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Effect of thermal aging on crystallization behaviors and dynamic mechanical properties of glass fiber reinforced polyphenylene sulfide (PPS/GF) composites

Peiyuan Zuo¹  · Abbas Tcharkhtchi¹ · Mohammadali Shirinbayan¹ · Joseph Fitoussi¹ · Farid Bakir²

Abstract

In this study, the main purpose is to systematically evaluate isothermal and non-isothermal crystallization behavior of short glass fiber-reinforced polyphenylene sulfide polymer composites (PPS/GF) by a wide range of commonly applied models and also to precisely discuss the crystallization evolution and dynamic mechanical properties together with the consideration of thermal aging effects. Some interesting progress concerning this study can be concluded as follows: the Avrami model was used to examine the isothermal crystallization behavior of PPS/GF and the Avrami plot results exhibit that the isothermal crystallization contains primary and second crystallization process. In terms of non-isothermal crystallization, the Jeriorny model and Mo model could describe the mechanism of nucleation and crystal growth of PPS/GF material under study. Also, the activation energy of non-isothermal crystallization is calculated (-58.78 kJ/mol) by Kissinger method. Another important aspect is that thermal aging has an obvious effect on crystallization behaviors of PPS under study. The degree of crystallinity increases from 44% (virgin sample) to 56% after 96 h of aging at 200 °C. After a long period of oxidation up to 1080 h at 200 °C, the crystallinity degree decreases to 36.6% due to thermo-oxidation effect. DMA results imply that thermal aging may lead to more crosslinking reactions and result into more restriction of molecule mobility in PPS composite materials.

Keywords Poly-Phenylene sulfide (PPS) · Crystallization · Kinetic model · Thermal aging effect · Dynamic mechanical properties

Introduction

Polyphenylene sulfide (PPS) exhibits good dimensional stability, thermal stability and electrical properties as well as

mechanical strength. Also, PPS-based materials, when reinforced with glass/carbon fibers/related filaments, have been popularly used as a high-performance material in recent years, not only in terms of structural materials fields (e.g., aerospace and automobile industries), but also in other various fields such as electrodes, separators, etc. In last couple of years, there are many literatures focusing these aspects.

On the one hand, some researchers pay much attention to mechanical properties of PPS materials. For example, Park et al. [1] modified PPS composites reinforced with carbon fibers and they found the method of electrophoretic surface deposition of multi-walled carbon nanotubes can improve the flexural properties of PPS composites. Zhao et al. [2] prepared PPS nonwovens with ultra-high content of glass fiber fabrics by thermo-compression lamination method and these nonwovens showed a significant increase in various mechanical properties. Moreover, Backe et al. [3] characterized the ultrasonic fatigue behaviors of carbon fiber fabric reinforced PPS composites for aircraft applications and the authors found that lifetime-oriented investigations at stress ratios between $R = 0.1$ and 0.51 exhibited an exponential decrease of the bearable

✉ Peiyuan Zuo
2015-1027@ensam.eu

Abbas Tcharkhtchi
abbas.tcharkhtchi@ensam.eu

Mohammadali Shirinbayan
mohammadali.shirinbayan@ensam.eu

Joseph Fitoussi
joseph.fitoussi@ensam.eu

Farid Bakir
farid.bakir@ensam.eu

¹ Arts et Metiers Institute of Technology, CNAM, PIMM, HESAM University, F-75013 Paris, France

² Arts et Metiers Institute of Technology, CNAM, LIFSE, HESAM University, F-75013 Paris, France

stress amplitudes in the range between 10^6 and 10^9 cycles. Similarly, Stoeffler et al. [4] studied PPS composites reinforced with recycled carbon fiber for aerospace applications and the main findings showed that the recycled carbon fiber reinforced PPS composites had a comparable mechanical properties to equivalent compounds fabricated by industrial grades of short virgin carbon fiber. Also, Maaroufi et al. [5] investigated the post-fire compressive behavior of carbon fibers woven-ply PPS laminates for aeronautical applications and the prior fire-exposure led to increased damages due to PPS matrix thermal decomposition. Liu et al. [6] used thermoplastic prepregs in a double-belt press to fabricate carbon fiber reinforced PPS composite and the results showed that a relative lower process velocity ($0.2 \text{ m}\cdot\text{min}^{-1}$) could produce this composite with a good tensile and interlaminar shear properties which are comparable to that of compression-molded composites.

On the other hand, PPS-based materials also have other important applications in various fields. For example, Aramid nanofiber / PPS nonwoven composite separator was fabricated by Zhu et al. [7] through a facile papermaking method for lithium ion battery applications and the results showed that the introduced polar aramid nanofibers in the PPS composite separator could dramatically regulate the porosity and improve the following electrode properties. Luo et al. [8] investigated a PPS nonwoven-based composite separator and the authors concluded that PPS nonwoven-based composite possessed higher porosity and air permeability as well as other improved electrical properties when compared with commercialized polyolefin separator. Chitosan modified PPS-based microfiber membrane for effective antibacterial activity and oil-in-water emulsion separation was fabricated by Huang et al. [9] and this membrane had a promising long-term separation in terms of oily wastewater treatment.

