



Science Arts & Métiers (SAM)

is an open access repository that collects the work of Arts et Métiers Institute of Technology researchers and makes it freely available over the web where possible.

This is an author-deposited version published in: <https://sam.ensam.eu>
Handle ID: <http://hdl.handle.net/10985/21312>

To cite this version :

Audrey BERRIOT, Nolwenn FOUGERON, Xavier BONNET, Helene PILLET, Pierre-Yves ROHAN
- Evaluation of the Agreement Between Ultrasound-Based and Bi-Planar X-Ray Radiography-
Based Assessment of the Geometrical Features of the Ischial Tuberosity in the Context of the
Prevention of Seating-Related Pressure Injury - 2021

Any correspondence concerning this service should be sent to the repository

Administrator : scienceouverte@ensam.eu





Science Arts & Métiers (SAM)

is an open access repository that collects the work of Arts et Métiers Institute of Technology researchers and makes it freely available over the web where possible.

This is an author-deposited version published in: <https://sam.ensam.eu>
Handle ID: <http://hdl.handle.net/10985/21312>

To cite this version :

Audrey BERRIOT, Nolwenn FOUGERON, Xavier BONNET, Helene PILLET, Pierre-Yves ROHAN
- Evaluation of the Agreement Between Ultrasound-Based and Bi-Planar X-Ray Radiography-
Based Assessment of the Geometrical Features of the Ischial Tuberosity in the Context of the
Prevention of Seating-Related Pressure Injury - 2021

Any correspondence concerning this service should be sent to the repository

Administrator : scienceouverte@ensam.eu



1 **Evaluation of the agreement between Ultrasound-**
2 **based and bi-planar X-Ray radiography-based**
3 **assessment of the geometrical features of the Ischial**
4 **Tuberosity in the context of the prevention of seating-**
5 **related pressure injury**

6
7 A.Berriot¹, N. Fougeron¹, X..Bonnet¹, H. Pillet¹ and P.Y. Rohan^{1*}

8
9 ¹Institut de Biomécanique Humaine Georges Charpark, Arts et Metiers Institute
10 Of Technology, 151 bvd de l'Hôpital, 75013. Paris, France

11 **Abstract**

12 The proper management of the local mechanical environment within soft tissues
13 is a key challenge central the prevention of Pressure Ulcers (PUs). Magnetic
14 Resonance (MR) imaging is the preferred imaging modality to measure geometrical
15 features associated with PUs. It is a very time-consuming method and it represents
16 a major barrier to the clinical translation of risk assessment tools. There is a growing
17 enthusiasm of the community for the use of B-mode ultrasound imaging as a
18 practical, alternative technology suitable for bedside or outpatient clinic use. The
19 objective was to evaluate the agreement between US-derived measurements and bi-
20 planar X-ray radiography-derived measurements of geometrical features of the
21 Ischial Tuberosity in a realistic loaded sitting position in healthy volunteers. The
22 reproducibility of the US-based assessment of radii of curvature, evaluated in a
23 subset of 4 subjects using the ISO 5725-2 framework was 1.7 mm and 1.3 mm in the
24 in the frontal and sagittal plane respectively (95 % CI = 3.5 mm and = 2.6 mm
25 respectively). Out of the 13 subjects included, the ischial tuberosity border was
26 visible on the US image of 7 healthy subjects only. The mean of differences
27 computed on the 7 subjects using Bland-Altman plots were +3.3 mm and -5.7 mm
28 in the frontal and sagittal planes respectively. The corresponding 95% CI in the
29 frontal and sagittal planes were respectively 1.8 mm and 3.7 mm. These differences
30 however were not statistically significant (Wilcoxon signed-rank test). More effort
31 is needed to establish and standardise optimal measurement procedures and test
32 protocols for the assessment of geometrical features of the IT using US.

33 **1 INTRODUCTION**

34 A Pressure Ulcer (PU) is defined as “*a localized injury to the skin and underlying*
35 *soft tissue, usually over a bony prominence, caused by sustained pressure, shear or*
36 *a combination of these*” (NPUAP, EPUAP, PPPIA, 2014). It is a complication pri-
37 marily related to the care and treatment of individuals who have difficulty moving
38 or changing positions: for example, those people with a disability and the elderly
39 (Demarré et al., 2015). It appears in situations where excessive mechanical loads
40 are applied to the skin, such as, for example, during mechanical interaction between

41 a person and support surfaces (hospital bed) or medical devices (Manual Wheel-
42 chair, prosthetic socket, exoskeleton, etc.). PU prevention remains a major health
43 challenge for Europe due to the human and financial cost of prolonged hospitaliza-
44 tion, reduced quality of life, loss of autonomy and social isolation. However, current
45 risk assessment tools do not allow for a correct identification of the risks nor putting
46 an effective prevention in place (Coleman et al., 2013).

47 In the literature, a lot of research has sought to explain soft tissue injury risk factors
48 in terms of the local mechanical environment (i.e. internal stresses and strains that
49 satisfy mechanical equilibrium) within soft tissue (Oomens et al., 2015). In
50 particular, it has been shown by combining an animal model of Deep Tissue Injury
51 with computational modeling that direct deformation damage was only apparent
52 when a certain strain threshold was exceeded (Ceelen et al., 2008). In humans,
53 computational modelling of load-bearing soft tissue has shown that bony
54 prominences induce substantial stress concentrations, which explains why these
55 areas are vulnerable to pressure ulcers (Linder-Ganz et al., 2008). Laboratory and
56 animal studies propose several aetiological mechanisms by which stress and internal
57 strain interact with damage thresholds to result in pressure ulcer development
58 including localized ischaemia (Loerakker et al., 2011), reperfusion injury (Jiang et
59 al., 2011), impaired lymphatic drainage (Gray et al., 2016). and sustained cell
60 deformation (Bouten et al., 2003; Gefen et al., 2008)

