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1 **THERMAL OXIDATION OF DIALLYLBISPHENOL A - BISMALIMIDE NETWORKS. COMONOMER EFFECT**
2 **AND KINETIC MODELLING**

3

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10

11 **ABSTRACT**

12 Pure BMI resin based on 4,4'-bismaleimidodiphenylmethane (BMI) and its copolymers with various
13 quantities of 2,2'-diallylbisphenol A (BMI-DABPA 2-1, BMI-DABPA 1-1, BMI-DABPA 1-2) were thermally
14 aged. Ageing at 160°C was monitored by FTIR and showed the greatest reactivity of diallyl groups which
15 accelerate the degradation of BMI-DABPA copolymers. It was confirmed by a gravimetric study of
16 ageing under nitrogen or oxygen at 350 and 375°C. A co-oxidation kinetic model was proposed for
17 describing the oxidation of BMI and BMI-DABPA systems. The effect of the main kinetic parameters was
18 discussed from a parametric study. The main rate constants were estimated from the fitting of
19 experimental curves and comparable gravimetric data from literature.

20

21 **KEYWORDS**

22 Bismaleimide resins, 2,2'-Diallylbisphenol A, thermal oxidation, mass loss, kinetic modelling

23

24 **1. INTRODUCTION**

25 BMI resins were first obtained from homopolymerization of bismaleimide monomers, the most
26 common one being the 4,4'-bismaleimidodiphenylmethane (Figure 1a). Polymerization can be
27 achieved even in absence of peroxide or imidazole catalysts [^{1,2,3}] and gives networks with high glass
28 transition (300°C or more) [3,⁴] and interesting mechanical properties (specific strength at break) but
29 displaying a poor toughness (below 1 MPa.m^{1/2}) [4,⁵]. Many strategies were implemented for improving

30 this latter such as (i) increasing the distance between crosslink nodes or (ii) adding comonomers such as
31 for example 2,2'-diallylbisphenol A (DABPA – Figure 1b). This is the case of existing commercial systems
32 such Matrimid 5292 [6]. For example, a Allyl + BMI « copolymer » [7] displays stress at break and impact
33 resistance are respectively around 145 MPa and 12 kJ.m⁻², which is much higher than data given for the
34 « homopolymer » BMI (40-80 MPa for stress at break [4] and impact strength around 8 kJ.m⁻² [8]).

35 Such materials are usually employed in demanding applications where thermal stability is crucial.
36 Previous works address the case of various homopolymers where the non-reactive group between
37 maleimide groups was changed [9, 10, 11]. However, there is, to the best of our knowledge, very few
38 studies [12, 13] dealing with the effect of comonomers and in particular the effect of the BMI/diallyl
39 stoichiometric ratio on thermal stability.

40 Degradation of pure BMI was mostly investigated in non-isothermal conditions by means of classical
41 TGA tests [9, 10, 11]. However, isothermal ageing studies exist but are scarce [9, 14, 15, 16], which limits the
42 understanding of the degradation mechanism.

43 Ageing experiments must in general be used for predicting lifetime in service conditions. For that
44 purpose, it is well established that a kinetic model must be used. Kinetic parameters must correspond
45 to elementary processes involved in degradation, and obey Arrhenius law. The simulation of
46 experimental results allows an estimation of the values of the parameters used in kinetic models in
47 accelerated conditions. The extrapolation of those values at service temperatures allows to predict the
48 degradation rate at those conditions. A « proof of concept » of the predictive capability of kinetic
49 model was published by Colin et al [17] who successfully simulated the mass loss kinetics of a BMI based
50 material. However, the proposed kinetic model corresponds to the simple case where there is only one
51 sort of reactive unit in the material, which is clearly not the case in the case of BMI-DABPA networks.

52

53 In this paper, we will hence synthesize and degrade samples with various alkyl/maleimide
54 stoichiometry's in order to:

55 - investigate the effect of comonomers on stability for isothermal ageing under nitrogen, or under
56 oxygen by performing isothermal tests,

57 - characterize the chemical trackers of oxidation in link with the BMI-DABPA formulation,

58 - discuss on the effect of DABPA and propose a first kinetic model of degradation for pure BMI and BMI-
59 DABPA copolymers. We will focus on its capability to simulate mass loss since this latter is linked to
60 shrinkage and latter cracking [18, 19].

61

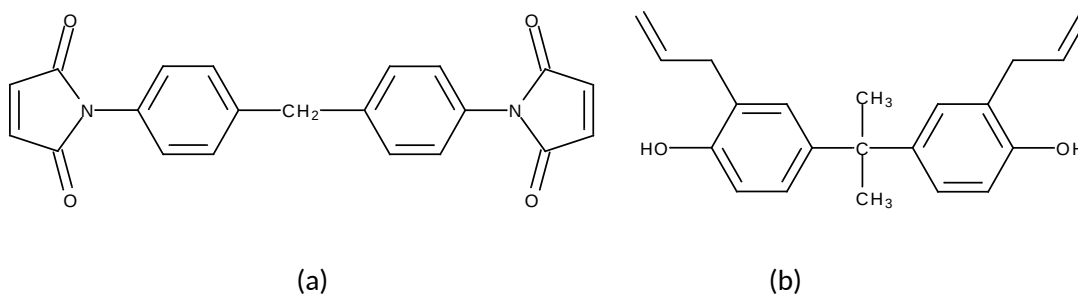
62 **2. EXPERIMENTAL**

63

64 **2.1. Materials**

65

66 Materials were synthesized using two comonomers given in Figure 1: 4,4'-
67 Bismaleimidodiphenylmethane (CAS: 13676-54-5 - ref 227463-100G supplied by Sigma Aldrich) and
68 2,2'-Diallylbisphenol A (CAS: 1745-89-7 - ref 413526-100ML supplied by Sigma Aldrich).



71 **Figure 1. Structure of 4,4'-Bismaleimidodiphenylmethane (a) and 2,2',diallylbisphenol A (b).**

72

73 Materials were obtained from the following curing cycles:

74 - for BMI films: Thickening of reactive mixture during 10 min at 170°C, then 10 min at 175°C after which
75 samples were pressed using a laboratory press (240 bars without use of spacer) during 1 h at 180°C + 1
76 h à 190°C + 2 h à 200°C. The obtained films have a thickness about 40 µm.

77 - for BMI-DABPA films: Thickening of reactive mixture during 30 min at 150°C + 20 min at 180°C after
78 which samples were pressed using a laboratory press (240 bars without use of spacer) 1 h at 180°C + 1 h
79 at 190°C + 2 h at 200°C. The obtained films have a thickness about 20 µm. Copolymers are detailed in
80 Table 1.

