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To cite this version :

Thomas POTTIER, Guénaél GERMAIN, Madalina CALAMAZ, Anne MOREL, Dominique COUPARD - Sub-millimeter measurement of finite strains at cutting tool tip vicinity - Experimental Mechanics - Vol. 54, n°6, p.1031-1042 - 2014

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Sub-Millimeter Measurement of Finite Strains at Cutting Tool Tip Vicinity

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Abstract The present paper details a simple and effective experimental procedure dedicated to strain measurement during orthogonal cutting operations. It relies on the use of high frame-rate camera and optical microscopy. A numerical post-procedure is also proposed in order to allow particle tracking from Digital Image Correlation (DIC). Therefore strain accumulation within finite strains framework is achieved. The significant magnitude of the calculated strains is partially due to a singular side effect that leads to local material disjunction. The strain localization in the Adiabatic Shear Band (ASB) exhibits different strain paths at various locations along this band and a non-linear evolution of the strain accumulation. A focus is made on the formation mechanisms of serrated chips obtained from Ti6Al4V titanium alloy. The side observation performed during this work allow to proposed three possible scenarios to explain this very phenomenon.

Keywords Orthogonal cutting · Digital image correlation · Chip segmentation · Adiabatic shear band · Machining

Introduction

To achieve high performance machining, it is of high interest to collect data about the chip formation mechanisms. They can help to understand and improve the integrity of the machined surface, e.g., roughness, geometrical dimensions, microstructure, residual stresses, deformation levels, as well as the wear resistance of the tool [1]. To obtain quantitative data concerning transient strain, strain rate and temperature fields in very small areas (the primary Z_I , secondary Z_{II} and tertiary Z_{III} deformation zones), numerical simulations have been developed which enable these parameters and their evolution to be evaluated. The results only have meaning if suitable friction laws [2, 3] and material models [4–6] are used. They are currently validated merely by macroscopic data, such as cutting forces, chip morphology and tool/chip contact length. Thus, details on the behavior in the cutting zone are still lacking due to the difficulty, through experimentation, for industrial cutting parameters, to obtain local data that may link with the simulations.

Direct measurements of deformation field parameters, such as velocity of material flow and strain, have mostly been performed by quick-stop devices (QSDs). The fundamental idea is to retract the tool from the workpiece [7] or to accelerate the workpiece to separate it from the tool [8] as rapidly as possible, in order to *freeze* the process. Komanduri and Brown [9] investigated the mechanics of chip segmentation in machining of a ferrite-pearlitic steel using an explosive QSD. They found that the chip segmentation process arises as a result of instabilities in the cutting process. Jaspers and Dautzenberg [7] obtained clear photographs of chip roots on an AISI 1045 steel. Following the shear strain representation proposed by [10, 11] they predicted strain in the primary shear zone. Another way to

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estimate strains is to mark the material with micro grids inscribed upon the side of the workpiece by mechanical abrasion [12], chemical abrasion or photo-etching lithographic printing methods as used by [13]. The velocity and strain values are estimated from the micro grids distortion. [14] proposed a variation of the grid deformation technique, which could be used in machining, using steel specimens that contained pearlite ‘stringers’. The stringers served as intrinsic internal grids whose distortion can be measured to estimate the strain. However a major drawback of QSDs is the time necessary to interrupt the cutting process. Even if improvements have been made in devices design [7], this delay time can trigger a modification of the deformation state in the cutting zone. Moreover experiments are very time-consuming since achieving a complete restitution of the formation sequence requires quick stops at various deformation stages.

An alternative to QSDs is the use of high-speed cameras. Indeed new performances in terms of acquisition frequencies, frame rate, exposure time, image resolution and signal-to-noise ratio, now allow to work close to industrial cutting speed. Pujana et al. [13] used such a technique on a square grid marked 42CrMo4 steel. They managed to analyze the deformed squares at a cutting speed up to 300 *m/min*, deduced strains and consequently strain rates in the primary shear zone on the hypothesis of plane strain conditions. Nevertheless, at such cutting speed, the capture apparatus is only able to render 1.5 images per segment and thus only provides a glance at a more complex process. More recently, [15] proposed a method to replace the grids using flow line shape analysis. Four lines were drawn parallel to the cutting direction on the side of the workpiece using a mechanical scratching method. The velocity, strain rates and strain distributions were calculated from the mathematical expression of the streamline functions. Orthogonal cutting tests were conducted up to 1020 *m/min*. But a high feed of 0.84 *mm* had to be selected to guarantee a sufficient spatial resolution and avoid an underestimation of strain. The use of Digital Image Correlation (DIC) has also been reported to analyze the cutting zone. Hijazi and Madhavan [16] have developed a complex dedicated device composed of four non-intensified digital cameras set in dual frame mode to perform a 4 images acquisition at 1 MHz.

In the present paper, DIC technique has also been chosen. It is performed from the use of a single high frame rate imager and optical microscopy. Such experimental apparatus allows to monitor strain at several instants during the chip formation process. The following therefore presents first the experimental procedure. Details are given on cutting configuration and observation device. Then the DIC post-processing is described. Its accuracy is discussed. A following section is dedicated to the numerical estimation of strain from displacement fields. Finally the obtained results

are presented and discussed. Mechanisms of chip formation are then proposed based on these experimental data.

Experimental Setup

Material and Cutting Characteristics

The cutting configuration is chosen to be orthogonal. Cutting tests are performed on a planer machine GSP 2108 R.20 which allows varying the cutting velocity between 6 and 60 *m/min*. Uncoated carbide inserts with a tool holder manufactured for the planer machine (rake angle : 0°) are used. The tool is fixed and the cutting speed is applied to the machine table on which the workpiece is set up, along a direction perpendicular to the cutting edge (orthogonal cutting operation). The workpiece moves perpendicular to the observation axis.

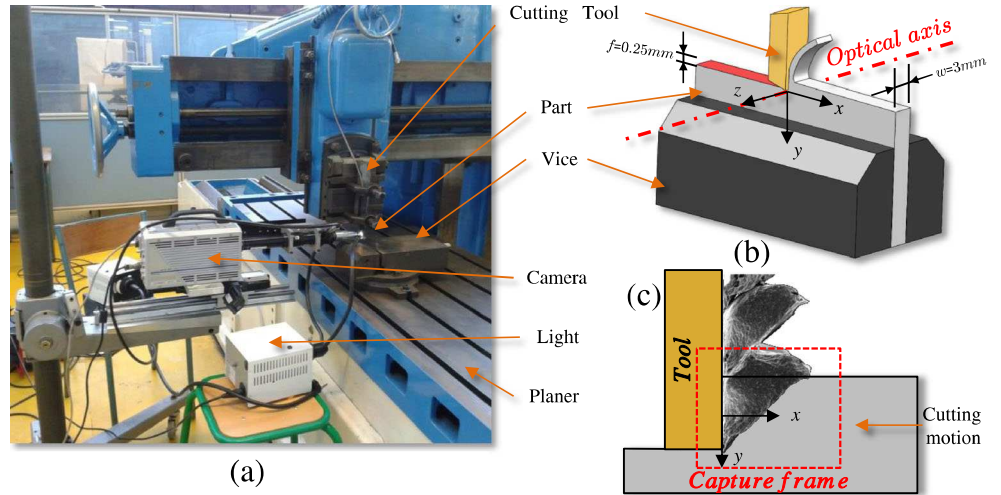
The width of cut ($w = 3 \text{ mm}$) is given by the dimensions of the Ti6Al4V workpiece ($100 \times 60 \times 3$). A cutting depth of $f = 0.25 \text{ mm}$ is selected. This choice results from a balance between the need of large shear zone (lower magnification required) and the need to limit the out-of-plane effects (optical depth of field). The instruction of cutting speed is set to $V_c = 6 \text{ m/min}$. These cutting parameters are expected to generate serrated chips (see Fig. 1c) on a material well known for segmenting even at low cutting speeds [9, 18].