To make better use of this material, there are also some fundamental references regarding crystallization behaviors of PPS materials [10–13]. For example, Furushima et al. [14] studied crystallization/melting kinetics of PPS and they found that the half-time crystallization of isothermally melt-crystallized PPS showed a downward convex curve with a minimum at $160 \text{ }^\circ\text{C}$. Liu et al. [15] studied the crystal structure of PPS / carbon fiber composites fabricated by additive manufacturing and they found that the intensities of the diffraction peaks originated from PPS increased until the annealing time reached 9 h, which showed an improvement in crystal perfection due to molecular chain rearrangement. Also, nucleating agent plays an important role during crystallization of PPS materials. For example, Deng et al. [16] reported nanodiamond as an efficient nucleating agent for PPS and they clarified that the Avrami equation and Mo method provided that a fairly satisfactory description for the non-isothermal crystallization of PPS in both pure and composite forms. Nanodiamond particles provided a heterogeneous nucleation effect on PPS by remarkably increasing the crystallization temperature and improving the crystallization rate. Moreover, some fillers or

particles can also have the effects as nucleating agent. In this aspect, Chen et al. [17] investigated isothermal crystallization kinetics of PPS doped with amorphous carbon or crystalline graphite particles. Both types of carbon forms had been found to affect the crystallization behavior of PPS in some extent. Similarly, Jiang et al. [18] prepared a series of composites by blending PPS with multi-walled carbon nanotubes at 1, 2 and 3 wt% to investigate nucleation effect of hydroxyl-purified multi-walled carbon nanotubes in PPS composites. They revealed that the enthalpy ΔH_c of the composites increased with increasing multi-walled carbon nanotubes whereas the crystallization temperature decreased progressively.

Moreover, many researchers take the effect of annealing or curing processes into consideration and these annealing or curing processes could directly affect the crystallization behavior and further other properties such as morphologies and mechanical properties. Lee et al. [19] investigated the effect of curing on the crystallization rates of PPS and PPS/carbon fiber composites by DSC technique. They found the crystallization rate of PPS was enhanced with increasing degree of curing. Moreover, Lu et al. [20] studied the effects of annealing on relaxation behavior of PPS film material. DSC results suggested that annealing caused the PPS film to relax some of its rigid amorphous fraction and increase its crystallinity. DMA results showed a corresponding increase in the temperature location of the dissipation peak and a decrease in its amplitude when T_α increased above $100 \text{ }^\circ\text{C}$. Similarly, Lee et al. [21] investigated commercial PPS by thermal curing and they found an increase of molecular weight due to crosslinking. They concluded the crosslinking of PPS affected crystallization behaviors significantly. To a certain extent, crosslinking acted as nucleation agents, but excessive crosslinking hindered the crystallization. Morphology observed by polarized optical microscopy suggested that thermal curing for as little as 1 day contributed to the spherulite structure having a smaller size and that was not observed with pure PPS. Boey et al. [22] analyzed the effect of annealing on the non-linear creep deformation of the PPS composite specimens and indicated that the creep deformation for both 20 and 40% reinforced samples were relatively similar despite the difference in the amount of fiber reinforcement. In contrast, with the crystallinity percent increasing, the value of the creep stress and strain rate components decreased exponentially. In addition, thermal history should also be taken into consideration as an important factor during crystallization. For example, Chung et al. [23] studied the effect of thermal history on crystal structure of PPS. They found the dimensions of the crystal lattice were depended upon prior thermal conditions. Moreover, Caminiti et al. [24] investigated the PPS isothermal cold crystallization behavior and they showed that the quenching procedure did not secure the perfect reproducibility, which may influence the concentration of these nuclei and the crystallization rate of polymeric materials.

Also, to meet the increasing requirement for different properties of PPS, PPS was studied in form of blended polymers or reinforced composites. In aspect of blended polymers containing PPS. For example, the effect of Poly ether ether ketone on crystallization and multiple melting behavior of PPS was studied by Mai et al. [25] and they found that an increase in the T_c and also the intensity of the T_c peak of PPS. Some research also [26] reported pure, glass, carbon and aramid fiber reinforced PPS. They showed the system of aramid fiber/PPS had a much shorter half-time of crystallization than the other three systems. More researches concerning crystallization were focused on various PPS composites. Desio et al. [27] studied the isothermal crystallization from the melt of unreinforced PPS and of carbon, aramid, and glass fiber reinforced PPS composites. The results indicated that the influence of fibers on PPS crystallization was not only fiber specific, but also strongly dependent on the surface treatment. In general, fiber reinforced systems crystallized faster than unreinforced PPS, and the degree of crystallinity was relatively lower. And also, they observed that the rate of crystallization was improved in those systems which exhibited trans-crystallinity in thin PPS film/single fiber composites. Cole et al. [28] studied the crystallinity in PPS-carbon composites by using diffusion reflection FTIR spectroscopy and DSC techniques, and they found isothermal annealing induced a secondary type of crystallization which gave a structure whose “melting point” was about 15 °C higher than the annealing temperature. Heating PPS in air at temperature near its melting point caused structural changes, resulting in a lower ultimate degree of crystallinity and a lower melting point.

On the other hand, DMA tool is powerful to study polymer/polymer miscibility in polymer blends and also measure the glass transition temperature of polymer. Moreover, it can obtain an idea about the storage modulus, loss modulus and damping behavior. Yang et al. [29] prepared PPS/multiwall carbon nanotube composites and observed increased T_g and storage modulus of PPS via DMA. Wu et al. [30] studied thermal behaviors and viscoelastic properties of PPS/epoxy resin by DMA test and showed that the epoxy resin can promote degradation and branching of PPS during melting mixing due to its poor thermal stability.

Reviewing these literatures helps us to get an overall understanding of the crystallization behaviors and dynamic mechanical properties of raw PPS materials. However, there is not so much research concerning the detailed discussion related to the thermal aging effect on crystallization behaviors and dynamic mechanical properties for thermal aged PPS materials. So, it seems very meaningful and important to verify the common models and methodologies for isothermal or non-isothermal crystallization behaviors in PPS composite system under our study, which is reinforced with short glass fibers. Also, it should be emphasized that it is very innovative and significant to consider long-time thermal aging effect on

crystallization behaviors and dynamic mechanical properties since this work will make some positive contribution to the further application of PPS materials in practice.

Materials and test techniques

Materials and sampling

PPS composite materials are supplied by Valeo Company in France. The details about these materials can be summarized as follows: The supplied PPS is black plate with density of around 1.58 g/cm³ and the weight percent of glass fiber is 30%. The material has a water absorption of 0.02%. Films with a thickness of 20 μm or rectangular plate samples were placed in the ovens (with circulation of air) and the temperatures of aging were chosen from 100 °C to 200 °C for different aging time. More details concerning thermal aging process can be seen in our previous publications [31–33].