81

82 **2.2. Exposure conditions**

83 Samples were aged in ventilated ovens (AP60, SCS, France) under atmospheric air at 160°C. Ageing was
84 monitored by FTIR and elemental analysis.

85 Ageing under 100% N₂ or 100% O₂ atmosphere was performed in situ in TGA cell.

86

87 **2.3. Characterization methods**

88

89 **2.3.1. ThermoGravimetric Analysis**

90 TGA measurements were performed using a Q500 apparatus driven by QSeries Explorer (TA
91 Instruments). After a $20^{\circ}\text{C min}^{-1}$ heating, isothermal degradation was performed at a constant
92 temperature equal to 350 and 375°C either under 100% N_2 or 100% O_2 atmosphere supplied by a
93 continuous $50 \text{ ml}\cdot\text{min}^{-1}$ gas flow.

94

95 **2.3.2. Fourier Transform InfraRed spectroscopy**

96 FTIR spectroscopy in transmission mode was carried out using a Frontier spectrophotometer
97 (PerkinElmer) by averaging 8 scans at 1 cm^{-1} resolution between 400 and 4000 cm^{-1} .

98

99 **2.3.3. Elemental Analysis**

100 Carbon and hydrogen measurements were performed on a homemade Carbon / Hydrogen elemental
101 micro-analyzer (Institut des Sciences Analytiques, UMR5280 CNRS, Villeurbanne). About 1.5 mg of
102 sample weighted in silver cups (3.2×6 , Sántis Analytical AG, Teufen, Switzerland) dropped into a unit
103 combustion in a flow of $50 \text{ ml}\cdot\text{min}^{-1}$ of pure oxygen. The combustion system is equipped by two
104 furnaces held at 1050°C for the upper one and 850°C for the lower and contain a vertical glass
105 combustion tube, half filled with 11 cm of CuO oxidation catalyst (Copper oxide wire 0.7mm, Sántis
106 Analytical) and silver wool (Silberwolle Carl ROTH GmbH, Karlsruhe, Germany) used as halogens trap.
107 Carbon and hydrogen have been respectively turned into carbon dioxide (CO_2) and water (H_2O). The
108 measurements of both molecules have been done using a $\text{CO}_2/\text{H}_2\text{O}$ non-dispersive infrared detector
109 (Rosemount NGA 2000). A calibration has been daily established by measuring standards references
110 (molecules pure at 99.9%). Then up to 8 samples were injected. To be sure of the lack of calibration-
111 drift, 2 standards reference were introduced and measured as sample, every eight analyses. The
112 uncertainty of measurements has been determined at ± 0.10 for H measurement and ± 0.30 for
113 carbon measurement. Reference standards used for calibration and stability controls are high purity
114 compounds purchased from Sigma Aldrich corp. (Saint-Louis, Missouri, USA): Methionine (C: 40.25 %,
115 H: 7.43 %), Glycine (C: 36.36%, H: 6.10%), Taurine (C: 19.20%, H: 5.20%), Cystine (C: 29.99%, H: 5.03%),
116 Valine (C: 51.26, H: 9.46%), Tryptophan (C: 64.69%, H: 5.92%).

117

118 **3. RESULTS**

119

120 **3.1. Thermal stability**

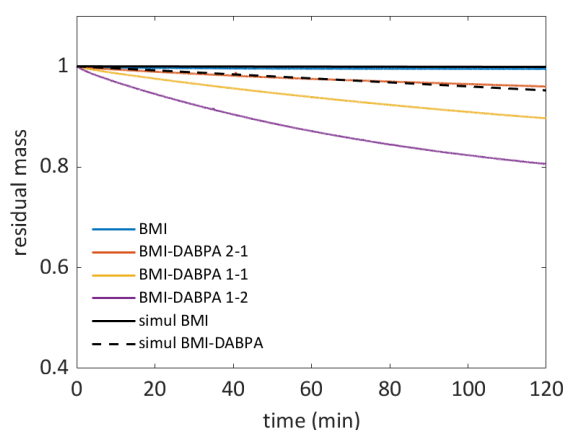
121 The thermal stability of systems was first investigated by studying in situ degradation of BMI and BMI-
122 DABPA networks using TGA either under inert atmosphere or under pure oxygen at elevated
123 temperatures (350 and 375°C) as shown in Figure 2. The following conclusions can be drawn:

124 - BMI can be considered as relatively stable under inert atmosphere (less than 1% mass loss)
125 consistently with literature data [9] but the addition of DABPA comonomer promotes thermal
126 degradation.

127 - The presence of oxygen accelerates the degradation rate.

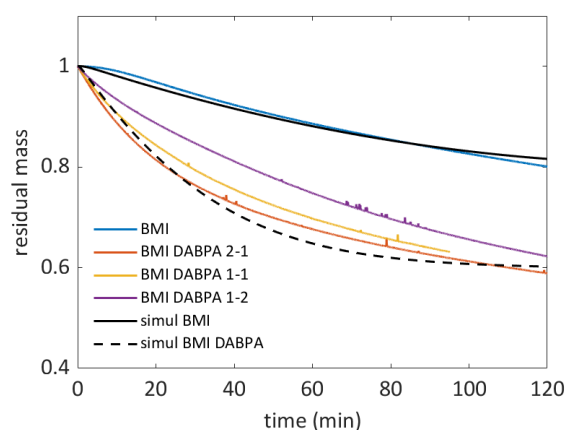
128 - In presence of oxygen, the DABPA also accelerates degradation compared to pure BMI. However,
129 differences between BMI-DABPA 2-1, BMI-DABPA 1-1 and BMI-DABPA 1-2 under oxygen are weaker
130 than for degradations under nitrogen. BMI-DABPA 1-2 always is the less stable material for ageing
131 under inert atmosphere, but this is not necessarily the case under oxygen. A definitive explanation
132 would need to finely characterize the structure of copolymers with high DABPA content (presence of
133 homopolymerized DABPA sequences) and the stabilizing effect of phenolic groups, which is out of
134 reach using basic laboratory tools used in this work.