61
62 Based on the rationale that elucidating the relationship between external loads
63 and internal local stresses and strains within loaded soft tissues has the potential of
64 improving the management and prevention of PUs, several Finite Element (FE)
65 models of the buttock have been proposed in the literature based on MRI or CT scan
66 data (Al-Dirini et al., 2016; Levy et al., 2013; Linder-Ganz et al., 2007; Luboz et
67 al., 2018; Zeevi et al., 2017). Because of the limited availability of MRI or CT-Scan
68 systems and of the long segmentation time associated with the creation of full 3D
69 subject specific FE models from these imaging systems, all the studies in the liter-
70 ature included the data of only one individual (Al-Dirini et al., 2016; Luboz et al.,
71 2014). As far as the authors are aware of, the only attempts to account for this var-
72 iability were limited to (i) semi-3D modelling (N=6 able-bodied volunteers in
73 (Linder-Ganz et al., 2007); N=12 in (Linder-Ganz et al., 2008); and N=6 in (Linder-
74 Ganz et al., 2009)) and (ii) one attempt at 3D modelling (N=6 in (Moerman et al.,
75 2017)). In addition, the representation of a realistic unloaded sitting position is jeop-
76 arded by the experimental limitations of MRIs and CT-scans: Long acquisition
77 times of MR imaging prevent a prolonged unloaded sitting configuration without
78 resorting to devices (Al-Dirini et al., 2016) while the confinement of the scanner
79 limits the acquisition to the lying position only (Luboz et al., 2014).

80
81 Recent developments in 3D reconstruction techniques from low dose calibrated
82 bi-planar X-ray imaging (EOS imaging, Paris, France) provide a promising
83 alternative tool for patient-specific validated 3D modelling of the pelvis (Ghostine
84 et al., 2017). Moreover, unlike CT scanner or MRI systems where the patient is in

85 a supine position, this technique provide bi-planar images of the subject in a weight-
86 bearing position.

87
88 In a previous study, and as an alternative to MRI-based/CT-scan-based assess-
89 ment, a methodology combining low-dose biplanar X-ray images (EOS imaging,
90 Paris, France), B-mode ultrasound images and optical scanner acquisitions in a non-
91 weight-bearing sitting posture has been proposed for the fast generation of patient-
92 specific FE models of the buttock and applied to 6 healthy subjects (Macron et al.,
93 2018). To investigate the ability of a local model of the region beneath the ischium
94 to capture the internal response of the buttock soft tissues predicted by a complete
95 3D FE model from a limited number of parameters, a simplified model was devel-
96 oped based on data compatible with daily clinical routine (Macron et al., 2020).
97 This study highlighted that the local mechanical environment within soft tissues is
98 very sensitive (in the statistical sense i.e. variance-based sensitivity analysis) to the
99 geometry of bony prominences and the relative thickness of the different soft tissue
100 elements. Of particular interest, the sensitivity analysis showed that the maximum
101 shear strain in the muscle tissue was very sensitive (29%) to the radius of curvature
102 of the ischium in the plane perpendicular to the shortest radius of curvature. These
103 results are in line with other results in the literature supporting the widely accepted
104 idea that bone geometry will affect internal stresses and strains occurring under
105 bony prominences (see for example (Gefen, 2010; Luboz et al., 2015) for heel ul-
106 cers).

107
108 B-mode ultrasound (US) imaging represents a promising alternative for as-
109 sessing geometrical feature-related risk factor bedside or in a clinic with standard
110 medical equipment. US imaging offers the advantages of being portable, non-inva-
111 sive, with few contraindications and rapid result interpretation. There is therefore a
112 high interest in the community for developing clinical protocols that are suited to
113 reliable parameter assessment (Akins et al., 2016; Gabison et al., 2019; Swaine et
114 al., 2018). If the measurement of the adipose and muscle tissue thicknesses in the
115 vicinity of the ischium using US has been shown to be both reliable and highly
116 correlated with MRI assessment (Akins et al., 2016), the measurement of the radius
117 of curvature of the ischium, was, on the contrary, reported to have a poor inter op-
118 erator reliability (Akins et al., 2016; Swaine et al., 2018).

119
120 In this perspective, we propose to evaluate, in this exploratory study, the agreement
121 between US-derived and bi-planar X-ray radiography-derived measurements of
122 geometrical features of the Ischial Tuberosity (IT) in a realistic loaded sitting
123 position in healthy volunteers, to quantify the global standard deviation of
124 reproducibility using the ISO standard 2725-2 and to quantify the influence of the
125 angular position of the pelvis in the seated position on the US-based assessment of
126 radii of curvature

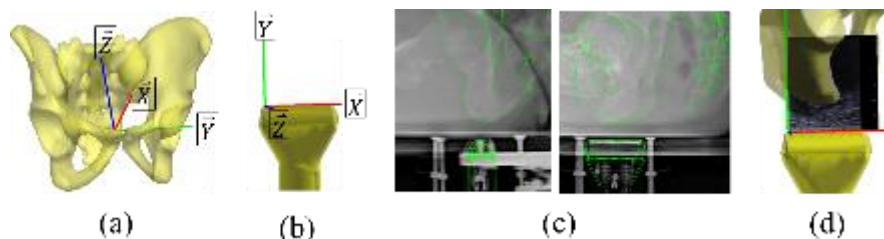
155 slowly unload his weight with his arms while visually keeping the ischium as
 156 aligned as possible with the probe (figure 1(b-c)). This allowed to measure soft tis-
 157 sue thickness in the unloaded position. An additional pair of radiographs was also
 158 acquired in the standardized free standing position (Faro et al., 2004) for the purpose
 159 of 3D reconstruction of the pelvis from the EOS radiographs according to the pro-
 160 cedure developed previously by (Mitton et al., 2006)