Optics and Field Measurements

One of the main improvement of the present study is the use of high magnification optics allowing the capture of sub-millimeter zones of interest. For instance, in [19] the use of a 3X optical microscope allows a pixel size of 8.2 μm at 250 *fps*, in [20] the use of a high definition camera and a similar magnification allows a pixel size of 1.4 μm at 2000 *fps*. The work of [13] proposes the use of a 12X video-microscope for a pixel size of 4.9 μm at 25000 *fps*. Finally, [16] proposes to use 4 standard CCD sensors triggered successively in order to obtain 4 images with an inter-frame time of 0.001*ms* (equivalent to 1*Mfps*) at very high magnification (pixel size: 0.27 μm). However, monitoring the chip formation process require a complete sequence of images. Therefore, the proposed capture process relies on a Photron Fastcam APX-RS camera.

The spatial resolution is a critical parameter in investigating large strain gradients, especially when localization phenomena are involved. The use of high speed camera limits quite drastically the number of measured pixels. Subsequently, the link between frame rate and frame resolution is responsible for limiting the maximum cutting speed of an observation. The choice of the capture parameters is

Fig. 1 (a) Experimental apparatus [17]. (b) Geometry of the cutting and coordinates system. (c) Side view of the scene showing the camera capture frame and the serrated chip (SEM view overlaid)



governed by the will to obtain several images of one segment formation. In order to keep a sufficient spatial resolution, the acquisition is set at $f = 18000 \text{ fps}$ with an exposure time of $6.6 \mu\text{s}$. This setting ensures a resolution of 384×352 pixels.

A tunable optical video-microscope is used and its magnification (M_t) is set to 35X. The field of view is then $650 \times 600 \mu\text{m}$, with a pixel size of $1.65 \mu\text{m}$. With such settings, a cutting speed of $V_c = 6 \text{ m/min}$ provides about 45 images of one segment formation (assuming that the width of a segment can roughly be approximated by $f = 0.25 \text{ mm}$). One should also notice that such an optical apparatus is responsible for optical aberrations of unknown nature. Under this condition, one should be careful in the use of DIC when estimating the correlation between a reference (undeformed) image and a deformed one that has undergone serious displacement within the aberration field. Accordingly, iterative correlation should be preferred (see section “[Calculation Parameters](#)”).

Lighting the scene is a non-trivial issue and deserve to be discussed further here. The presented images are captured using a 200W halogen light source and an optic-fiber light guide. Set at full power this device is not sufficient to capture images with an exposition time of $6.6 \mu\text{s}$. Actually the beam splitter embedded within the video-microscope is responsible for a significant loss of the incoming light flux (indeed the half of it). Therefore the light guide was positioned outside of the microscope tube, about 5 mm away from the observed scene. The approximated angle of incidence is 30° . Nevertheless, lighting remains one of the main constraint in high-speed imaging especially under microscopic conditions where over-exposure and/or under-exposure may become significant issues.

Digital Image Correlation

Calculation Parameters

The whole captured sequence is made of 2568 frames representing the formation of 52 chip segments. However, only one segment formation has been selected for post-processing purpose. Hence, 45 images are investigated. Each image is post-processed through Digital Image Correlation (DIC) in order to retrieve the incremental displacement field. For this purpose, each image is split in square elements that create a virtual grid upon the sample surface (denoted $\mathcal{M}_0 = \{x_0; y_0\}$). The resolution of this grid (the gauge length) is set to 10×10 pixels, corresponding to $17 \times 17 \mu\text{m}^2$. The correlation process consists in looking for the most probable deformed pattern in the neighborhood of each node of this grid in terms of grey level. The displacement fields of each element are then assessed by the means of a bi-linear interpolation. Finally, the displacement at image n is assessed by correlating the n th image with the previous image ($n-1$)th. A zero-mean formulation of the correlation parameter is used in order to prevent from error due to non-constant lighting. The correlation parameter used in the present study are summarized in Table 1. Calculations are performed using 7D software [21].

Table 1 Main parameters of the digital image correlation

Grid size	Pattern size	Grey level interpolation	Displacement fields interpolation
10×10	10×10	bicubic	bilinear

The choice of incremental correlation relies on several considerations. Firstly, as mentioned above, the optical aberration leads to a significant error when large displacements are involved [22] and comparing image n and $n - 1$ instead of n and 1 decrease such displacements. Secondly, in presence of very significant strains, the likeness of image no.1 and n is poor and the correlation process cannot return information over the whole correlation grid \mathcal{M}_0 . In other words, the material fed in the right hand side of image n has no counter part in image 1 for it is still out of the frame at that time.

Displacement Uncertainties

Estimating the measurement uncertainties of speckle-related DIC techniques, is known to be a complex task. Lots of studies have been addressed in this field and the point of the present paper is not to discuss any further in this matter. However, the poor quality of the obtained images (low resolution, optical aberration, camera measurement noise, unpainted surface) give raise to the question of the accuracy/noise of the DIC obtained displacement fields. Among the several parameters impacting the DIC accuracy, speckle quality and pattern size are often addressed as the most critical ones [23, 24].

The benchmark speckles generated numerically in [23] offer a fast way to qualitatively investigate a given speckle. Indeed the estimation of the autocorrelation of the texture allows a comparison with the 3 proposed speckle. Figure 2(a) show the texture and the autocorrelation surface of a 10×10 pattern. Figure 2(b) depicts a comparison of the speckle under investigation with those proposed in [23]. Hence, it can be seen that the obtained texture exhibits a sufficient quality to ensure a proper DIC (though between standard and coarse).

Another approach in evaluating speckle quality is the use of rigid body motion [25]. A non-deformed zone of the image is investigated over 5 successive images and the displacement norm is monitored. The average displacement in the zone is then subtracted. Subsequently, the residual stands for the noise generated by speckle imperfection. Alike any random variable, it can be characterized by its standard deviation. Figure 2(c) shows that for the chosen pattern size (10×10) the displacement uncertainties can be assumed to be about $0.0181 \text{ pixels} \approx 0.031 \mu\text{m}$ (say a signal-to-noise ratio of 165 in the non-deformed zone).