135



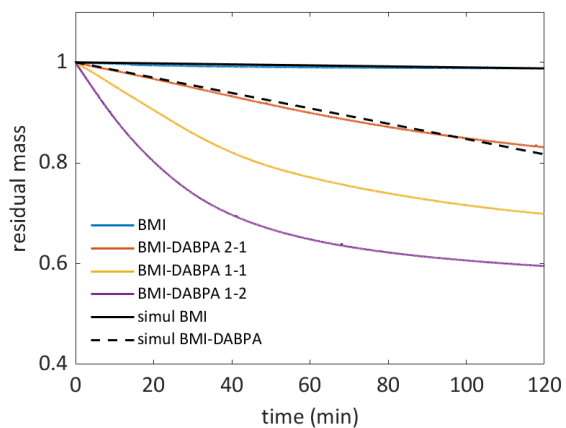
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(a)



(b)

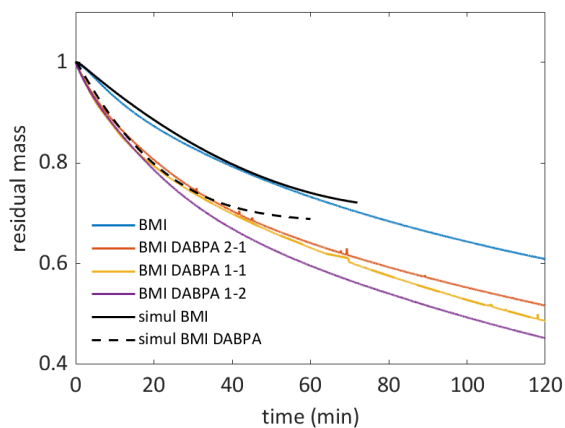
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138

139

(c)



(d)

140 **Figure 2. Mass loss curves of BMI and BMI-DABPA at 350°C (a, b) and 375°C (c, d) under inert**
 141 **atmosphere (a, c) and oxygen (b, d). Full lines correspond to kinetic modelling described in**
 142 **« Discussion » section.**

143

144 **3.2. Chemical changes**

145 Samples were first characterized by elemental analysis. Results are given in Table 1 and confirm an
 146 acceptable reliability of the method for characterizing the structure of unaged materials.

147

148

149

		BMI	BMI-DABPA 2-1	BMI-DABPA 1-1	BMI-DABPA 1-2
BMI weight ratio		1	0.699	0.538	0.368
theoretical	%C	0.704	0.738	0.757	0.776
	%O	0.179	0.156	0.144	0.131
	%H	0.039	0.051	0.057	0.064
experimental	%C	0.693	0.699	0.713	0.702
	%O	0.188	0.159	0.187	0.205

	%H	0.039	0.048	0.059	0.056
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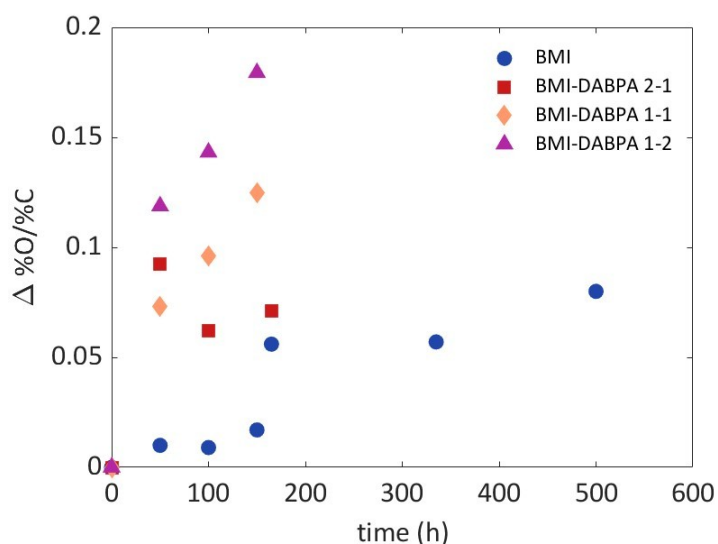
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151 **Table 1. Mass composition of the reactive mixture and elemental analysis of BMI and BMI-DABPA**
 152 **networks.**

153

154 During thermal ageing, all materials display an increase in their oxygen content (illustrated as the ratio
 155 of oxygen concentration over carbon one [²⁰]). Despite some outliers, data also confirm that BMI-
 156 DABPA copolymers oxidize faster than BMI homopolymer.

157



158

159 **Figure 3. Changes in elemental analysis.**

160

161 In order to go further in the understanding of chemical structure and its changes, FTIR spectra analysis
 162 were performed for unaged and aged samples. Spectra for unaged samples in several regions are given
 163 in Figure 4.

164 As expected from their theoretical structure given in Scheme 1, BMI homopolymers are mainly
 165 characterized by the methylene groups at 2930 cm⁻¹ (Figure 4a) and the presence of residual double
 166 bonds concentration (Figure 4d).

167 The main following differences due to DABPA comonomer can be observed:

168 - the stretching of hydroxyl bond at around 3400 cm⁻¹ (Figure 4a)

169 - the stretching of C-H in methyl groups CH_3 at 2970 cm^{-1} (Figure 4b)
170 - the C-O stretching of phenol groups at 1250 cm^{-1} (Figure 4c)
171 - the out of plane bending of alkenes in the $600 - 1000\text{ cm}^{-1}$ (Figure 4d). Here, absorbances of allyl at
172 989 and 914 cm^{-1} [13] are not detected, meanwhile 832 ($\delta_{\text{C}=\text{C}}$ in BMI) and 690 cm^{-1} ($\delta_{\text{C}=\text{C}-\text{H}}$ cis in BMI)
173 absorbances still seem present. It would suggest that networks are not fully polymerized [1]. We
174 however did not try to optimize curing degree, keeping in mind that post-curing must occur in situ
175 during the heating ramp prior to 350 and 375°C isothermal ageing for the experiments reported in
176 Figure 2.