Characterization methods

Differential scanning calorimetry (DSC)

The differential scanning calorimetry (DSC) measurements were carried out with the DSC Q10 V9.0 Build 275 (TA Instruments, Guyancourt, France). The samples of mass between 5 and 10 mg were placed in hermetic aluminum capsules. The sample was heated up to 300 °C with a temperature rate of 10 °C/min under the atmosphere of Nitrogen (40 ml/min) and was kept at this temperature for 10 min. Subsequently, it was cooled down with different cooling rates (5~25 °C/min) to observe the non-isothermal crystallization behaviors or it was cooled down to some fixed temperatures to see the isothermal crystallization behaviors.

The degree of crystallinity X_C is calculated from the following relationship:

$$X_C = \frac{\Delta H_f}{\Delta H_f^0 * \varphi} * 100\% \quad (1)$$

With X_C =crystallinity degree, ΔH_f =enthalpy of fusion, ΔH_f^0 = pure crystalline phase enthalpy of fusion, φ = percent of matrix.

Dynamic mechanical analysis

Dynamic Mechanical Analysis (DMA) tests were carried out using the Q800 DMA instrument to measure major transition temperatures and viscoelastic behavior. These tests were conducted under the following conditions: the first step is to do an alternating bending configuration in our case and then the selected test temperatures were chosen between 25 °C and

200 °C. The frequency is chosen at 1 or 10 Hz with the increasing temperature rate of 0.5 °C/min. The sample had a rectangular shape (35 × 12 × 3 mm³).

Wide X-ray diffraction

The Wide X-ray diffraction (WXR) patterns are scanned by using Cu-K α radiation sources operated at 40 KV and 20 mA with diffraction angle ranging from 3 ° to 40 ° with the speed of 5 °/min. The diffraction peak is at 2 θ = 20.4°.

Crystallization behaviors of PPS/GF composites

Isothermal crystallization behavior

Isothermal thermograms of PPS/GF composites obtained by cooling a molten sample to the isothermal crystallization temperature (T_c) are shown in Fig. 1. It can be seen that the crystallization of PPS/GF is strongly affected by the given T_c . With increasing the T_c , the peaks tend to be more and more flat and this is mainly due to the decreasing of crystallization rate.

For a general crystallization behavior of polymers, the crystallization weight fraction, $\chi(t)$, is obtained from DSC exotherms of polymers by means of the ratio between the partial area at time t and the total exotherms area, i.e.,

$$\chi(t) = \int_{t_0}^t \left(\frac{dH}{dt} \right) dt / \int_{t_0}^{\infty} \left(\frac{dH}{dt} \right) dt \quad (2)$$

Where: $\frac{dH}{dt}$ is the heat flow rate and t_0 is the induction time.

With this following result in Fig. 2, one can conclude that the higher isothermal temperature corresponds to longer

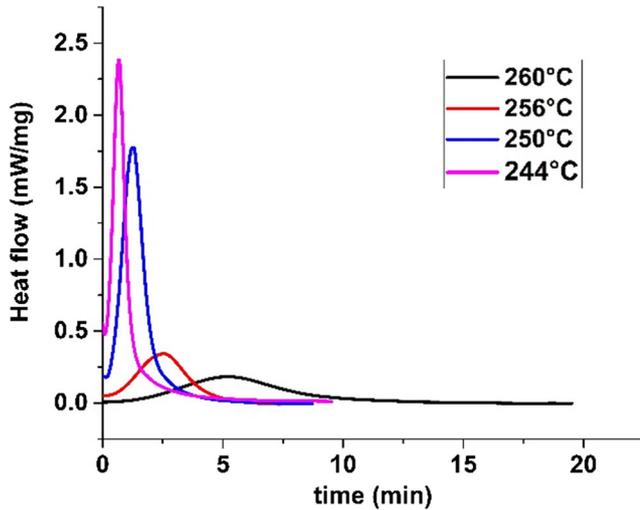


Fig. 1 The heat flow curves of PPS composites at different isothermal temperatures from melt point

relative crystallization time. For example, lower isothermal temperatures below 256 °C accomplish their crystallization in 5 min while this value for 260 °C is relatively 3 times higher (with 15 min).

Analysis of the crystallization kinetic of PPS composites under isothermal condition is accomplished with the application of the Avrami equation according to the results of DSC. Actually, for a general crystallization kinetics of a semi-crystalline polymer, most researchers use developed models based on an Avrami classical theory [34]. In detail, the Avrami treatment concerning crystallinity χ versus time can be drawn as the following expression:

$$1 - \chi(t) = \exp[-Kt^n] \quad (3)$$

Where $\chi(t)$ is the relative crystallinity at time t ; K , the crystallization rate constant depending on nucleation and growth rates; and n , the Avrami crystallization exponent depending on the nature of nucleation and growth geometry of crystals. Avrami plots can be constructed by plotting $\log[-\ln(1 - \chi(t))]$ versus $\log(t)$.