Finally, the standard deviation of the measured displacement can also be estimated through the Mean Intensity Gradient (MIG) of the speckle pattern [26]. It is shown that under some assumptions, the random error is given by:

$$\text{std}(u) \approx \frac{\sqrt{2}\sigma}{n \times \delta_f} \quad (1)$$

where σ is the standard deviation of the measurement noise, N the subset size and δ_f the MIG. In the present study the MIG equals $\delta_f = 9.22$ and the noise ($\sigma = 1.025 \text{ pixel}$) is evaluated from the subtraction of two consecutive images captured prior to any motion of the sample. Hence the standard deviation of the measured displacement is approximated by: $\text{std}(u) \approx 0.0157 \text{ pixels} \approx 0.027 \mu\text{m}$ which is consistent with the rigid motion approach.

Out-of-plane Motion

Unlike the work presented in [19], the cutting geometry does not impose constraint on the observed side of the chip. It means that the chip is free to swell along the optical axis of the microscope and therefore impose accounting for the out-of-plane deformation in the sheared section. The magnitude

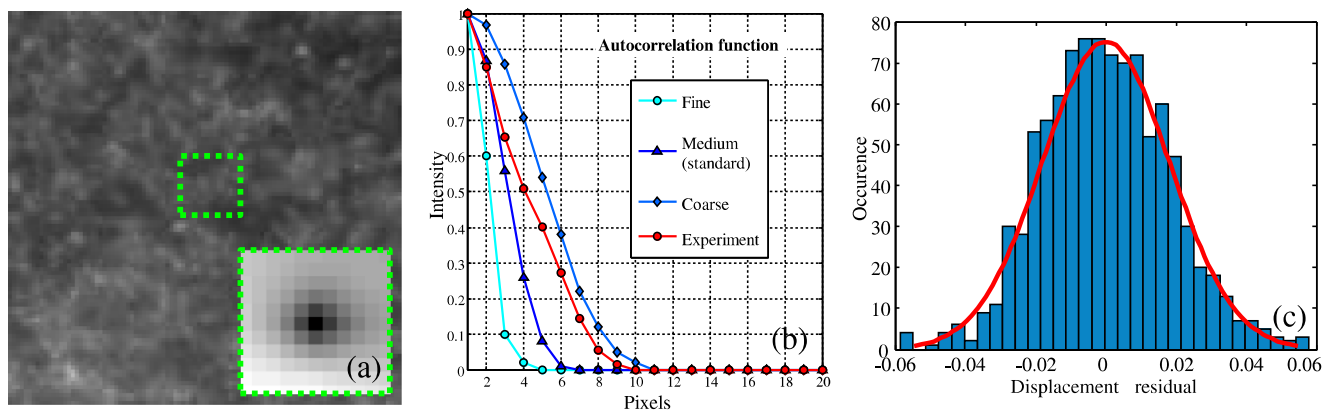


Fig. 2 (a) Image detail window 100×100 . and autocorrelation zoom 10×10 . (b) Associated centered and normalized autocorrelation function radius at half height [23]. (c) Distribution of normalized displacement vector norm

of the out-of-plane deflection is estimated from either SEM-MEX technique (stereoscopic 3D reconstruction Fig. 3(a) and chromatic confocal surface metrology (Altmet 500). The approximated magnitude of the out-of-plane deflection is $\Delta z \approx \pm 35 \mu m$ for both measurements. However, one should notice that this measurement is performed *post-mortem* and does not account for the elastic deformation of the chip which is then neglected.

Several studies have been addressed on the estimation of DIC error due to out-of-plan motion and theoretical models enable the assessment of the errors raised from such motion. The work of [27] proposes both a single lens model and a telecentric model to account for the virtual magnification of objects moving along the optical axis. The nature of the objective in used in this study (infinitely corrected plan-apochromatic) disable the used of any of these models. Hence, the error estimation has been performed from experimental means. A planar speckled plate was moved along the optical axis and a picture was captured every $10 \mu m$ (within a range of $-40 \mu m$ to $+40 \mu m$ from the focus plane). DIC was then used to estimate the virtual strains due to out-of-plane motion. Figure 3 shows that the error in terms of strains is maximized by $\varepsilon_{max} \approx 0.0055$. Since the swelling of the chip is not homogeneous over the chip segment, some regions are more affected by this error than others. However, the small magnitude of such error compared to the estimated strains (see section “Cumulated Strain in a Segment”) leads to consider it as negligible in the presented study case. One should notice that this error source can be minimized by the use of telecentric optics as discussed in [27] and [28].

Strain Calculation

Finite Strain Framework

The main difficulty in estimating displacement and strain fields relies on the use of incremental correlation which

disable the tracking of a given material point. For every image, the increment of displacement is given at the undeformed/reference location as

$$\begin{cases} \Delta U_x(x_0, y_0, k) \\ \Delta U_y(x_0, y_0, k) \end{cases} \quad (2)$$

where (x_0, y_0) are the grid coordinates (identical for every image pair) and k is the image number. This only information does not enable the estimation strains (whether in initial or final configuration) since material tracking can not be achieved, cumulating strain and different location is just not right. The evaluation of the deformed coordinates $\{x_k; y_k\}$ at every step/images of the deformation process is performed through triangular bi-linear interpolation.

$$\begin{cases} x_k = x_{k-1} + \Delta U_x(x_{k-1}, y_{k-1}, k) \\ y_k = y_{k-1} + \Delta U_y(x_{k-1}, y_{k-1}, k) \end{cases} \quad (3)$$

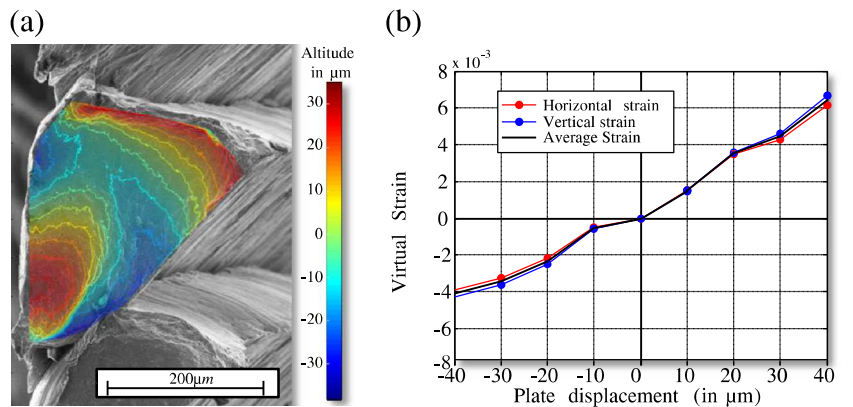
with

$$\begin{cases} \Delta U_x(x_{k-1}, y_{k-1}, k) = \sum_{i=1}^3 \phi_i(x_{k-1}, y_{k-1}) \times \Delta U_x(x_0, y_0, k) \\ \Delta U_y(x_{k-1}, y_{k-1}, k) = \sum_{i=1}^3 \phi_i(x_{k-1}, y_{k-1}) \times \Delta U_y(x_0, y_0, k) \end{cases} \quad (4)$$

where the ϕ_i are the classical triangular shape functions. The knowledge of displacement increments offers a straight forward access to the velocity fields V_x and V_y . Assuming a constant capture rates of the images, it therefore comes $V_x = \Delta U_x$ and $V_y = \Delta U_y$. Then the components of the strain rate tensor are:

$$\begin{cases} \mathbb{D}_{xx}(x_k, y_k, k) = \frac{\partial V_x(x_k, y_k, k)}{\partial x_k} \\ \mathbb{D}_{yy}(x_k, y_k, k) = \frac{\partial V_y(x_k, y_k, k)}{\partial y_k} \\ \mathbb{D}_{xy}(x_k, y_k, k) = \frac{1}{2} \left(\frac{\partial V_y(x_k, y_k, k)}{\partial x_k} + \frac{\partial V_x(x_k, y_k, k)}{\partial y_k} \right) \end{cases} \quad (5)$$