177

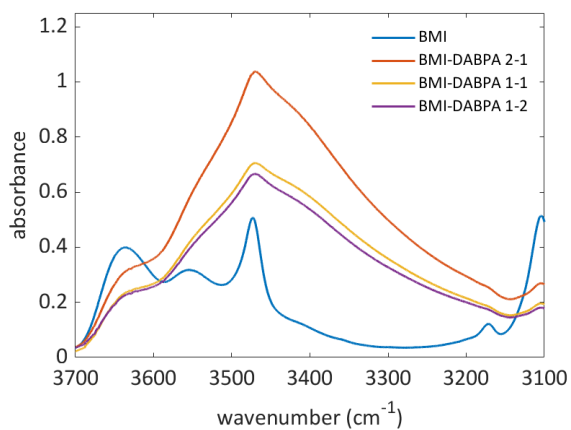
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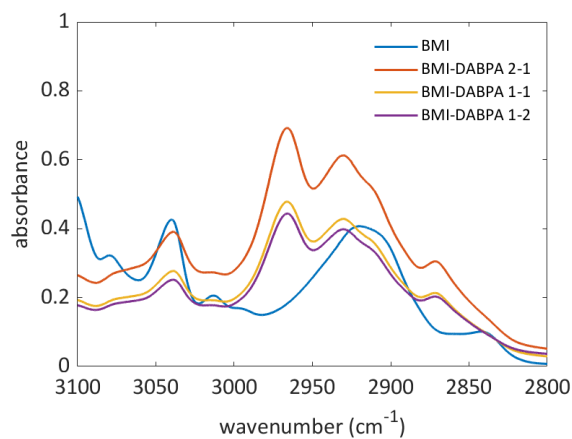
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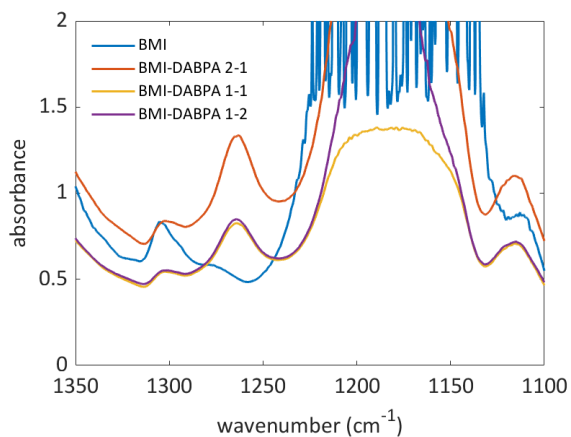
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(a)



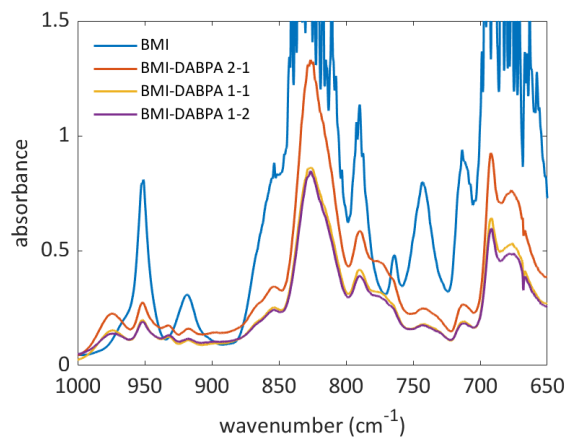
(b)



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186

(c)



(d)

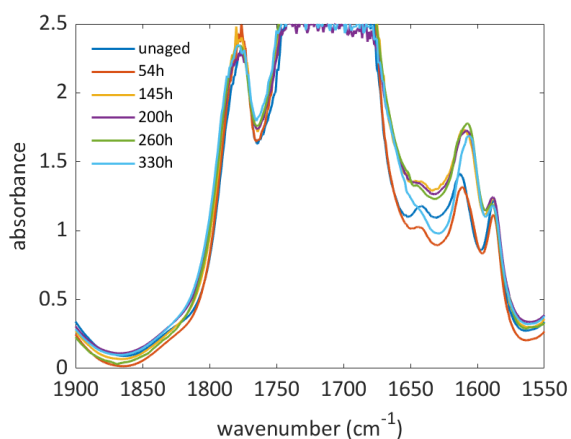
187 **Figure 4. InfraRed spectra of BMI homopolymer and BMI-DABPA copolymers in the region of**
 188 **hydroxyls (a), C-H stretching (b), fingerprint (c) and C=C double bond bending region (d).**

189

190 After thermal ageing at 160°C, the following differences (discussed in the following of this paper) were
 191 systematically observed (Figures 5 and 6):

192 - an increase in the carbonyl region, more specifically in the 1600 to 1700 cm⁻¹ wavenumber range,
 193 which could correspond to the appearance of benzophenone functions, or any other kinds of
 194 conjugated ketones, consistently with previous results [16,²¹].

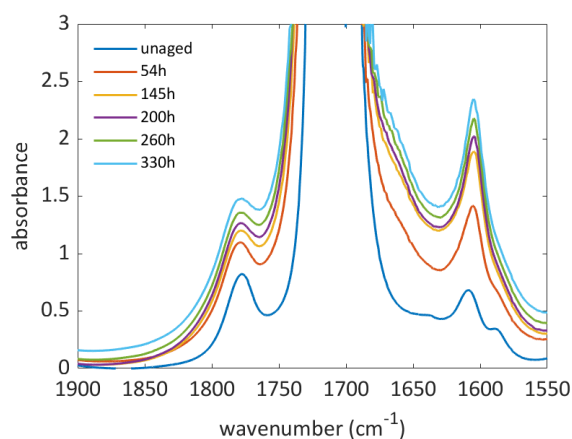
195 - the disappearance of aromatic =C-H stretching (above 3000 cm⁻¹) which may be due to volatile loss
 196 (see above) or isomerization. Actually, the appearance of a new absorbance at 930 cm⁻¹ accompanied
 197 by the increase of a sharp band at 1610 cm⁻¹, could correspond to the appearance of new >C=C< double
 198 bonds (see also Supplementary information SI-1).



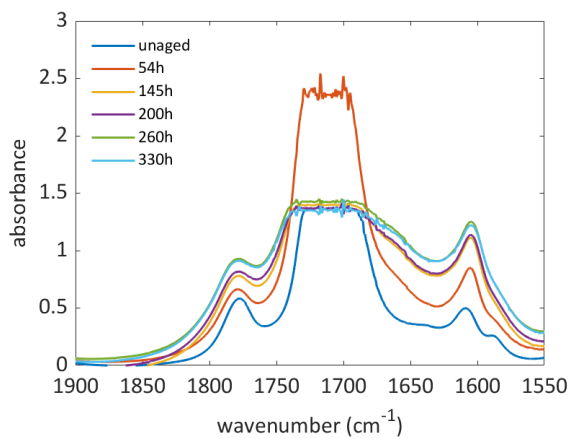
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(a)