According to the relative crystallinity result above, it is possible to apply Avrami plot to explain the crystallization behavior of PPS/GF under study (see Fig. 3 and Table 1). First of all, with increasing T_c , the curves tend to shift to higher crystallization time. Moreover, one can see all curves can be divided as three domains including primary crystallization areas as well as two stages and secondary crystallization area. In detail, the curves in two stages of primary crystallization areas tend to be linear while the curves in secondary crystallization areas seem non-linear. Also, the stage 1 in primary area has a very small k_c (less 0.247) and this k_c corresponds to the rate of crystallization. With increasing T_c , the k_c tends to be smaller, indicating that higher T_c decreases the crystalliza-

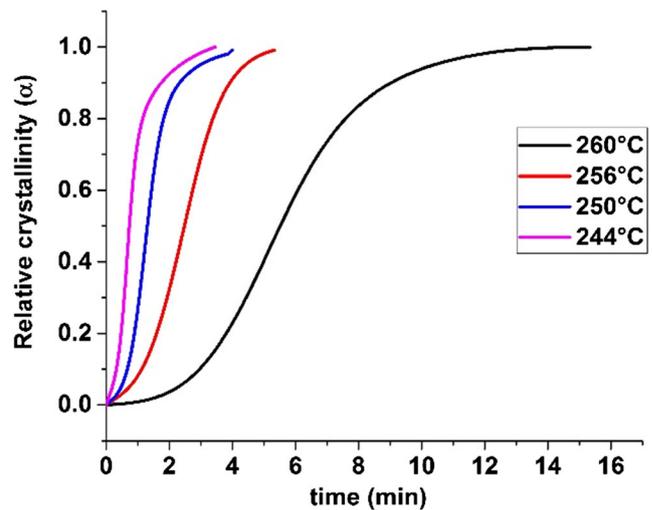


Fig. 2 The relative crystallinity curves of PPS composites at various isothermal temperatures

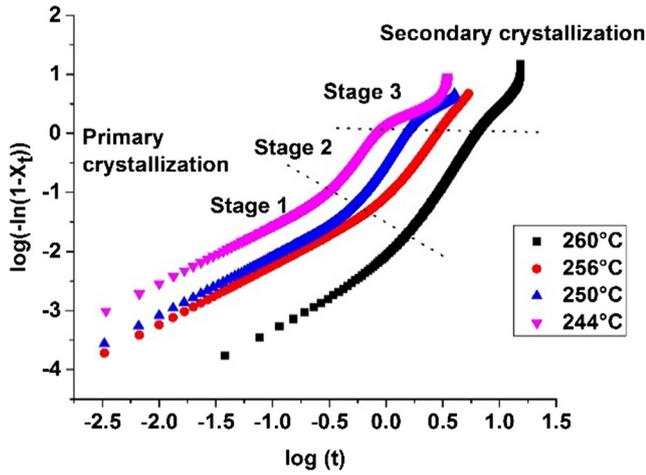


Fig. 3 Avrami Plot of $\log(-\ln(1-\chi(t)))$ against $\log t$ for isothermal crystallization of PPS composites

tion rate. In stage 2, the k_c increase to a relative higher value above 2, this means that in this stage, the crystallization rate is faster than that in the first stage. In contrast, secondary crystallization seems to be non-linear and it seems hardly to be explained by the Avrami model.

In addition, we may define a crystallization half-time, $t_{1/2}$, as the time required for $\chi(t)$ to achieve one half of $\chi(\infty)$; i.e.,

$$\frac{\chi_{t_{1/2}}}{\chi_{\infty}} = 1/2 \quad (4)$$

Plotting of $\log(t_{1/2})$ against T_c can be seen in Fig. 4. One can see that with increasing T_c , $t_{1/2}$ has an straightly increasing trend.

Non-isothermal crystallization behavior

DSC curves obtained at different cooling rates ranging from 5 to 25 °C for PPS are shown in Fig. 5. One can note that the cooling rate has a significant effect on the crystallization behavior of PPS and the crystallization peak temperature corresponding to the maximum crystallization shifts to lower temperature with the cooling rate increasing. For PPS crystallization, it is interesting to note the exothermic crystallization peaks are single and very sharp. This implies secondary

Table 1. Isothermal crystallization kinetic parameters calculated from the Avrami equation.

Samples	Isothermal temperatures (°C)	Primary crystallization					
		Stage one			Stage two		
		k_c	n	R^2	k_c	n	R^2
PPS/GF	244	0.247	0.969	0.999	2.436	1.413	0.998
	250	0.082	0.996	1	2.902	0.317	0.997
	256	0.057	0.996	0.999	2.511	0.069	0.999
	260	0.0083	1.3	0.987	2.314	0.008	0.996

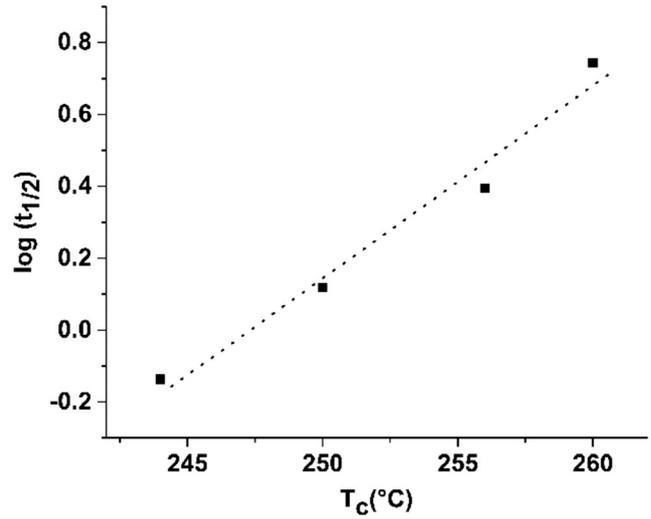


Fig. 4 Plot of $\log(t_{1/2})$ against T_c

crystallization has no obvious effect on the PPS non-isothermal crystallization behavior.

Figure 6 shows the results of relative crystallization α as a function of crystallization time at different cooling rates. One can note all curves show S-sharp and the relative crystallization increases very slowly initially and afterwards, that the slope of curve enhances sharply in the middle period, and then tends to be slow in the end. Also, it can be seen the crystallization time is mainly dependent on cooling rate since the crystallization time duration reduces rapidly with the cooling rate rising.

Also, it should be noticed that the $t_{1/2}$ decrease with increasing cooling rates (see Fig. 7). This mainly because the higher cooling rate has a higher crystallization rate, which will definitely shorten the accomplishment time of crystallization.