Fig. 3 (a) SEM image of the chip side, overlaid with the measured altitude map. (b) Error estimation on strains due to out-of-plane motion



The cumulated displacement at material point location is then used to calculate the updated Lagrangian strain tensor as:

$$\mathbb{E}(x_k, y_k, k) = \mathbb{D}(x_k, y_k, k) + \sum_{m=1}^k \sum_{i=1}^3 \phi_i(x_k, y_k) \times \mathbb{D}(x_m, y_m, m) \quad (6)$$

where $1 < k < N_f$ and N_f is the number of frame in the sequence. \mathbb{E} is then the cumulated strain with respect to the initial configuration but expressed over the current deformed grid $\{x_k; y_k\}$ (Updated Lagrangian Configuration). Such a formulation allows a straight forward comparison with standard Finite-Element commercial codes and is therefore well suited for model validation and/or identification.

Modal Derivation

The major issue related to the implementation of equation (6) comes from the noisy nature of displacements obtained by DIC approaches which lead to significant signal-to-noise ratio (SNR) when derived. Such numerical instabilities prevent from direct derivation of displacements when these latter exhibit high SNR, e.g.: natural speckle, small spatial resolution, inconsistent lighting, strain localization.. All of these problems arises with the combined use of high-speed photography and high magnification. Hence, filtering method should be considered and implemented.

In the present study, a modal projection method is used [29]. This method consist in projecting the displacement fields within a modal basis and build the strain fields from a weighted sum of modal space-derivative. The displacement increment is written as:

$$V_x(x_k, y_k, k) = \sum_{p=1}^N \lambda_p(k) Q_p(x_k, y_k) \quad (7)$$

where N is the truncation order (the number of modes used for reconstruction) here set to 350, λ_p the modal coordinates and Q_p the modal vectors. These latter are here evaluated from dynamics vibration theories. Indeed, prior to any calculation, the basis $\mathfrak{B} = \{Q_1, Q_2 \dots Q_N\}$ is calculated by solving the classical dynamics problem:

$$\left(M^{-1} K - \frac{1}{\omega_i^2} \mathbb{I} \right) Q_i = 0, \quad (8)$$

where M is the mass matrix, K the stiffness matrix and ω_i the modal pulsation. The problem is solved using Finite Element discretization over a mesh build using one node per pixel of the captured image.

Once the velocity fields are projected within \mathfrak{B} the linearity of the derivative operator states that:

$$\mathbb{D}_{ij}(x_k, y_k, k) = \frac{\partial V_i}{\partial x_j} = \sum_{p=1}^N \lambda_p(k) \frac{\partial Q_p(x_k, y_k)}{\partial x_j} \quad (9)$$

This approach, though uncommon in strain derivation applications, has proved its worth in various noise related problems [30–32].

Results and Discussion

Cumulated Strain in a Segment

Figure 4 shows the shape of the displacement and principal strain fields during chip segment formation. Adiabatic shear bands (ASB) are clearly highlighted by significant strain magnitudes (up to 3) at these locations. In addition, it can be noticed that the inner part of the segment does not significantly deforms (columns *c* and *d*) image no. 45).

Moreover, the actual cutting speed can be evaluated from the actual displacements increments measured in an undeformed zone of the image. For this purpose the displacement norm within the lower right side of the image (see Fig. 4(a)) is averaged and gives $V_c \approx 5.63 \text{ m/min}$ which is slightly lower than the instruction ($V_c = 6 \text{ m/min}$).

As mentionned in the above, the measured strains are significant. However, a close monitoring of the image sequence shows the outbreak of a localized black line (Fig. 5(a)). In order to determine the nature of this phenomenon, complementary SEM investigations have been carried out. As shown in Fig. 5(b), a material disjunction (or *crack*) appears on the free side of the chip.

The fact that, at some point of the deformation process, the material splits in segments leads to reconsider the strains magnitude assessment. The DIC process such as presented in this paper keeps cumulating strains even though material undergoes segmentation. Hence, the final strain magnitude within ASB is not relevant as such from a continuum mechanics standpoint. The values (up to 3) as depicted in Fig. 4(cd) are indeed greatly overestimated. It is then required to monitor the outbreak of this material disjunction.

For this purpose, the study of the strain rates within the ASB as depicted in Fig. 6 provides a straight forward way to monitor the crack propagation. From the curves presented in Fig. 6(b) it is noticeable that a segment is formed from three successive stages.

Stage 1 – The strains are concentrated at the tooltip vicinity. The inner part of the chip slowly deforms (Fig. 4(d)). During this stage an out-of-plane swelling of the segment is clearly visible. It is fully formed around image no.30.