161 2.2 Data Analysis

162 2.2.1 Bimodal image registration

163 3D reconstruction of the pelvis (figure 2(a)) was performed from the EOS radi-
 164 ographs in the standing position according to the procedure developed previously
 165 by (Mitton et al., 2006). The 3D subject-specific model of the pelvis was then pro-
 166 jected on the frontal and sagittal radiographs in the loaded sitting positions (in both
 167 the acquisition with the US probe in the frontal plane and the acquisition with the
 168 US probe in the sagittal plane). The position of the pelvis was manually adjusted
 169 until the contours matched those of the radiographs (figure 2(c)). The pelvic coordi-
 170 nate system (figure 2(a)) was defined from the left and right acetabula and S1
 171 endplate of the 3D reconstruction following the definition given by (Dubois, 2014).
 172

173 Similarly, the 3D CAD model of the linear US probe (figure 2(b)) was projected
 174 on the frontal and sagittal radiographs in the loaded sitting positions. The position
 175 was manually adjusted until the contours matched those of the radiographs (figure
 176 2(c)). The probe coordinate system (figure 2(b)) was defined from the corners of
 177 the top part of the probe (transducer array). The 2D US image was positioned in the
 178 3D EOS cabin space using the probe coordinate system (figure 2(d)).
 179



180
 181 *Figure 2: (a) 3D reconstruction of the pelvis and associated coordinate system (b) 3D CAD*
 182 *model of the linear US probe and associated coordinate system (c) cropped frontal and*
 183 *sagittal radiographs in the loaded sitting position with projection of i) 3D reconstruction of*
 184 *the pelvis and ii) 3D CAD model of the probe respectively iv) Bimodal image registration*

185 2.2.2 Assessment of morphological parameter

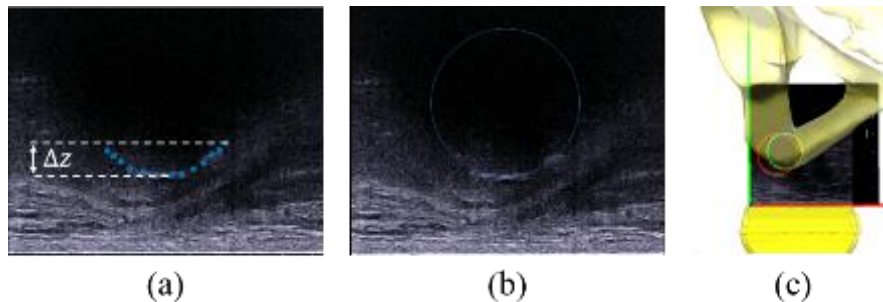
186 **US-based assessment of radii of curvature (US-RoC) and soft tissue thickness**
 187 **(US-STT).** In both acquisitions (US probe in the frontal and sagittal planes
 188 respectively), 10 points were manually selected on the lowest part of the ischial
 189 tuberosity border visible on the US image in the seated position (figure 3(a)). The

190 radius of curvature (figure 3(b)) was computed using a least-squares regression
 191 procedure using a custom-made MATLAB subroutine (MathWorks, Natick, MA,
 192 USA). The height of the selection, denoted Δz , was defined as the difference
 193 between maximum-altitude and the minimum-altitude points (figure 3(a)). The
 194 vertical component of the distance between lowest point of the IT and overlying
 195 skin surface was used to define the soft tissue thickness.

196

197 **EOS-based assessment of the radii of curvature (EOS-RoC) and soft tissue**
 198 **thickness (EOS-STT).** In both acquisitions (US probe in the frontal and sagittal
 199 planes respectively), the pelvis surface mesh intersecting points with the US probe
 200 plane were computed using a custom-made MATLAB subroutine (MathWorks, Na-
 201 tick, MA, USA). The points in the range Δz (previously determined for each con-
 202 figuration and for each subject) from the minimum-altitude point were selected. The
 203 radius of curvature was computed using the same least-squares regression procedure
 204 as for the US-based data points. Both the US-based and EOS-based least squares
 205 fitting circles were superposed on US image and 3D reconstruction of pelvis in the
 206 EOS cabin (global) coordinate system (figure 3(c)). The vertical component of the
 207 distance between the lowest point of the pelvis surface mesh intersecting with the
 208 US probe plane and overlying skin surface was used to define the soft tissue thick-
 209 ness.

210



211

212 *Figure 3: (a) Points manually selected on the inferior border of each IT (b) least squares*
 213 *fitting circle (c) US-based and EOS-based least squares fitting circles (respectively in red*
 214 *and green) superposed on US image and 3D reconstruction of pelvis in the EOS cabin (global*
 215 *coordinate system).*

216

2.2.3 Statistical analysis

217

218 On a subset of 4 subjects (26 ± 1 year old), the inter-observer reproducibility
 219 standard deviation (SD_r) of the US-based assessment of radii of curvature was
 220 computed using the method described in the ISO standard 5725 (ISO, 1994). Each
 221 US image was processed 3 times by 3 operators in both acquisitions (US probe in
 222 the frontal and sagittal planes respectively). Reproducibility was estimated by
 223 computing the 95% confidence interval ($95\%CI = 2 \cdot SD_r$).

