pang X, Yang H, Qiao L, Wang Y (2008) Characterization of the mechanical properties and failure modes of hard coatings deposited by RF magnetron sputtering. *Surf Coat Technol* 202:3354–3359. <https://doi.org/10.1016/j.surfcoat.2007.12.020>
19. Luo F, Pang X, Gao K, Yang H, Wang Y (2007) Role of deposition parameters on microstructure and mechanical properties of chromium oxide coatings. *Surf Coat Technol* 202:58–62. <https://doi.org/10.1016/j.surfcoat.2007.04.066>
20. Mahieu S, Depla D (2009) Reactive sputter deposition of TiN layers: modelling the growth by characterization. *J Phys D Appl Phys* 42:053002. <https://doi.org/10.1088/0022-3727/42/5/053002>
21. Mori T, Fukuda S, Takemura Y (2001) Improvement of mechanical properties of Ti/TiN multilayer film deposited by sputtering. *Surf Coat Technol* 140:122–127. [https://doi.org/10.1016/S0257-8972\(01\)01021-0](https://doi.org/10.1016/S0257-8972(01)01021-0)
22. Rahmoun K, Iost A, Keryvin V, Guillemot G, Chabane Sari NE (2009) A multilayer model for describing hardness variations of aged porous silicon low-dielectric-constant thin films. *Thin Solid Films* 518:213–221. <https://doi.org/10.1016/j.tsf.2009.07.040>
23. Sproul WD (1996) Reactive sputter deposition of polycrystalline nitride and oxide superlattice coatings. *Surf Coat Technol* 87:170–176. [https://doi.org/10.1016/S0257-8972\(96\)02977-5](https://doi.org/10.1016/S0257-8972(96)02977-5)
24. Wang Z, Zhang D, Ke P, Liu X, Wang A (2015) Influence of substrate negative bias on structure and properties of TiN coatings prepared by hybrid HIPIMS method. *J Mater Sci Technol* 31:37–42. <https://doi.org/10.1016/j.jmst.2014.06.002>
25. Yue J, Liu Y, Li G (2008) Microstructure and mechanical properties of VN/SiO₂ nanomultilayers synthesized by reactive sputtering. *Mater Lett* 62:1621–1623. <https://doi.org/10.1016/j.matlet.2007.09.040>