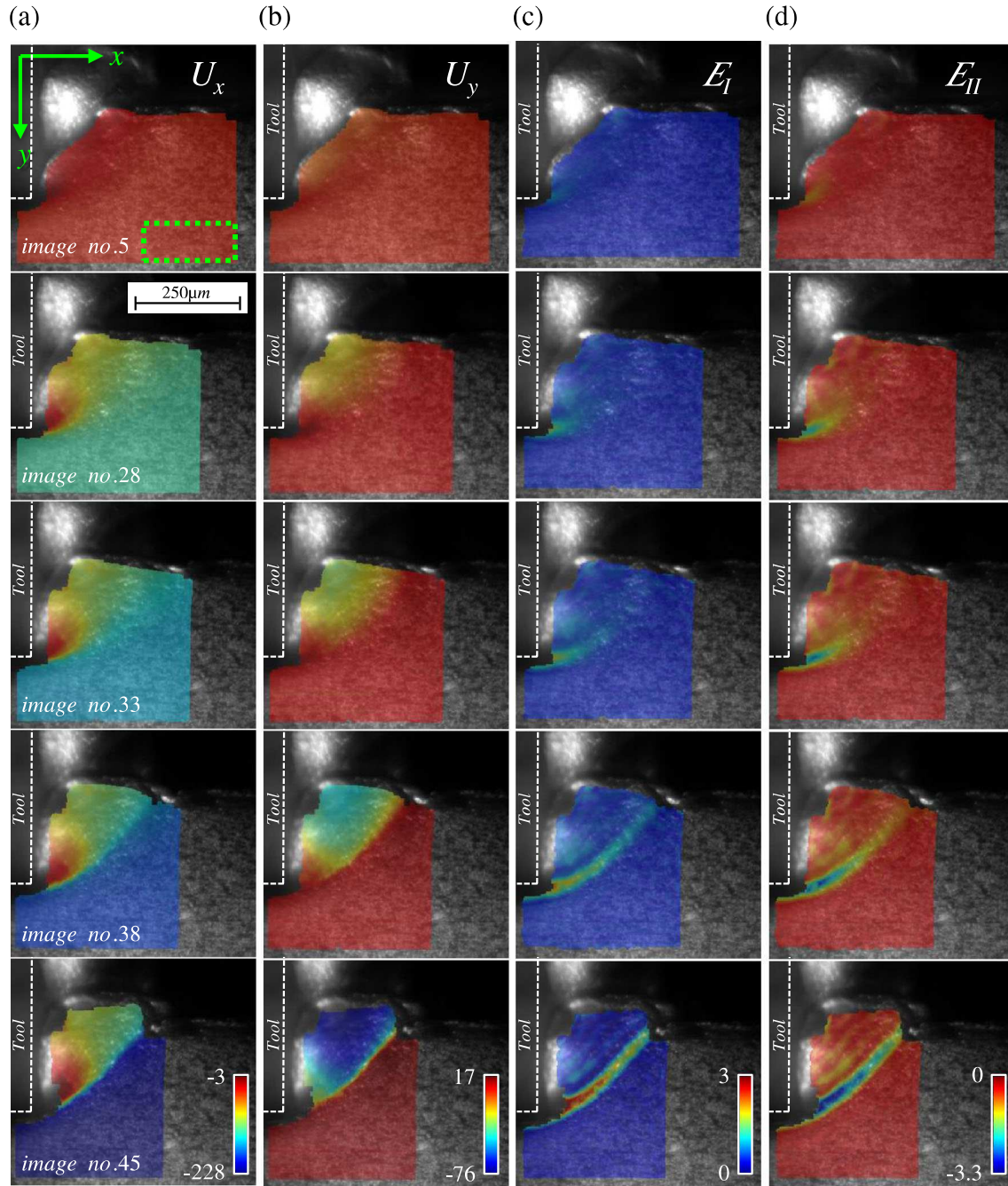
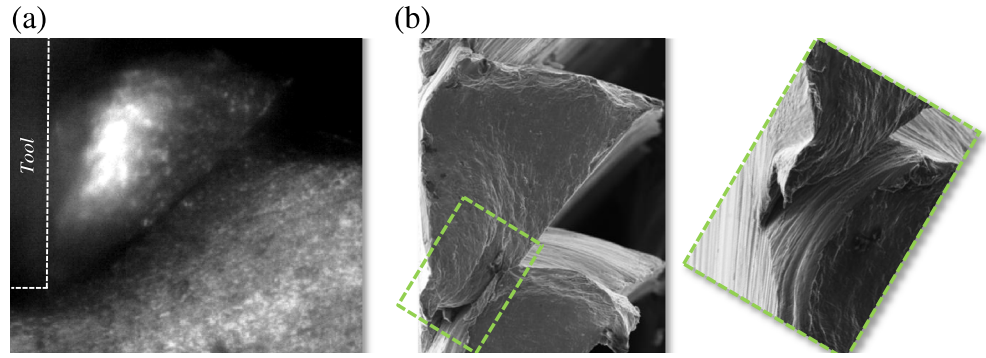


Fig. 4 Displacements and principal strain fields at five time steps. The total elapsed time is 2.2 ms corresponding to the formation of one segment. (a) Horizontal displacement (in μm). (b) Vertical displacement (in μm). (c) Major strain. (d) Minor strain. The green rectangle represent the zone where displacements are averaged for the cutting speed estimation

Stage 2 – The strain rapidly cumulates along the ASB from bottom to top. The strain rates reach significant magnitudes (up to 4.10^3 s^{-1}) and lead to a material failure (this latter point is specifically discussed in section “[Chip Segmentation Process](#)”).

Stage 3 – During the last images, strain rates stabilize, the segment is fully formed and slips on both the cutting face and the next segment (to be formed). Indeed, since material failure occurs the segment is animated with a rigid body motion. At this point, cumulating strains is

Fig. 5 (a) Image captured during segment formation (contrast modified to enhance black line visibility). (b) SEM view of the chip side and detail view of the crack



no longer valid from a continuum mechanics standpoint.

Figure 6(b) also shows that the times spent for stage 2 goes shorter when moving from point 1 to point 3. In other words, the material failure accelerates from the tooltip to the free surface. Considering the decreasing of the resisting cross-section, this results is indeed expectable.

Figure 7 shows the last measured state of strain before material failure (at the end of stage 2) for 19 points along the ASB. It can be seen that the deformation process that leads to failure slightly differs from one end of the ASB to the other. Different strain paths are observed and can be sorted in three categories:

Zone Z_{IA} : Nearby the tooltip, the ASB deforms mainly in compression with significant magnitudes. This process is slow and start very early in the sequence (Fig. 6(b), point P_1 and Fig. 7(b)).

Zone Z_{IB} : Moving away from the tool tip, the ASB deforms in compression/shear but with lower magnitudes. The strain rates curves in Fig. 7(c) show an acceleration of the phenomenon: the material is less deformed at failure in this zone but reaches it faster.

Zone Z_{IC} : Finally, around the free surface, the state of strain turns into pure shear. At this time of the sequence

the cutting speed reaches a cycle maximum. It is noticeable that the resisting cross section tends toward its minimum at the same time. It seems plausible that the two observations are related, however only a rigorous measurement of the cutting force may validate such hypothesis.

The study of strain rates enables to follow the crack tip when propagating along the ASB. This criterion, though unautomated yet, corroborates the visual observations of the images sequence. It allows to limit the strain accumulation and evaluate strains at failure. These latter appears to be heterogeneous and lower than expected by numerical calculation [33, 34]. These observations points the need of a better understanding of the decohesion phenomenon and the segmentation process.