224

The agreement between the US-based and EOS-based assessment of radii of
 curvature of the IT was described graphically with a Bland-Altman plot with mean

225 of differences, reported with corresponding 95% confidence interval (CI), and lower
 226 and upper limits of agreement, calculated as $\text{mean} \pm 1.96 \times \text{standard deviation}$.
 227 Differences were assessed using a Wilcoxon-Signed-Rank Test (paired data) at the
 228 default 5 % significance level and was further described

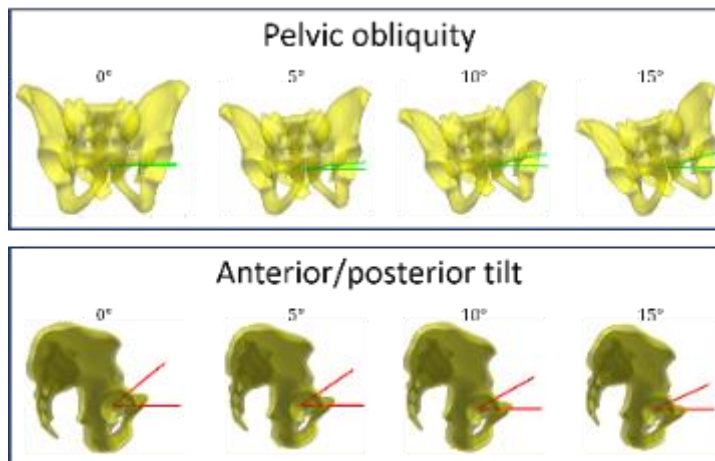
229 **2.2.4 Impact of pelvis angular position on the computed radii of curvature**

230 A sensitivity study was performed to quantify the influence of the angular position
 231 of the pelvis in the seated position on the US-based assessment of radii of curvature.
 232

233 Prior to this step, the maximum difference in the relative angular position of each
 234 pelvis to that of the average pelvic pose (averaged position and orientation) was
 235 quantified as follows: For each acquisition, the angular position of the pelvis frame
 236 was expressed in the EOS cabin (global) coordinate system. The orientation matrix
 237 of the relative angular position of each pelvis to that of the average pelvic pose was
 238 calculated. The decomposition of the rotation matrix was done using the XYZ rota-
 239 tion sequences of Cardan angles. The averaged position and orientation of all the
 240 pelvic frames was computed.

241

242 The procedure for the sensitivity study was the following: Each pelvis was re-
 243 positioned in the averaged pelvic position (i.e. transformed so that the pelvis frame is
 244 aligned with that of the average pelvic pose). Then, for each pelvis, the pelvic obli-
 245 quity (rotation around the global X-axis) and the anterior/posterior tilt (rotation
 246 around the global Y-axis) were modified independently by an increment of 5°, 10°
 247 and 15°. For each configuration, the (EOS-based) radius of curvature was computed
 248 according to the procedure described in section 2.2.2.
 249



250

251 *Figure 4: To assess the impact of small perturbations of the pelvic angular position during*
 252 *seating on the radius of curvature estimated using the procedure described in section 2.2.2,*
 253 *both (a) the pelvic obliquity and (b) the anterior/posterior tilt were modified independently*
 254 *by an increment of 5°, 10° and 15° and the radius of curvature was computed.*

255 **3 RESULTS**

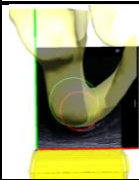
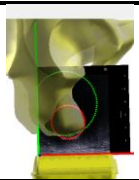
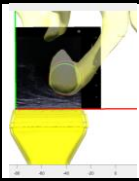
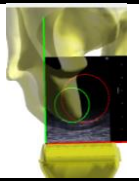
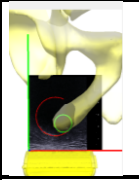
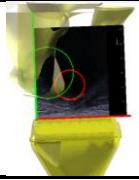
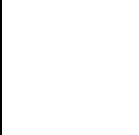
256 Out of the 13 subjects included, the ischial tuberosity border was visible on the
 257 US image of 7 healthy subjects only (4 men and 3 women; age: 28 ± 6 years, weight:
 258 66 ± 7 kg, BMI: 21.6 ± 2.2 kg/m²). The results presented in this section therefore
 259 focuses on these 7 subjects only.

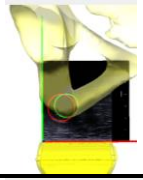
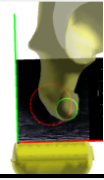
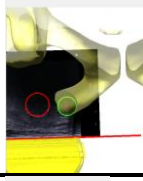
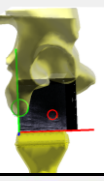
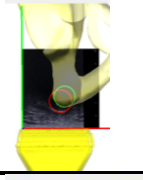
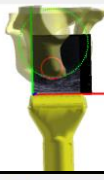
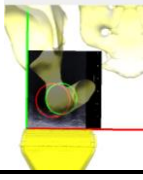
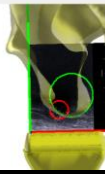
260 **3.1 Assessment of morphological parameter**

261 The reproducibility of the US-based assessment of radii of curvature was 1.7 mm
 262 (95% CI = 3.5 mm) in the frontal plane and 1.3 mm (95 % CI = 2.6 mm) in the
 263 sagittal plane respectively.
 264

265 The results of the bimodal image registration and of the assessment of the radii
 266 of curvature and soft tissue thickness in both acquisitions (US probe in the frontal
 267 and sagittal planes respectively) are given in Table 1 below together with the results
 268 of the US-based and EOS-based assessment of Radii Of Curvature (RoC) and Soft
 269 Tissue Thickness (STT).