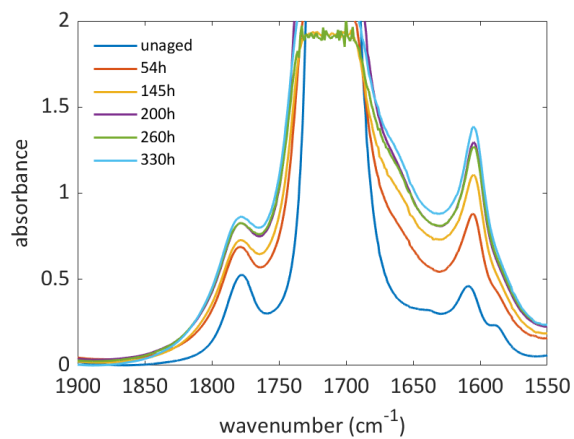
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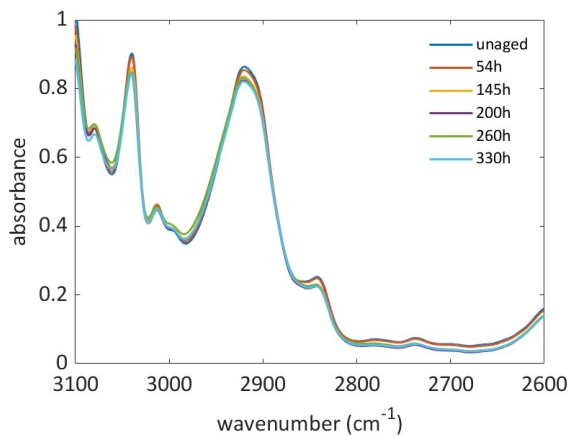


(d)

203 **Figure 5. FTIR spectra in the carbonyl region for BMI (a), BMI-DABPA 2-1 (b), BMI-DABPA 1-1 (c)**
 204 **and BMI-DABPA 1-2 (d) thermally oxidized at 160°C under air.**

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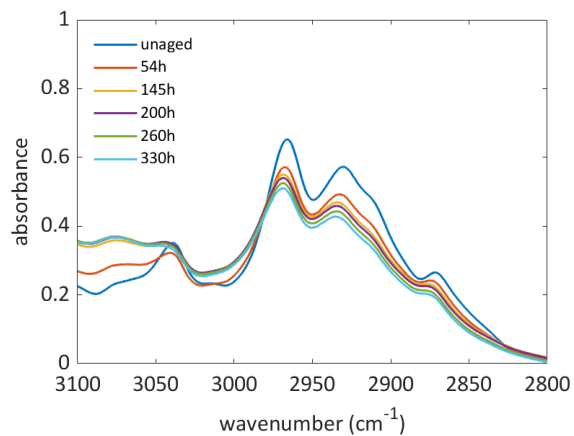
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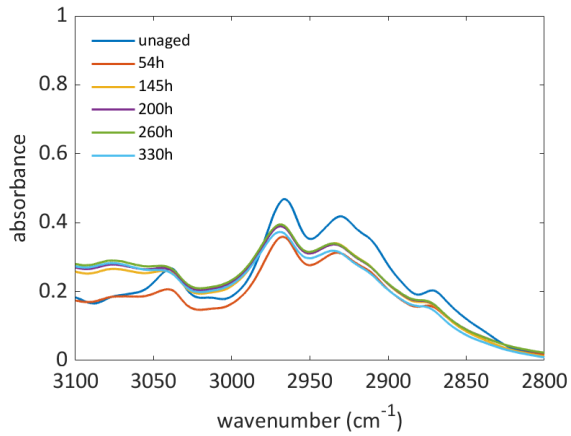
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(a)



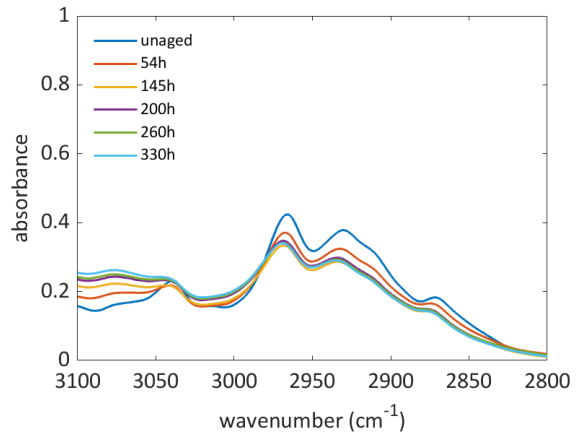
(b)



209

210

(c)



(d)

211 **Figure 6. FTIR spectra in the C-H stretching region for BMI (a), BMI-DABPA 2-1 (b), BMI-DABPA 1-1**
 212 **(c) and BMI-DABPA 1-2 (d) thermally oxidized at 160°C under air.**

213

214 Finally, our results unambiguously show that the use of DABPA as comonomer is detrimental to
 215 thermal stability of BMI based resins, either under nitrogen or in presence of oxygen.

216

217

218 **4. DISCUSSION**

219

220 The first aim of this section is to propose an explanation of the chemical changes in link with the initial
221 structure of networks, and try to explain why diallylbisphenol A lowers thermal stability of BMI-DABPA
222 copolymers. The second aim is to propose a reasonable kinetic model based on the reactivity of each
223 comonomer so as to describe the reactivity of the family of BMI-DABPA networks.

224

225 **4.1. Structural changes observed in BMI-DABPA**

226

227 Let us start by recalling the theoretical structure of BMI and BMI-DABPA 2-1 copolymers (Scheme 1). In
228 BMI homopolymers, the polymerization occurs along the double bonds (even in absence of radical
229 initiator), as depicted in Scheme 1. In BMI-DABPA copolymers, polymerization occurs in two stages: a
230 Michael addition of alkene (hold by diallylbisphenol A) followed by a Diels Alder reaction with another
231 bismaleimide group. The ideal stoichiometry is here one diallyl group for two maleimides ones.