Jeziorny model

Based on Avrami model, Jeziorny model [35] is commonly used to characterize the non-isothermal crystallization process, and the equation can be written as follows [36–39]:

$$\alpha = \ln[-\ln(1-\chi(t))] = \ln K + n \ln t \quad (5)$$

$$\ln K_c = \frac{\ln K}{\beta} \quad (6)$$

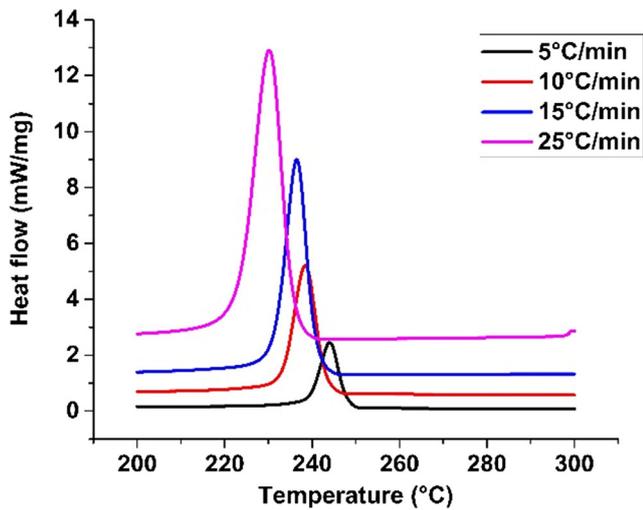


Fig. 5 The heat flow curves of PPS composites at various cooling rates (5~25 °C / min)

Where α is the fraction of relative crystallinity and $\chi(t)$ is relative crystallization fraction at time (t); K is crystallization rate constant; n is the Avrami constant and K_c is corrected crystallization rate constant, β is cooling rate.

After plotting the curve according to this model, one can note the plot of $\ln(-\ln(1-\chi(t)))$ against $\ln t$ gives a straight line with a high R^2 (>0.99) for all cooling rates (see Fig. 8). This means Jeziorny model can describe and verify the non-isothermal crystallization process for this PPS/GF material very well. Also, it is interesting to note from Table 2 the parameter K_c is related to the rate of crystallization. The value of K_c increases with the cooling rate rising, presenting that the crystallization rate becomes faster. This means that increasing cooling rate can improve the crystallization rate of PPS/GF under study.

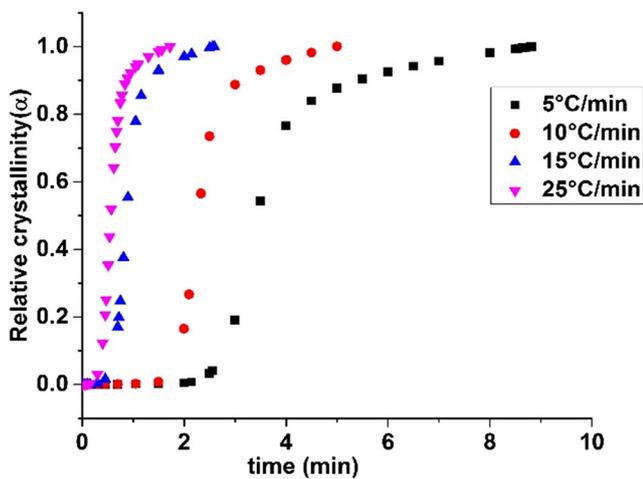


Fig. 6 The relative crystallinity curves of PPS composites at various cooling rates (5~25 °C / min)

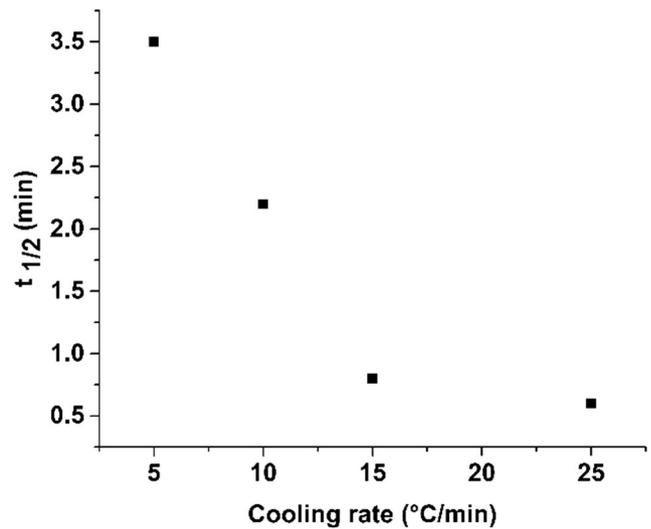


Fig. 7 The relationship of crystallization half time $t_{1/2}$ and cooling rate

Mo model

Mo model was proposed by a combination of Ozawa equation and Avrami equation to describe the non-isothermal crystallization kinetics of polymers, which can refer to the following equation [40, 41]:

$$\ln k + n \ln t = \ln K(T) - m \ln \beta \quad (7)$$

$$\ln \beta = \ln F(T) - \alpha \ln t \quad (8)$$

Where $\alpha = n/m$, $F(T) = [K(T)/k]^{1/m}$. $F(T)$ is related to the cooling rate, it represents the speed of the crystallization and m is the Ozawa exponent. With this relationship, one can plot the curve $\ln \beta$ against $\ln t$ (see Fig. 9).

More parameters can be seen in Table 3, high R^2 (>0.94) indicates that Mo model can well describe the crystallization behavior of PPS/GF composite materials.