270
 271 *Table 1: Results of the bimodal image registration and of the assessment of the radii of*
 272 *curvature and soft tissue thickness in both acquisitions. US-based (red) and EOS-based*
 273 *(green) least squares fitting circles are superposed on US image and 3D reconstruction of*
 274 *pelvis in the EOS cabin (global coordinate system). All dimensions are in mm.*

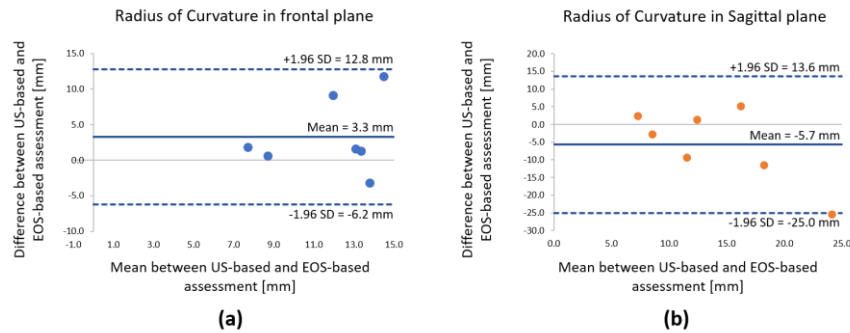
	Probe in the frontal plane (mm)			Probe in the sagittal plane (mm)		
1		US-ROC	12.2		US-ROC	12.5
		EOS-RoC	15.4		EOS-RoC	23.9
		Difference	-3.2		Difference	-11.4
		US-STT	11.7		US-STT	12.2
		EOS-STT	14.4		EOS-STT	14.5
		Difference	-2.7		Difference	-2.3
2		US-ROC	13.9		US-ROC	18.8
		EOS-RoC	12.3		EOS-RoC	13.6
		Difference	1.6		Difference	5.2
		US-STT	11.6		US-STT	16.1
		EOS-STT	11.5		EOS-STT	16.3
		Difference	0.1		Difference	-0.2
3		US-ROC	16.5		US-ROC	13.1
		EOS-RoC	7.4		EOS-RoC	11.7
		Difference	9.1		Difference	1.4
		US-STT	12.8		US-STT	12.6
		EOS-STT	14		EOS-STT	14.8
		Difference	-1.2		Difference	-2.2
4		US-ROC	20.4	US-ROC	8.5	
		EOS-RoC	8.6	EOS-RoC	6.0	
		Difference	11.8	Difference	-2.7	
		US-STT	16.3	US-STT	10.2	
		EOS-STT	12.6	EOS-STT	21.5	

		Difference	3.7		Difference	-11.3
5		US-ROC	8.6		US-ROC	7.2
		EOS-RoC	6.8		EOS-RoC	9.9
		Difference	1.8		Difference	-2.7
		US-STT	15.7		US-STT	13.9
		EOS-STT	16.6		EOS-STT	19.1
		Difference	-0.9		Difference	-5.2
6		US-ROC	9		US-ROC	11.4
		EOS-RoC	8.4		EOS-RoC	36.8
		Difference	0.6		Difference	-25.4
		US-STT	13.3		US-STT	16.4
		EOS-STT	16.3		EOS-STT	18.1
		Difference	-3		Difference	-1.7
7		US-ROC	14		US-ROC	6.9
		EOS-RoC	12.7		EOS-RoC	16.2
		Difference	1.3		Difference	-9.3
		US-STT	8.8		US-STT	8.7
		EOS-STT	11.7		EOS-STT	11.2
		Difference	-2.9		Difference	-2.5

275 Figure 5 below shows the Bland-Altman plot describing the agreement between
 276 US-based and EOS-based assessment of radii of curvature in the frontal and sagittal
 277 planes respectively. The bias or mean of differences were +3.3 mm and -5.7 mm in
 278 the frontal and sagittal planes respectively. The mean differences are not zero in
 279 either case and this means that, on average, the US measures 3.3 mm more than the
 280 EOS-based in the frontal plane (overestimation) and 5.7 less in the sagittal plane
 281 (underestimation) respectively. As can be further seen, the differences were of both
 282 positive and negative values. The corresponding 95% CI in the frontal and sagittal
 283 planes were respectively 1.8 mm and 3.7 mm. The lower and upper limits of agree-
 284 ment were respectively -6.2 mm and 12.8 mm in the frontal plane. The lower and
 285 upper limits of agreement were respectively -25 mm and 13.6 mm in the sagittal
 286 plane.

287 Results of the Wilcoxon signed-rank-test, however did not allow rejecting the
 288 null hypothesis about the differences between the US-based and EOS-based ROC
 289 (p values of 0.16 and 0.30 in the frontal and sagittal planes respectively). Determin-
 290 ing soft tissue thickness in the unloaded position was not always possible because
 291 the IT was not systematically visible on the US images.

292
 293



294
295
296
297

Figure 5 Plot of differences between US-based and EOS-based assessment of radii of curvature vs. the mean of the two measurements (data from table 1) in the frontal (a) and sagittal (b) planes respectively.

298

3.2 Impact of pelvis angular position on the computed radii of curvature

299

The maximum difference in the relative angular position of each pelvis to that of the average pelvic pose was 17° (anterior posterior tilt). This allows to estimate an order of magnitude of the inter-individual variability in pelvis pose in realistic loaded sitting position in healthy volunteers.

300

301

302

303

304

Increasing the pelvic obliquity, lead, on average, to a decrease in the EOS-based radius of curvature assessed (0.80 mm, 1.5 mm and 18 mm respectively for a rotation of 5° , 10° and 15° in the frontal plane; 0.2 mm, 0.6 mm and 0.1 mm respectively in the sagittal plane for a rotation of 5° , 10° and 15°).