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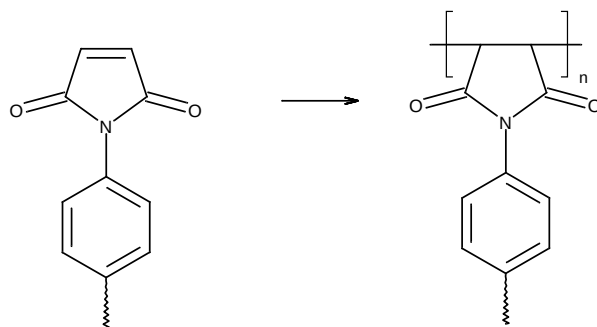
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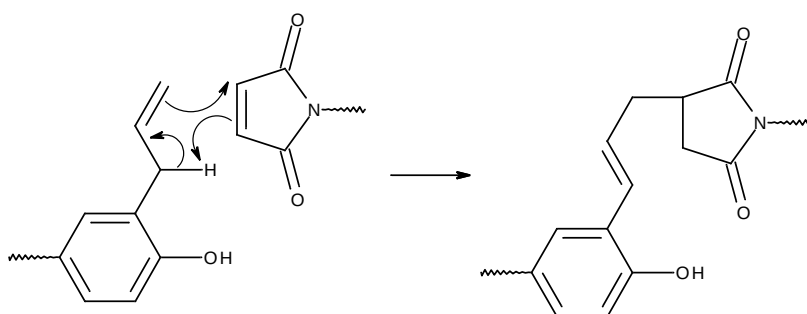
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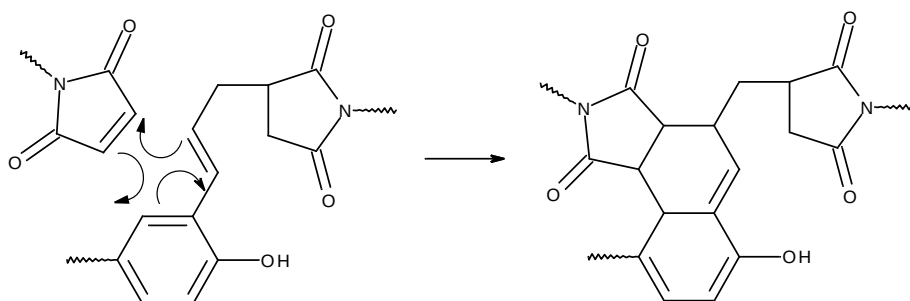
(a)



243

244

245



246

247

(b)

Scheme 1. Curing mechanism in BMI (a) and BMI-DABPA (b).

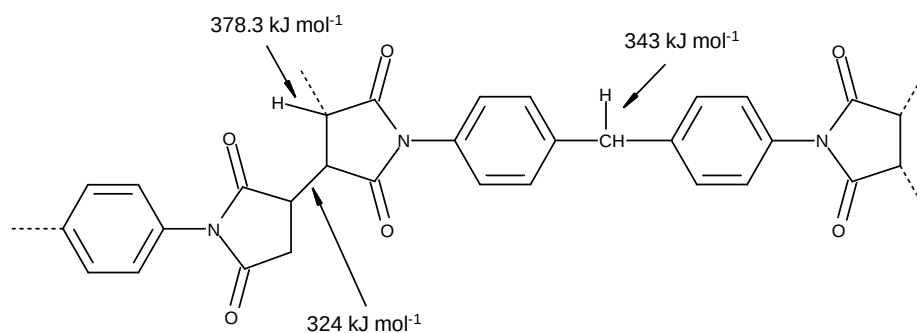
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250 Since only BMI and BMI-DABPA 2-1 correspond to well defined structures, we will focus on those two
 251 networks in the following, keeping in mind that thermal stability of BMI-DABPA 2-1, BMI-DABPA-1-1
 252 and BMI-DABPA 1-2 seem somewhat close.

253 To better understand the differences in terms of “structure-stability relationships”, some
 254 representative units of BMI homopolymer and BMI-DABPA 2-1 groups were analyzed using a recently

255 developed Machine Learning tool (Alfabet) allowing the determination of Bond Dissociation Energies,
256 and the possible « Achylle Heel » of each kind of polymer. Such an approach was recently successfully
257 tested on epoxies [22]. Using SMILES codes given in Supplementary Information SI-2, some BDE
258 corresponding to weak groups are given in Figure 7.

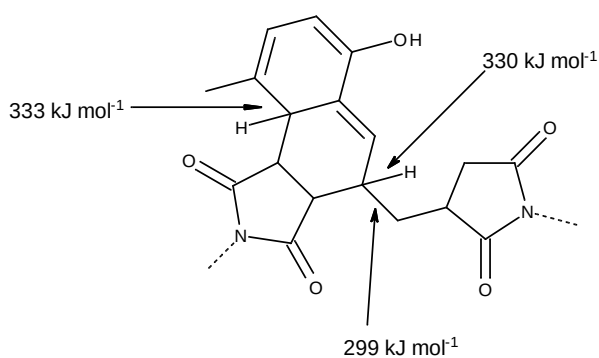
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260

261

(a)



262

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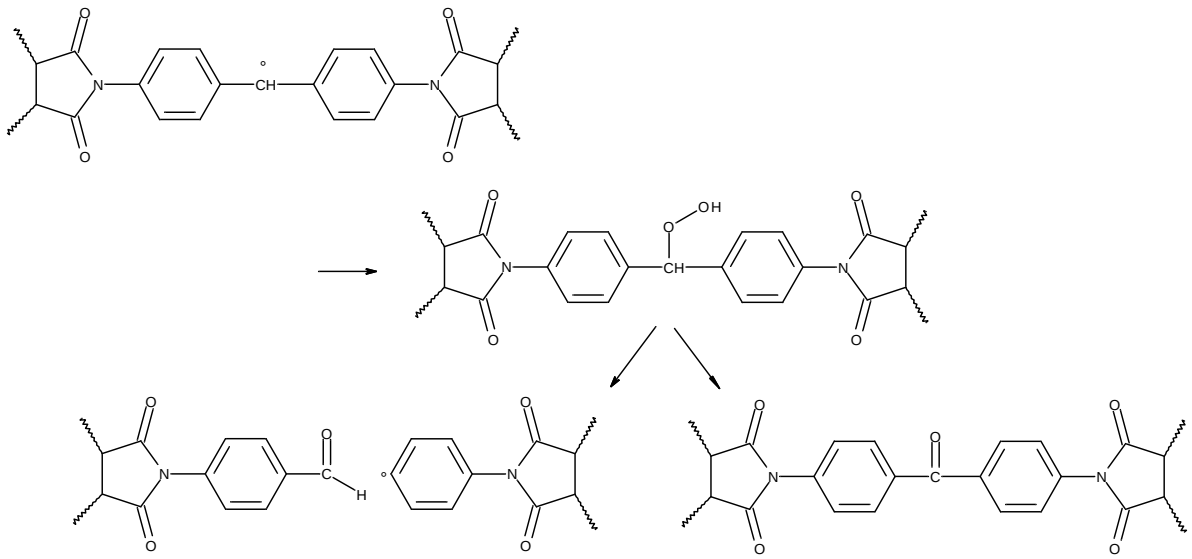
(b)

264 **Figure 7. Machine learning based estimation of some Bond Dissociation Energies in BMI (a) and**
265 **BMI-DABPA 2-1 (b).**

266

267 During oxidation, the appearance of signal located at around 1650 cm⁻¹ could come from the oxidation
268 of central methylene as depicted in Scheme 2. It is also possible to envisage that diphenyl substituted
269 methylene alkyl radicals isomerize and generate cyclohexadienone products. As proposed in Scheme
270 2b, it may explain why both absorbances of aliphatic and aromatic C-H seem to decrease (see Figure
271 6a).