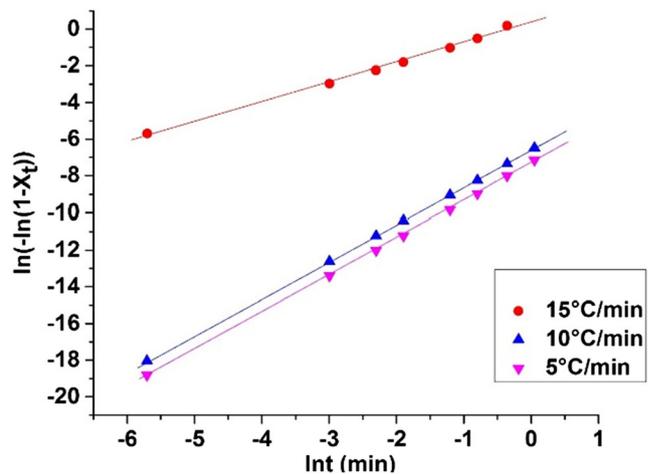


Fig. 8 Plot of $\ln(-\ln(1-\chi(t)))$ against $\ln t$ at various cooling rates (5~15 °C / min)

Table 2. Non-isothermal crystallization kinetics parameters from Jeziorny model.

	R ²	n	Ln K	K _c
5 °C/min	0.99	2.02	-7.33	0.23
10 °C/min	1	2.00	-6.61	0.52
15 °C/min	0.99	1.08	0.34	1.02
25 °C/min	0.99	3.55	0.91	1.04

Activation energy of non-isothermal crystallization

To calculate the activation energy in non-isothermal crystallization, Kissinger and coworkers [42] proposed a useful equation based on n-order kinetic model as follows:

$$\ln \frac{\beta}{T_p^2} = \ln \frac{AR}{E} - \ln[G(\alpha)] - \frac{E}{RT_p} \quad (9)$$

Where β is the cooling rate, T_p is the crystallization peak temperature. A is the pre-exponential factor and R is the universal gas constant. E is the activation energy and $G(\alpha)$ is the conversion function. With this Kissinger equation, a good linear relationship is traced between $\ln \frac{\beta}{T_p^2}$ vs. $\frac{1}{T_p}$ (see Fig. 10), and the activation energy in non-isothermal crystallization is obtained (-58.78 kJ/mol).

Further discussion

Evolution of crystallization behavior during thermal aging

In general, thermal aging process leads to a phenomenon involving a slow and irreversible change in terms of materials'

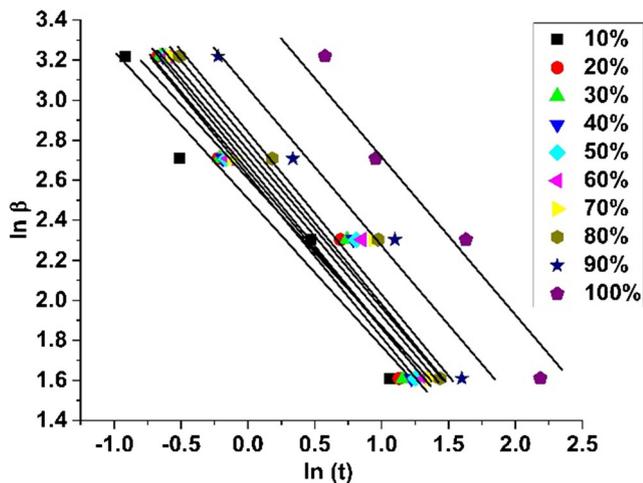


Fig. 9 $\ln \beta$ versus $\ln t$ for non-isothermal crystallization at different relative crystallinities

Table 3. Non-isothermal crystallization kinetics parameters from Mo model.

	R ²	Ln F(T)	a		R ²	Ln F(T)	a
10%	0.96	0.73	2.48	60%	0.95	0.49	3.30
20%	0.95	0.56	3.35	70%	0.94	0.45	3.30
30%	0.95	0.53	3.35	80%	0.97	0.43	3.36
40%	0.95	0.50	3.33	90%	0.96	0.42	3.37
50%	0.95	0.49	3.33	10%	0.95	0.36	3.41

properties. XRD is a powerful technique to analyze the crystallinity of materials. One can see the result in Fig. 11, the virgin sample has some obvious peaks at about $2\theta = 20.3^\circ$, which corresponds to the crystallized part in PPS/GF polymer composite. Interestingly, when the samples were treated in oven at different temperatures (100 °C to 200 °C) for 24 h, the peaks tend to increase and this implies some thermal treatment can also increase the crystallinity of PPS/GF materials.

The following part can be found in the thesis of Zuo [43], but the authors of Zuo et al. have revised this relevant part for this paper.

It should also be noticed that the polymer does not oxidize or degrade in the same way at different physical states. In glassy state, the amorphous phase is relatively fixed and compact and the mobility of the chains is very low. Also, the reaction of the polymer with oxygen is more difficult and slower. Comparatively speaking, in rubbery state, the oxidation occurs more easily and quickly. In the case of PPS composite materials, the result of the DMA test (Fig. 12) indicates that during oxidation at 140 °C, 160 °C, 180 °C and 200 °C, the amorphous phase is rubbery state. At 100 °C, this phase stays in the glass transition zone corresponding to a lower molecular mobility and reactivity. So, one should note in

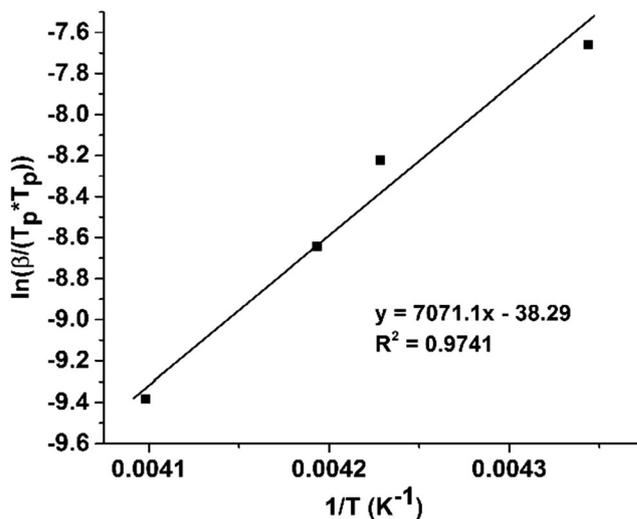


Fig. 10 Kissinger plot for calculating the non-isothermal crystallization activation energy of PPS/GF composite materials