305

306

307

308

309

310

311

312

313

4 DISCUSSION

314

The objective of this exploratory study was to evaluate the agreement between Ultrasound-based and bi-planar X-Ray radiography-based assessment of the geometrical features of the Ischial Tuberosity in the context of the prevention of seating-related pressure injury. Assessment of the geometry of bony prominences is important for PU prevention because the local mechanical environment within soft tissues – which has been shown to be a correlated to soft tissue injury risk (Ceelen et al., 2008; Loerakker et al., 2011) - is very sensitive (in the statistical sense i.e. variance-based sensitivity analysis) to the geometry of bony prominences (Gefen, 2010; Luboz et al., 2015; Macron et al., 2020). Based on these results, establishing routine ultrasound scans of the ischium could potentially lead to development of new ultrasound-based risk assessment tools that are more specific for identifying susceptibility to seating-related pressure injuries, particularly

315
316
317
318
319
320
321
322
323
324
325

326 considering the individual's internal anatomy. This probably explains the increasing
327 enthusiasm of the community for the measurement of this geometrical feature-
328 related risk factor using medical imaging.

329

330 Results obtained in this contribution on N=7 healthy however suggest that more
331 effort is needed to establish and standardise optimal measurement and processing
332 procedures and test protocols for the assessment of geometrical features of the IT
333 using US. On average, US-based assessment of radius of curvature underestimated
334 that of the EOS-based in the frontal plane and overestimated in the sagittal plane
335 respectively. This may be partly due to the fact that approximating the ischial tu-
336 berosity by a torus (two radii of curvature in the frontal and sagittal planes which
337 are not necessarily aligned with the IT orientation) is too gross and leads to biases
338 in the assessment of morphological parameters. This can also be explained by the
339 ultrasound imaging artefacts inherent to this technology, which, make the detection
340 of bone contours less robust. The fitting of the circle is also dependent on the pelvic
341 posture in sitting. If participants are sitting forward or backward, the circumference
342 of the lowest point of the IT changes dramatically and it is very difficult to measure
343 since the IT is flattened.

344

345 In the literature, Swaine and colleagues (2008) represented the ischium using
346 two radii of curvature (along anatomical planes, representing the shortest and
347 longest axis) – other authors limiting the analysis to only one plane (Akins et al.,
348 2016). If a good inter-rater reliability for soft tissue thickness assessment of the soft
349 tissue layers overlying inferior curve of IT (skin & fat, tendon & muscle, while
350 thickness) are generally reported, (Swaine et al., 2018) observed a poor inter-rater
351 reliability of sonographers in measuring diameter of the inferior curve of IT. This
352 result is in contrast to that reported by (Akins et al., 2016) who reported an higher
353 concordance value (ICC = 0.712). However, this earlier study utilised a single scan
354 operator to acquire images and two operators to post-process the data on the same
355 images. Such a post processing protocol will inevitably impact the decisions an
356 operator must make during real-time image acquisition and measurement. In this
357 study, a custom-made stool was designed to eliminate the uncertainty related to
358 exclude the impact of inter-operator variability in transducer rotation, medial/lateral
359 and cranial/caudal tiling and pressure exerted over the tissues during examinations.
360 Yet, the reproducibility of the US-based assessment of radii of curvature were
361 relatively high (95% CI = 3.5 mm in the frontal plane and 95 % CI = 2.6 mm in the
362 sagittal plane respectively), highlighting the effect of the procedure for extracting
363 morphologic parameters.

364

365 The results obtained in our study for US-based assessment of radius of curvature
366 are 13.5 ± 4.1 mm (range [8.6 mm – 20.4 mm]) in the frontal plane and 11.2 ± 4.2 mm
367 (range [6.9 mm – 18.8 mm]) in sagittal plane respectively. This is within the same
368 range as reported by (Akins et al. 2016) (between 8.5 mm and 20.0 mm) and
369 (Swaine et al. 2018) (24.2 ± 5 mm in the short axis, 30.0 ± 8 mm in the long axis,
370 respectively. Out of the 13 subjects included in the studies of (Macron et al., 2020,

2018), 6 were excluded for the assessment of the IT curvature in this study since the ischium was not visible due to thick tissue layer of subjects. This can emphasize US-based measurement of IT curvature is highly dependent not only on operator but also the subject. The use of a linear probe represents a limitation of the current study since it is not adapted it has limited penetration. As a perspective work, the use of a curvilinear ultrasound probe will be explored to allow for imaging patients where the image depth penetration and width capture requirements are greater, such as young trauma patients with high muscle bulk, morbidly obese patients with significant subcutaneous fat and patients with fluid overload.

The results obtained in this study for EOS-based assessment of radius of curvature are 10.2 ± 3.2 mm (range [6.8 mm – 15.4 mm]) in the frontal plane and 16.9 ± 10.4 mm (range [6.0 mm – 36.8 mm]) in sagittal plane respectively. A plausible explanation for the discrepancy between US-based and EOS-based assessment of radii of curvature is the level of accuracy if 3D-reconstructions from bi-planar X-ray images compared to CT-scan data. It has been reported that shape differences between 3D models obtained from bi-planar X-rays and CT-scan are, on average 1.6 mm (Mitton et al., 2006).

Recent studies suggest that B-mode Ultrasound imaging constitutes a promising alternative that could overcome some limitations of MRI. Further investigations need to be done in order to estimate the system's overall accuracy in a controlled laboratory setting using precisely built phantom. To make a conclusion on the potential clinical accuracy, the differences between the clinical and laboratory settings must be carefully examined.