Chip Segmentation Process

The development of numerical models of machining operations has become significant in the last decade and the modeling of the segmentation phenomena is a key issue in the validation of material models (either for constitutive

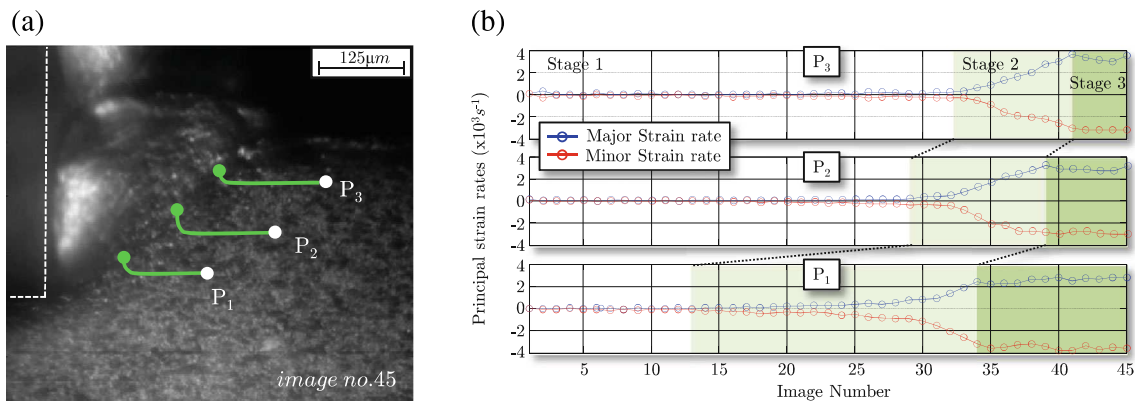


Fig. 6 (a) Initial and final position of the three investigated points (P_1 , P_2 and P_3). (b) Principal strain rates evolution over the 45 images of the film (at P_1 , P_2 and P_3)

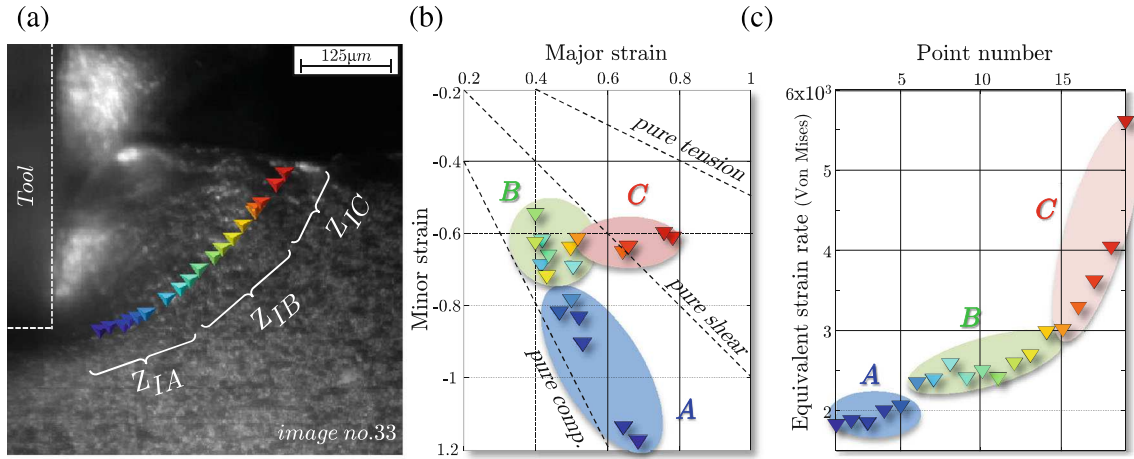


Fig. 7 (a) The three sub-zones of the ASB and the 19 selected points. (b) State of strain at failure. (c) strain rates at failure for the selected points

models and for damage evolution laws) [4]. A close monitoring of the image sequence reveals that the crack grows from the tooltip to the top free surface over 17 images. This film shot on the side surface, clearly shows that the disjunction goes from end to end. It can be seen in Fig. 8 that the material is disconnected on the side from $\delta = 10 \mu\text{m}$ while that disconnection appear at the center at approximately $70 \mu\text{m}$. Say, a small part of the cross-section (in the triaxial pressure zone) is still attached to the next segment. It results in the formation of a serrated chip (and not a fully segmented one). As highlighted by [35], the presence of a high hydrostatic stress zone at the chip center prevents form crack formation at the tooltip vicinity. As a matter of fact, such zone cannot exist near the free surface of the chip which is consistent with the end-to-end crack observed on the side (Fig. 5(a)).

The formation process of this disjunction remains largely undocumented in the literature at least from an experimental

standpoint and no mention of side effects is made. However, the observations performed during this work show significant differences between the side and core disjunction processes. From the knowledge of the 3D nature of the chip formation process and other published observations, one may think of three possible scenarios to model the crack evolution:

The first scenario is depicted in Fig. 9(a). The crack initiate at the tooltip (on the side), propagates along the primary shear band, generates a step on the top surface, and keeps propagating backward (through-thickness) to the triaxial pressure zone. This hypothesis is backed by chip *post-mortem* micrography and QSP observations of polished chips and is widely acknowledge in the scientific community [36–38]. Regretfully, these observations are made at one given time of the formation process and cannot provide evolutionary information. Moreover, the material removal due to polishing disable the observation of side effects.

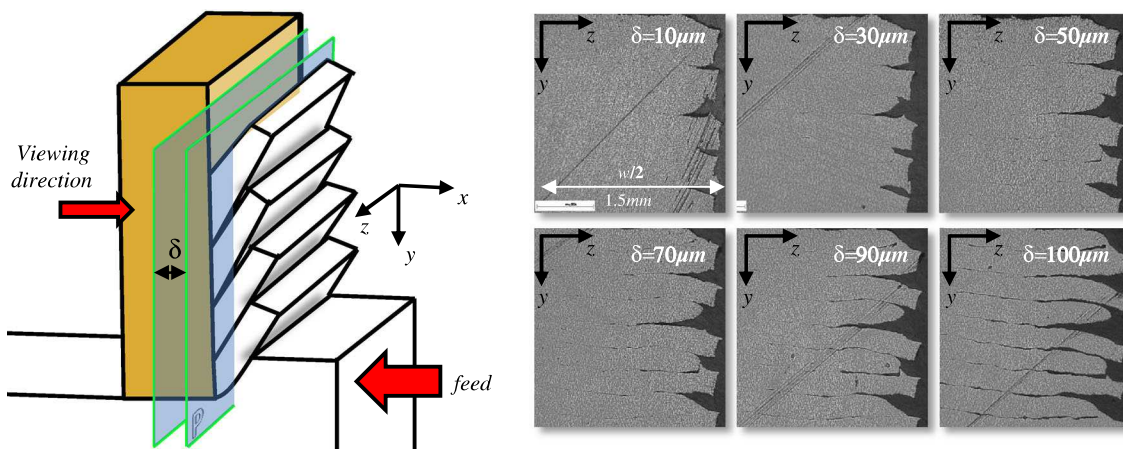


Fig. 8 Successive cuts of the chip through thickness showing an open crack at the left end but connected material within the hydrostatic stress zone