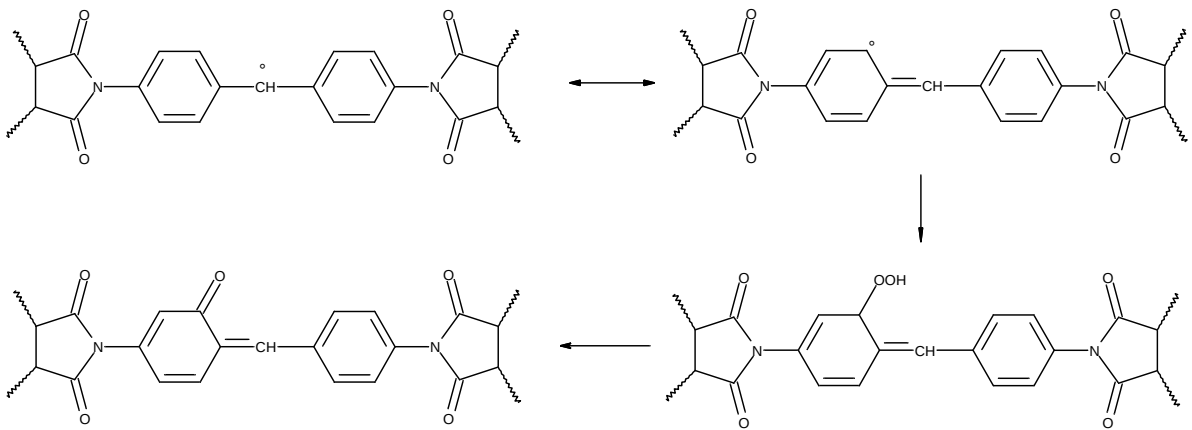
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(a)



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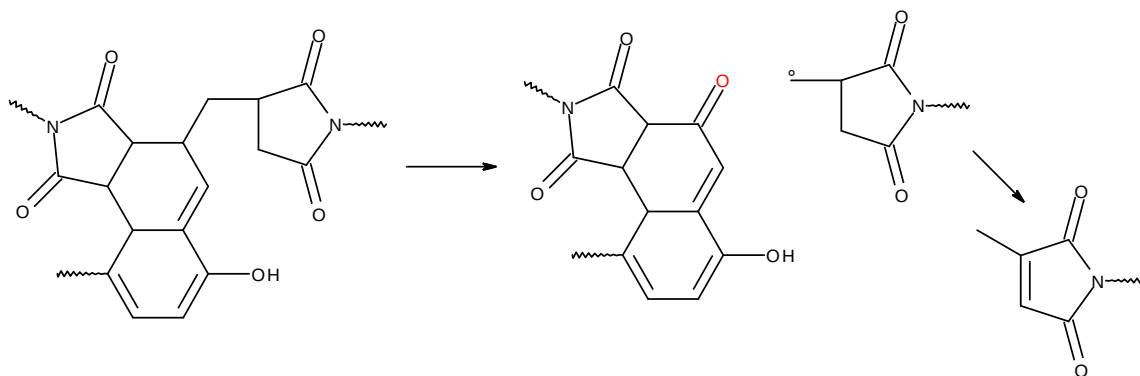
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277 **Scheme 2. Possible oxidation mechanism of BMI homopolymer) (a) or with (b).**

278

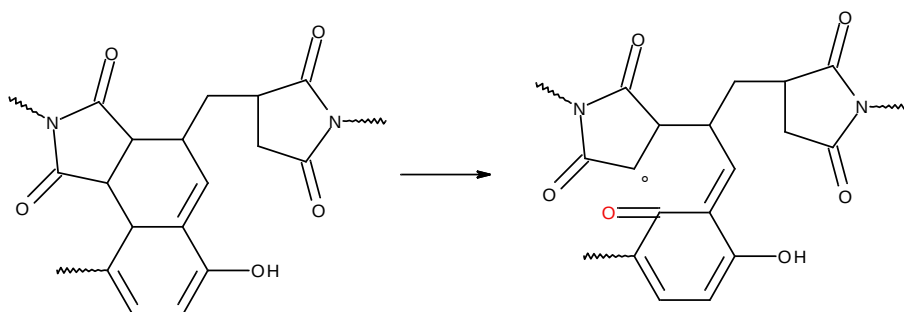
279 In the case of copolymer, it seems clear that the allylic C-H are easily oxidized into various kinds of
 280 ketones. In the case of copolymers, it is hence not surprising that the carbonyl region displays a new
 281 signal located between 1750 et 1800 cm^{-1} .

282



283
284

(a)



285
286

(b)

Scheme 3. Oxidation of allylic sites in BMI-DABPA.

287
288

289 The qualitative comparison of oxidized spectra for BMI homopolymer and BMI-DABPA copolymers
 290 suggests that copolymers are less stable than homopolymers. This is well in line with elemental analysis
 291 results. Dealing now with mass loss curves, it seems that oxidation generates more volatile compounds
 292 in the case of copolymers. We will now try to derive a kinetic model for describing the degradation
 293 kinetic and in particular mass loss curves of materials.

294

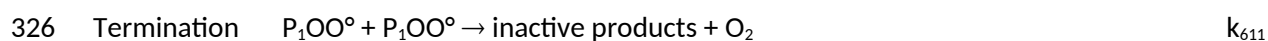
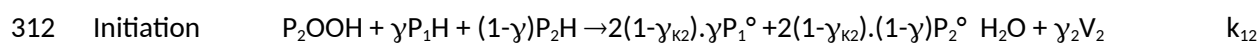
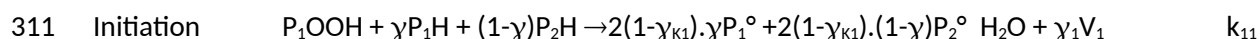
295 4.2. Kinetic modelling

296

297 We based on the general mechanistic scheme used for describing the oxidation of several polymers.
 298 This latter was in particular implemented for describing the oxidation of bismaleimide networks by
 299 Colin et al [17]. In its initial formulation, the model assumed that maleimides were the only reactive
 300 sites which is not the case here since there are strong discrepancies between BMI and BMI-DABPA 2-1.
 301 Instead of using a simple model with « genuine » constants for BMI and BMI-DABPA systems, we
 302 decided to develop a cooxidation kinetic model ^[23,24] where reactive sites for BMI (subscript 1) and
 303 DABPA (subscript 2) react independently or by crossed reactions and where the reactivity of BMI-