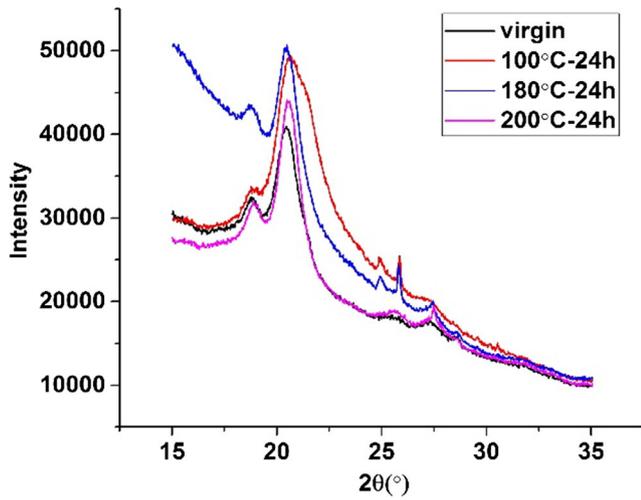


Fig. 11 XRD result obtained from PPS/GF sample

mind, the physical state is also related to the crystallization behaviors of polymer materials. Regarding the study of physical state, there is another further publication in our ongoing systematic research.

PPS is a semi-crystalline polymer, with an amorphous phase and a crystalline phase. The amorphous phase is much less compact. The oxygen can easily attack sites, which are the amorphous phase while oxygen cannot diffuse in the crystalline phase. Consequently, the thermal aging of the PPS has eventually resulted into the chemical structure change of the amorphous phase. This modification can be displayed in different ways: the crosslinking (appearing in certain cases and for certain period of aging), the scission of the macromolecular chains, the reduction of the molar mass, the embrittlement, the stiffening, the reorientation of the macromolecules, ... All these phenomena will happen in the amorphous phase and the crystalline phase during this period remains relatively intact. To understand the influence of thermal aging on the

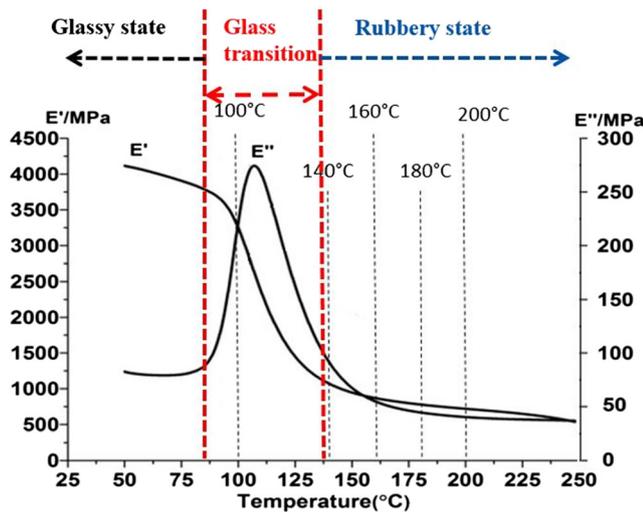


Fig. 12 Typical DMA results: different physical states (glassy and rubbery) and corresponding thermal aging temperature zones

mechanical properties, it is necessary to study this morphological evolution. The change in mechanical properties is more comprehensive through this microstructural modification. In the case of PPS/GF composite, the morphological characteristics can be tracked from the results of DSC and DMA tests based on virgin and aged PPS/GF samples (at 200 °C). Then it can be confirmed the T_g , the T_f , the crystallinity degree and the constants of the kinetic model of crystallization. Table 4 summarizes all these results.

One can notice that the T_g increases from 106 °C (virgin sample) to 121 °C (after 1080 h aging at 200 °C). This improvement can be explained as follows: (short-term) crosslinking and the reorientation and stiffening of macromolecules are derived from the chains breaking through oxidation and macromolecules tend to be less mobile in the amorphous zone.

It is also observed that the degree of crystallinity improves from 44% (virgin sample) to 56% after 96 h of aging at 200 °C. After a long period of oxidation (1080 h at 200 °C), the degree of crystallinity falls to 36.6%. It is very hard to explain this consequent drop in the crystallinity rate. Comparatively speaking, at this stage of degradation (1080 h) at 200 °C, the amorphous phase is seriously damaged and the morphological texture is totally modified.

In regard to the modification of the crystalline phase during thermal aging, the analysis of the change of the values concerning the constants of the model enables us to obtain the following findings:

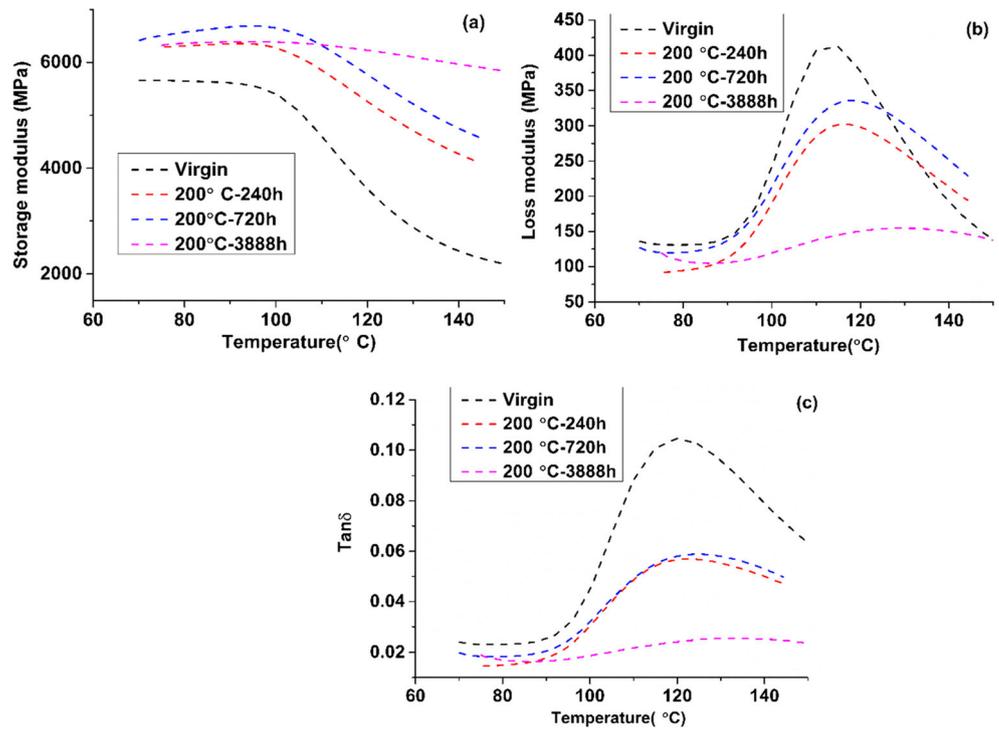
- The constant n depends on the nature of nucleation, the geometry of the crystallites and the density of the spherulites. The value of n is about 2 for virgin samples and aged at 200 °C up to 144 h. It can be assumed that during this period the crystalline phase is not very modified while, n decreases to 0.8 for the samples aged after 1080 h at 200 °C. This may indicate that the PPS material has almost lost its ability to nucleate and crystallize due to well excessive thermal aging when compared to its initial state.

Table 4. The parameters obtained from DMA and DSC.

Samples	Amorphous phase		Crystalline Phase	
	$T_g^{(*)}$ (°C)	$X_c^{(**)}$	$n^{(**)}$	$K_c^{(**)}$
Virgin	106	44.2	2.00	0.5
200 °C-20 h	108	45.0	2.10	0.88
200 °C-96 h	108	55.8	2.19	0.82
200 °C-144 h	—	52.9	2.27	0.97
200 °C-1080 h	121	36.6	0.8	0.6

^(*) T_g , obtained by DMA test at the peak of E'' , ($f = 1$ Hz); ^(**) X_c , n , K_c , obtained by DSC with a cooling speeding of 10 °C/min

Fig. 13 Storage modulus (a), loss modulus (b), $\tan \delta$ (c) evolution as a function of aging time at 200 °C (10 Hz)



- Comparatively speaking, K_c is associated with the crystallization rate and the increase in K_c represents the increase in the crystallization capacity. At the beginning of thermal aging, the growth in K_c was observed from 0.5 (virgin sample) to 0.97 (sample of 200 °C - 144 h). This implies that aging can improve the rate of crystallization. However, in the long term (as 200 °C - 1080 h), when aging is well excessive and the polymer is completely degraded, the value of K_c (0.6) shows that the polymer crystallizes more slowly during crystallization.

Dynamic mechanical analysis (DMA) during thermal aging

DMA is a powerful tool to precisely follow the thermal dynamic properties of the polymer and composites. As is shown in Fig. 13(a), it illustrates the storage modulus of composites from different thermal aging conditions. For the samples aged at 200 °C, they all have high storage modulus than virgin samples, during all tested range of testing temperature. This implies that thermal aging may lead to more crosslinking reaction, which will finally restrict the molecule mobility.

Figure 13(b) gives the information about the loss modulus evolution as a function of aging time at 200 °C. It is interesting to mention that with the aging time increasing, all peak values drop and the shape of peaks broaden. This may imply more relaxations happen with the aging time increasing at 200 °C.

Moreover, it is well known that the $\tan \delta$ is extremely sensitive to all kinds of transitions, relaxation processes, structural heterogeneities, and morphologies of multiphase systems (such as polymers, polymer blends, fillers or composite materials) [44, 45]. Figure 13(c) shows the $\tan \delta$ evolution as a function of aging time at 200 °C. One can observe that with the aging time increasing, the $\tan \delta$ exhibit the decreasing trend. Fuente et al. [45] concluded in their research that the damping parameter ($\tan \delta$) was a sensitive indicator of degradation. Therefore, at temperature well above T_g , the modulus tends to increase whereas the damping decreases with a rise degree of degradation. In our results, it is confirmed for all of samples, the $\tan \delta$ declines with the aging time increasing. This indicates the degree of degradation seems more and more serious with the aging time increasing at 200 °C. Also, it is of importance to note that the evolution of $\tan \delta$ in a study of aged PPS samples may be a valuable tool for predicting the service life of these materials. Also, it is significant to notice that the results are consistent with the previous study in reference of Fuente et al. [45], which also proves in further that the damping parameter ($\tan \delta$) can be as an indicator or parameter to reflect obviously the degree of degradation in materials.

Conclusions

In this paper, isothermal and non-isothermal crystallization behaviors of PPS/GF were systematically studied and a wide range of commonly used models were applied in this material.

Also, this paper emphasizes the thermal aging effect on crystallization behaviors and dynamic mechanical properties. The main conclusions are presented as follows:

- To PPS/GF (30% wt, glass fibers) composite, the isothermal crystallization behaviors seem hardly to be described while the non-isothermal crystallization can be well described by a wide ranges of classic crystallization kinetic models.
- The crystallization behaviors of PPS materials can be significantly affected by the thermal aging, with an evolution of degree of crystallinity increasing from 44% (virgin sample) to 56% after 96 h of aging at 200 °C. After a long period of oxidation up to 1080 h at 200 °C, the crystallinity degree decreases to 36.6%.
- In the long term (such as 200 °C - 1080 h), the value of K_c (0.6) shows that the polymer crystallizes more slowly during crystallization when aging is dramatically excessive and the polymer is completely degraded.
- DMA results imply that thermal aging may lead to more crosslinking reaction and restriction of molecule mobility. Also, the degree of degradation seems more and more serious with the aging time increasing at 200 °C.

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