References

- Akins, J.S., Vallely, J.J., Karg, P.E., Kopplin, K., Gefen, A., Poojary-Mazzotta, P., Brienza, D.M., 2016. Feasibility of freehand ultrasound to measure anatomical features associated with deep tissue injury risk. *Med. Eng. Phys.* 38, 839–844. <https://doi.org/10.1016/j.medengphy.2016.04.026>
- Al-Dirini, R.M.A., Reed, M.P., Hu, J., Thewlis, D., 2016. Development and Validation of a High Anatomical Fidelity FE Model for the Buttock and Thigh of a Seated Individual. *Ann. Biomed. Eng.* 44, 2805–2816. <https://doi.org/10.1007/s10439-016-1560-3>
- Bouten, C. V., Oomens, C.W., Baaijens, F.P., Bader, D.L., 2003. The etiology of pressure ulcers: skin deep or muscle bound? *Arch. Phys. Med. Rehabil.* 84, 616–619. <https://doi.org/10.1053/apmr.2003.50038>
- Ceelen, K.K., Stekelenburg, A., Loerakker, S., Strijkers, G.J., Bader, D.L., Nicolay, K., Baaijens, F.P.T., Oomens, C.W.J., 2008. Compression-induced damage and internal tissue strains are related. *J. Biomech.* 41, 3399–3404. <https://doi.org/10.1016/j.jbiomech.2008.09.016>
- Coleman, S., Gorecki, C., Nelson, E.A., Closs, S.J., Defloor, T., Halfens, R., Farrin, A., Brown, J., Schoonhoven, L., Nixon, J., 2013. Patient risk factors for

- 414 pressure ulcer development: Systematic review. *Int. J. Nurs. Stud.* 50, 974–
415 1003. <https://doi.org/10.1016/j.ijnurstu.2012.11.019>
- 416 Demarré, L., Van Lancker, A., Van Hecke, A., Verhaeghe, S., Grypdonck, M.,
417 Lemey, J., Annemans, L., Beeckman, D., 2015. The cost of prevention and
418 treatment of pressure ulcers: A systematic review. *Int. J. Nurs. Stud.* 52,
419 1754–1774. <https://doi.org/10.1016/j.ijnurstu.2015.06.006>
- 420 Dubois, G., 2014. Contribution à la modélisation musculo-squelettique personnali-
421 sée du membre inférieur combinant stéréoradiographie et ultrason. (phd-
422 thesis). Ecole nationale supérieure d'arts et métiers - ENSAM.
- 423 Faro, F.D., Marks, M.C., Pawelek, J., Newton, P.O., 2004. Evaluation of a func-
424 tional position for lateral radiograph acquisition in adolescent idiopathic
425 scoliosis. *Spine* 29, 2284–2289.
- 426 Gabison, S., Hayes, K., Campbell, K.E., Swaine, J.M., Craven, B.C., 2019. Ultra-
427 sound imaging of tissue overlying the ischial tuberosity: Does patient po-
428 sition matter? *J. Tissue Viability*. <https://doi.org/10.1016/j.jtv.2019.07.001>
- 429 Gefen, A., 2010. The biomechanics of heel ulcers. *J. Tissue Viability* 19, 124–131.
430 <https://doi.org/10.1016/j.jtv.2010.06.003>
- 431 Gefen, A., van Nierop, B., Bader, D.L., Oomens, C.W., 2008. Strain-time cell-death
432 threshold for skeletal muscle in a tissue-engineered model system for deep
433 tissue injury. *J. Biomech.* 41, 2003–2012. <https://doi.org/10.1016/j.jbiomech.2008.03.039>
- 435 Ghostine, B., Sauret, C., Assi, A., Bakouny, Z., Khalil, N., Skalli, W., Ghanem, I.,
436 2017. Influence of patient axial malpositioning on the trueness and preci-
437 sion of pelvic parameters obtained from 3D reconstructions based on bi-
438 planar radiographs. *Eur. Radiol.* 27, 1295–1302.
439 <https://doi.org/10.1007/s00330-016-4452-x>
- 440 Gray, R.J., Voegeli, D., Bader, D.L., 2016. Features of lymphatic dysfunction in
441 compressed skin tissues – Implications in pressure ulcer aetiology. *J. Tis-
442 sue Viability* 25, 26–31. <https://doi.org/10.1016/j.jtv.2015.12.005>
- 443 ISO, 1994, ISO 5725-2 Accuracy (Trueness and Precision) of Measurements Meth-
444 ods and Results.—Part 2: Basic Method for the Determination of Repeat-
445 ability and Reproducibility of a Standard Measurement Method, Interna-
446 tional Organisation for Standardisation, Geneva, Switzerland (1994),
447 Retrieved from <https://www.iso.org/standard/69419.html>
- 448 Jiang, L., Tu, Q., Wang, Y., Zhang, E., 2011. Ischemia-reperfusion injury-induced
449 histological changes affecting early stage pressure ulcer development in a
450 rat model. *Ostomy. Wound Manage.* 57, 55–60.
- 451 Levy, A., Kopplin, K., Gefen, A., 2013. Simulations of skin and subcutaneous tissue
452 loading in the buttocks while regaining weight-bearing after a push-up in
453 wheelchair users. *J. Mech. Behav. Biomed. Mater.* 28, 436–447.
454 <https://doi.org/10.1016/j.jmbbm.2013.04.015>