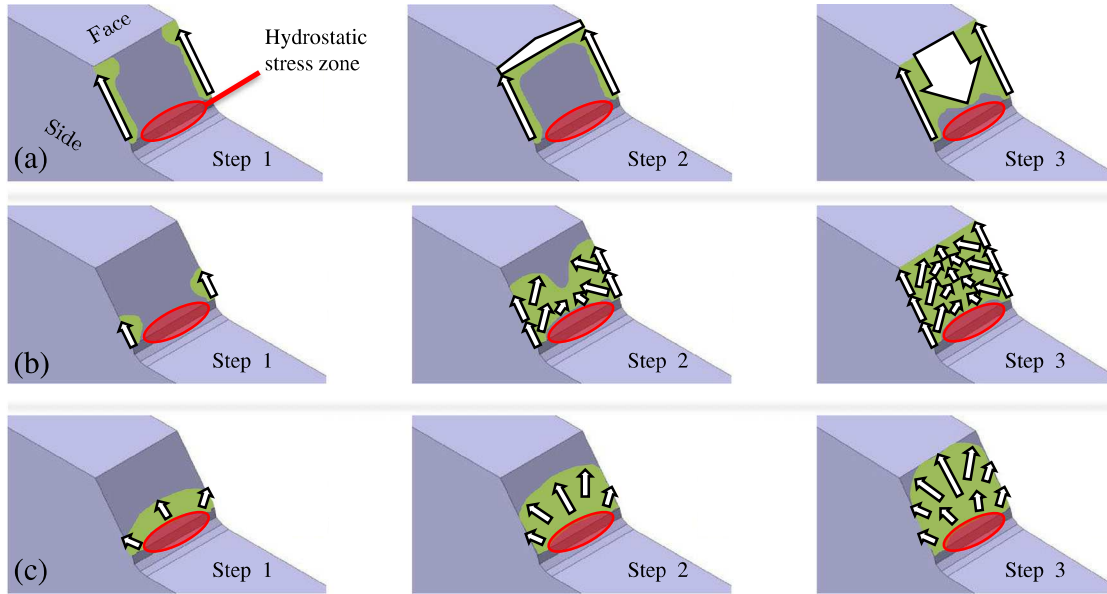


Fig. 9 (a) First scenario: face-to-core propagation of the crack (with side initiation). (b) Second scenario: side-to-core propagation of the crack (with side initiation). (c) core/side-to-face propagation of the crack with simultaneous initiation

The second scenario is depicted in Fig. 9(b). The crack initiates at the tooltip (on the side) and while propagating along the primary shear band it turns through-thickness when the hydrostatic pressure becomes low enough. Then, it reaches the face-side corner first, then the center of the face. This scenario is consistent with the 2D numerical observations performed by [39]. Authors have used the energy-based ductile fracture model proposed by [40] and performed chip micrographic observations. However, the numerical model is built under a 2D assumption and does not provide information on the side effects.

The third scenario, depicted in Fig. 9(c), is actually a variation of the second scenario. Instead of a side initiation, the crack initiates all along the borders of the triaxial zone. One may assume that the high compressive strains at these locations make the triaxial zone behave as a rigid body that slips on the cutting face. The crack is then initiated simultaneously on the side and through-thickness. This scenario, though not as well-established as the others, may explain the existence of the material voids visible in various chip micrographic observations [41, 42].

Discussion among those three possibilities is a complex experimental (and numerical) task and the purpose of this work is not validate (or discard) these hypothesis. However, various observations can offer leads on that matter. For instance, the constant strain rate observed right after the completion of the side crack observed in Fig. 6 is not really compatible with the first and second scenarios (where the segment is still not fully formed when the side crack runs from end to end). The first scenario does not explain the existence of material voids along the ASB. QSDs could be

a good way to investigate the crack geometry but also existence and location of material voids and side effects, upon condition that the instant of the tool separation is precisely known (high frame rate imaging can be used on that purpose). In addition, the use of in-process observations of the top face may help differentiate the 3 scenarios (outbreak of the crack on the top). Another lead would be a cutting force monitoring. It would enable to link strain rates and the evolution of the resisting cross-section. Finally, the effect of temperature is also to be investigated.

Conclusion

This paper discusses the difficulties using built-in strain measurement in machining conditions. It proposes a sub-millimeter procedure for image acquisition and a suitable numerical post-processing that enables strain evaluation during the segmentation process. Results show a significant strain localization within the ASB and heterogeneity of the deformation behavior along this band.

This work provides experimental evidences of a significant side effect and highlights the 3D nature of the chip (even in orthogonal cutting conditions). It therefore challenges the classical plane strain hypothesis widely acknowledged in literature. Indeed, chips are often wider than thick and this hypothesis holds as long as the averaged behavior is investigated. However, considering a chip formation process with crack initiation on the sides (where the plane stress hypothesis seems more suited) would clearly require the use of 3D finite element formulation.

In addition, the presented procedure offers a way to quantify the strains within the adiabatic shear band under the assumption of material continuity. However, as seen in the above, this hypothesis does not hold when serrated chip are produced. Hence, one understands that detecting the presence (or absence) of material disjunction is a serious issue and can lead to significant over-estimation of the strains. The development of a reliable criterion for crack detection (based on the orientation of the velocity gradient vector) is under construction and will be presented in future publication.

Two main drawbacks can be singled out of the presented experiments. The first one is the lack of in-process information on the magnitude and the shape of the out-of-plane deformation of the chip. It is a direct consequence of the chosen experimental procedure. Indeed, the topological study of this phenomenon is an experimental challenge of its own and constitutes a perceptive of this work. For this purpose, the use of stereo-imaging, computed tomography or any other non planar strain measurement technique seems inevitable.

Another drawback of the proposed procedure lies in the inability to measure strains at the direct vicinity of the cutting tool (i.e., in zones Z_{II} and Z_{III}). Indeed, experimental constraints are responsible for the lack of data at these locations. Firstly, the small depth of field and the out-of-plane position of the cutting tool lead to a fuzzy delimitation of the tool edges (fuzzy parts of the image around the theoretical position of the cutting tool). Secondly, the nonalignment of the lighting with the optical axis leads to over-exposure of the disoriented facets, especially during the out-of-plane deformation of the segment (white regions of the chip). A correction of these experimental limitations should be addressed in future works.

Finally, achieving a complete comparability between machining experiments and models will require the investigation of thermal effects. Several attempts has been made [43–45], but the fulfillment of an energy balance over the formation of one segment remains unexplored and surely constitutes the most challenging perspective of this work.