- 455 Linder-Ganz, E., Shabshin, N., Itzchak, Y., Gefen, A., 2007. Assessment of me-
456 chanical conditions in sub-dermal tissues during sitting: a combined ex-
457 perimental-MRI and finite element approach. *J. Biomech.* 40, 1443–1454.
458 <https://doi.org/10.1016/j.jbiomech.2006.06.020>
- 459 Linder-Ganz, E., Shabshin, N., Itzchak, Y., Yizhar, Z., Siev-Ner, I., Gefen, A.,
460 2008. Strains and stresses in sub-dermal tissues of the buttocks are greater
461 in paraplegics than in healthy during sitting. *J. Biomech.* 41, 567–580.
462 <https://doi.org/10.1016/j.jbiomech.2007.10.011>
- 463 Linder-Ganz, E., Yarnitzky, G., Yizhar, Z., Siev-Ner, I., Gefen, A., 2009. Real-time
464 finite element monitoring of sub-dermal tissue stresses in individuals with
465 spinal cord injury: Toward prevention of pressure ulcers. *Ann. Biomed.*
466 *Eng.* 37, 387–400. <https://doi.org/10.1007/s10439-008-9607-8>
- 467 Loerakker, S., Manders, E., Strijkers, G.J., Nicolay, K., Baaijens, F.P.T., Bader,
468 D.L., Oomens, C.W.J., 2011. The effects of deformation, ischemia, and
469 reperfusion on the development of muscle damage during prolonged load-
470 ing. *J. Appl. Physiol.* 111, 1168–1177. <https://doi.org/10.1152/jappphysiol.00389.2011>
- 471
- 472 Luboz, V., Bailet, M., Boichon Grivot, C., Rochette, M., Diot, B., Bucki, M., Payan,
473 Y., 2018. Personalized modeling for real-time pressure ulcer prevention in
474 sitting posture. *J. Tissue Viability* 27, 54–58.
475 <https://doi.org/10.1016/j.jtv.2017.06.002>
- 476 Luboz, V., Perrier, A., Bucki, M., Diot, B., Cannard, F., Vuillerme, N., Payan, Y.,
477 2015. Influence of the Calcaneus Shape on the Risk of Posterior Heel Ulcer
478 Using 3D Patient-Specific Biomechanical Modeling. *Ann. Biomed. Eng.*
479 43, 325–335. <https://doi.org/10.1007/s10439-014-1182-6>
- 480 Luboz, V., Petrizelli, M., Bucki, M., Diot, B., Vuillerme, N., Payan, Y., 2014. Bio-
481 mechanical modeling to prevent ischial pressure ulcers. *J. Biomech.* 47,
482 2231–2236. <https://doi.org/10.1016/j.jbiomech.2014.05.004>
- 483 Macron, A., Pillet, H., Doridam, J., Rivals, I., Sadeghinia, M.J., Verney, A., Rohan,
484 P.-Y., 2020. Is a simplified Finite Element model of the gluteus region able
485 to capture the mechanical response of the internal soft tissues under com-
486 pression? *Clin. Biomech.* 71, 92–100. <https://doi.org/10.1016/j.clinbiomech.2019.10.005>
- 487
- 488 Macron, A., Pillet, H., Doridam, J., Verney, A., Rohan, P.-Y., 2018. Development
489 and evaluation of a new methodology for the fast generation of patient-
490 specific Finite Element models of the buttock for sitting-acquired deep tis-
491 sue injury prevention. *J. Biomech.* 79, 173–180.
492 <https://doi.org/10.1016/j.jbiomech.2018.08.001>
- 493 Mitton, D., Deschênes, S., Laporte, S., Godbout, B., Bertrand, S., Guise, J.A. de,
494 Skalli, W., 2006. 3D reconstruction of the pelvis from bi-planar radiog-
495 raphy. *Comput. Methods Biomech. Biomed. Engin.* 9, 1–5.
496 <https://doi.org/10.1080/10255840500521786>

- 497 Moerman, K.M., van Vijven, M., Solis, L.R., van Haften, E.E., Loenen, A.C.Y.,
498 Mushahwar, V.K., Oomens, C.W.J., 2017. On the importance of 3D, geo-
499 metrically accurate, and subject-specific finite element analysis for evalu-
500 ation of in-vivo soft tissue loads. *Comput. Methods Biomech. Biomed.*
501 *Engin.* 20, 483–491. <https://doi.org/10.1080/10255842.2016.1250259>
- 502 National Pressure Ulcer Advisory Panel, European Pressure Ulcer Advisory Panel,
503 and Pan Pacific Pressure Injury Alliance, 2014, National Pressure Ulcer
504 Advisory Panel, European Pressure Ulcer Advisory Panel, & Pan Pacific
505 Pressure Injury Alliance Prevention and Treatment of Pressure Ulcers:
506 Quick Reference Guide. Guidelines, Retrieved from
507 [http://www.npuap.org/wp-content/uploads/2014/08/Quick-Reference-](http://www.npuap.org/wp-content/uploads/2014/08/Quick-Reference-Guide-DIGITAL-NPUAP-EPUAP-PPPIA-Jan2016.pdf)
508 [Guide-DIGITAL-NPUAP-EPUAP-PPPIA-Jan2016.pdf](http://www.npuap.org/wp-content/uploads/2014/08/Quick-Reference-Guide-DIGITAL-NPUAP-EPUAP-PPPIA-Jan2016.pdf) (2014)
- 509 Oomens, C.W.J., Bader, D.L., Loerakker, S., Baaijens, F., 2015. Pressure Induced
510 Deep Tissue Injury Explained. *Ann. Biomed. Eng.* 43, 297–305.
511 <https://doi.org/10.1007/s10439-014-1202-6>
- 512 Swaine, J.M., Moe, A., Breidahl, W., Bader, D.L., Oomens, C.W.J., Lester, L.,
513 O’Loughlin, E., Santamaria, N., Stacey, M.C., 2018. Adaptation of a MR
514 imaging protocol into a real-time clinical biometric ultrasound protocol for
515 persons with spinal cord injury at risk for deep tissue injury: A reliability
516 study. *J. Tissue Viability, Seating Biomechanics* 27, 32–41.
517 <https://doi.org/10.1016/j.jtv.2017.07.004>
- 518 Zeevi, T., Levy, A., Brauner, N., Gefen, A., 2017. Effects of ambient conditions on
519 the risk of pressure injuries in bedridden patients-multi-physics modelling
520 of microclimate. *Int. Wound J.* <https://doi.org/10.1111/iwj.12877>
521