References

- Mabrouki T, Rigal J-F (2006) A contribution to a qualitative understanding of thermo-mechanical effects during chip formation in hard turning. *J Mater Process Technol* 176:214–221
- Bahi S, Nouari M, Moufki A, El Mansori M, Molinari A (2011) A new friction law for sticking and sliding contacts in machining. *Tribol Int* 44:764–771
- Childs T (2006) Friction modelling in metal cutting. *Wear* 260:310–318
- Calamaz M, Coupard D, Girot F (2010) Numerical simulation of titanium alloy dry machining with a strain softening constitutive law. *Mach Sci Technol* 14(2):244–257
- Hor A, Morel F, Lebrun J-L, Germain G (2013) An experimental investigation of the behaviour of steels over large temperature and strain rate ranges. *Int J Mech Sci* 67:108–122
- Shi B, Attia H, Tounsi N (2010) Identification of material constitutive laws for machining - part i: An analytical model describing the stress, strain, strain rate, and temperature fields in the primary shear zone in orthogonal metal cutting. In: *Journal of Manufacturing Science and Engineering, Transactions of the ASME* 132
- Jaspers S, Dautzenberg J (2002) Material behaviour in metal cutting: Strains, strain rates and temperatures in chip formation. *J Mater Process Technol* 121:123–135
- Buda J (1972) New methods in the study of plastic deformation in the cutting zone. *CIRP Ann* 21:17–18
- Komanduri R, Brown R (1981) On the mechanics of chip segmentation in machining. *J Eng Ind* 103:33–51
- Ernst H, Merchant M (1941) Chip formation, friction and high quality machined surfaces. *Surf Treat Metals* 29:299–378
- Lee E, Shaffer B (1951) The theory of plasticity applied to a problem of machining. *J Appl Mech* 18:405–413
- Childs T (1971) A new visio-plasticity technique and a study of curly chip formation. *Int J Mech Sci* 13:375–387
- Pujana J, Arrazola P, Villar J (2008) In-process high-speed photography applied to orthogonal turning. *J Mater Process Technol* 202:475–485
- Chaudhri M (1993) Subsurface deformation patterns around indentation in workhardened mild steel. *Phil Mag Lett* 67(67):107–115
- List G, Sutter G, Bi X, Molinari A, Bouthiche A (2013) Strain, strain rate and velocity fields determination at very high cutting speed. *J Mater Process Technol* 213:693–699
- Hijazi A, Madhavan V (2008) A novel ultra-high speed camera for digital image processing applications. *Meas Sci Technol* 19:085503 (11p)
- Germain G, Morel F, Lebrun J, Morel A (2007) Machinability and surface integrity for a bearing steel and a titanium alloy in laser assisted machining (optimisation on LAM on two materials). *Lasers Eng* 17(5–6):329–344
- Shaw M, Dirke S, Smith P, Cook N, Loewen E, Yang C (1954) Machining titanium. In: *Machining titanium*. In: MIT Rep. (4th edn.) - Massachusetts Institute of Technology
- Gnanamanickam E, Lee S, Sullivan J, Chandrasekar S (2009) Direct measurement of large-strain deformation fields by particle tracking. *Meas Sci Technol* 20:095710 (12p)
- Guo Y, Efe M, Moscoso W, Sagapuram D, Trumble K, Chandrasekar S (2012) Deformation field in large-strain extrusion machining and implications for deformation processing. *Script Mater* 66:235–238
- Vacher P, Dumoulin S, Morestin F, Mguil-Touchal S (1999) Bidi-mensional strain measurement using digital images. *Proc Inst Mech Eng* 213:811–817
- Pottier T, Moutrille M-P, Le-Cam J-B, Balandraud X, Grédiac M (2009) Study on the use of motion compensation techniques to determine heat sources. Application to large deformations on cracked rubber specimens. *Exp Mech* 49:561–574
- Bornert M, Brémand F, Doumalin P, Dupré J-C, Fazzini M, Grédiac M, Hild F, Mistou S, Molimard J, Orteu J-J, Robert L, Sirel Y, Vacher P, Wattrisse B (2008) Assessment of digital image correlation measurement errors: methodology and results. *Exp Mech* 49:353–370
- Pan B, Xie H, Wang Z, Qian K, Wang Z (2008) Study on subset size selection in digital image correlation for speckle patterns. *Opt Express* 16:7037–7048
- Triconnet K, Derrien K, Hild F, Baptiste D (2009) Parameter choice for optimized digital image correlation. *Opt Lasers Eng* 47:728–737

26. Pan B, Lu Z, Xie H (2010) Mean intensity gradient: an effective global parameter for quality assessment of the speckle patterns used in digital image correlation. *Opt Lasers Eng* 48:469–477
27. Sutton MA, Yan JH, Tiwari V, Schreier WH, Orteu JJ (2008) The effect of out-of-plane motion on 2d and 3d digital image correlation measurements. *Opt Lasers Eng* 46:746–757
28. Pan B, Yu L, Wu D (2013) High-accuracy 2d digital image correlation measurements with bilateral telecentric lenses: error analysis and experimental verification. *Exp Mech* 53:1719–1733
29. Pottier T, Louche H, Samper S, Favrelière H, Toussaint F, Vacher P (2012) A new filtering approach dedicated to heat sources computation from thermal field measurements. In: *Photomechanics*, Montpellier, France
30. Chrysochoos A, Louche H (2000) An infrared image processing to analyse the calorific effects accompanying strain localisation. *Int J Eng Sci* 38:1759–1788
31. Le Goic G, Favrelière H, Samper S, Formosa F (2011) Multi scale modal decomposition of primary form, waviness and roughness of surfaces. *Scanning* 33(5):332–341
32. Wang W, Mottershead J, Sebastian C, Patterson E (2011) Shape features and finite element model updating from full-field strain data. *Int J Solids Struct* 48:1644–1657
33. Calamaz M, Limido J, Nouari M, Espinosa C, Coupard D, Salan M, Girot F, Chieragatti R (2009) Toward a better understanding of tool wear effect through a comparison between experiments and sph numerical modelling of machining hard materials. *Int J Refract Met Hard Mater* 27:595–604
34. Shih A (1995) Finite element analysis of the rake angle effects in orthogonal metal cutting. *Int J Mech Sci* 1:1–17
35. Komanduri R, von Turkovich B (1981) New observations on the mechanisms of chip formation when machining titanium alloys. *J Wear* 69(2):179–188
36. Gentel A, Hoffmeister H (2001) Chip formation in machining Ti6Al4V at extremely high cutting speeds. *CIRP Ann Manuf Technol* 50(1):49–52
37. Nakayama K, Arai M, Kanda T (1988) Machining characteristics of hard materials. *CIRP Ann Manuf Technol* 37(1):89–92
38. Vyas A, Shaw M (1999) Mechanics of saw-tooth chip formation in metal cutting. *J Manuf Sci Eng* 121(2):163–172
39. Hua J, Shivpuri R (2004) Prediction of chip morphology and segmentation during the machining of titanium alloys. *J Mater Process Technol* 150(1–2):124–133
40. Cockcroft M, Latham D (1968) Ductility and workability of metals. *J Inst Met* 96:33–39
41. Braham-Bouchnak T (2010) étude du comportement en sollicitation extrême et de l'usinabilité d'un nouvel alliage de titane aéronautique : le Ti555-3. Ph.D. thesis, École Nationale Supérieure des Arts et Métiers
42. Courbon C (2011) Vers une modélisation physique de la coupe des aciers spéciaux : intégration du comportement métallurgique et des phénomènes tribologiques et thermiques aux interfaces. Ph.D. thesis, Ecole Centrale – Université de Lyon
43. Abukhshim N, Mativenga P, Sheikh M (2006) Heat generation and temperature prediction in metal cutting: a review and implications for high speed machining. *Int J Mach Tools Manuf* 46:782–800
44. Arrazola J, Arriola I, Davies M (2009) Analysis of the influence of tool type, coatings, and machinability on the thermal fields in orthogonal machining of AISI 4140 steels. *CIRP Ann Manuf Technol* 58:85–88
45. Filice L, Umbrello D, Beccari S, Micari F (2006) On the FE codes capability for tool temperature calculation in machining processes. *J Mater Process Technol* 174:286–292