304 DABPA copolymers is ruled by rates constants specific to each site. Moreover, our results (in particular
 305 of mass loss data under inert atmosphere) showed the existence of a « pure » thermolytical process
 306 that we simply modeled by reaction (0) generating two alkyl radicals and (4) corresponding to their
 307 termination by coupling. The mechanistic scheme is written as follows:

308



329 Meaning of symbols are detailed in Table 2.

Symbol	Meaning
P_1H, P_2H	Unreacted substrate
P_1°, P_2°	Alkyl radical
P_1OO°, P_2OO°	Peroxy radical
P_1OOH, P_2OOH	Hydroperoxide
V_{01}, V_{02}	Volatiles generated by thermolysis
ρ_{01}, ρ_{02}	Yield for volatile generation from substrate decomposition
V_1, V_2	Volatiles generated by thermal oxidation
ρ_1, ρ_2	Yield for volatile generation from oxidation
$u_{01}M_{v01}, u_{02}M_{v02}$	Contribution to mass loss from substrate decomposition
$u_{01}M_{v01}, u_{02}M_{v02}$	Contribution to mass loss from oxidation
γ	Probability of P_1H or P_2H attack by any HO° or P_iO° radical
γ_{k1}, γ_{k2}	Yield for cage reaction $P_iO^\circ + HO^\circ \rightarrow$ inactive product (carbonyl)
k_i, k_{ij}	Rate constant
E_i, E_{ij}	Activation energy

331

332

Table 2. Signification of kinetic parameters.

333

334 The balance equation for initiation are justified in Supplementary Information SI-3. This scheme leads
 335 to the differential system given in Supplementary Information SI-4. It allows mass loss to be predicted
 336 from :

337

$$338 \quad \frac{d m}{dt} = \frac{32}{\rho} \left(k_{21} [P_1^\circ] [O_2] + k_{22} [P_2^\circ] [O_2] - k_{611} [P_1OO^\circ]^2 - k_{612} [P_1OO^\circ] [P_2OO^\circ] - k_{622} [P_2OO^\circ]^2 \right) - \frac{(18 + v_1 M_{v1})}{\rho}$$

339

340 System was solved using ODE23s from Matlab® using the following initial conditions at $t = 0$, $[P_1^\circ]_0 =$
 341 $[P_2^\circ]_0 = [P_1OO^\circ]_0 = [P_2OO^\circ]_0$

342

343 The initial substrate concentration was calculated as follows:

344 ① For pure BMI, each monomer holds a diaryl methylene group so that:

345
$$[P_1H]_0 = \frac{\rho}{M_1} = 3.6 \text{ mol l}^{-1}$$

346 M_1 being the molar mass of BMI (358 g mol⁻¹)

347 ② For BMI-DABPA 2-1, concentration in BMI comonomer and diallylbisphenol A is weighted by the
348 weight ratio of BMI in the mixture considering that each diallylbisphenol A holds 4 reactive sites:

349
$$[P_1H]_0 = \frac{\rho}{M_1} \cdot \frac{2M_1}{2M_1 + M_2} = 2.5 \text{ mol l}^{-1}$$

350
$$[P_2H]_0 = 4 \frac{\rho}{M_2} \cdot \frac{M_2}{2M_1 + M_2} = 5 \text{ mol l}^{-1}$$

351 M_2 being the molar mass of DABPA (308 g mol⁻¹)

352 The total initial concentration in hydroperoxide was arbitrarily fixed equal to 0.001 mol l⁻¹ so that:

353 - For pure BMI:

354
$$[P_1OOH]_0 = 0.001 \text{ mol l}^{-1}$$

355 - For BMI-DABPA 2-1 copolymer:

356
$$[P_1OOH]_0 = 0.00035 \text{ mol l}^{-1}$$

357
$$[P_2OOH]_0 = 0.00065 \text{ mol l}^{-1}$$

358

359 The oxygen concentration was fixed equal to 0.04 mol l⁻¹ consistently with [25].

360

361 The main complexity is the high number of parameters in the kinetic model. Many of them were fixed
362 in order to have the less possible number of adjustable parameters. Here, we implemented the
363 following approach:

364 - Rate constants were first determined for pure BMI and then for BMI-DABPA 2-1.

365 - Under nitrogen, only k_{oi} and k_{4ij} are needed to fit the curves of mass loss. Those values were then
366 utilized for simulating degradation under oxygen without change.

367 - The rate constants k_{01} , k_{02} and the yields for volatile release were adjusted from the parametric study
368 presented in Figure 2 by fitting the curves under inert atmosphere. Figure 8a illustrates a parametric
369 study for the k_0 value.

370 - According to the analysis of oxidation mechanisms presented in the previous section, reactive sites
371 were identified because of their bond dissociation energies. It allows the estimation of the rate
372 constants values for the $\text{POO}^\circ + \text{PH} \rightarrow \text{POOH} + \text{P}^\circ$ values from the semi-empirical values proposed by
373 Korcek et al [26]:

$$374 \quad \log_{10} k_3^{\text{sec-POO}^\circ}(30^\circ\text{C}) = 16.4 - 0.2 * \text{BDE}$$

$$375 \quad E_3^{\text{sec-POO}^\circ} = 0.55 \times (\text{BDE} - 62.5)$$

$$376 \quad \log_{10} k_3^{\text{tert-POO}^\circ}(30^\circ\text{C}) = 15.4 - 0.2 * \text{BDE}$$

$$377 \quad E_3^{\text{tert-POO}^\circ} = 0.55 \times (\text{BDE} - 65)$$

378 - The rate constants for termination (k_{4ij} , k_{5ij} , k_{6ij}) should in principle be determined from a study under
379 varying oxygen pressures [27]. In the absence of this latter, we used the following assumptions: (i) $10^{10} >$
380 $k_{4ij} > k_{5ij} \gg k_{6ij}$, (ii) $k_{5ij} = 5 \times 10^8 \text{ l mol}^{-1} \text{ s}^{-1}$ and $k_{6ij} = 10^5 \text{ l mol}^{-1} \text{ s}^{-1}$ keeping in mind that the rate constant for
381 the termination between two POO° (k_{6ij}) mainly influences the kinetics under high oxygen pressures,
382 (iii) $k_{412} = (k_{411} \times k_{422})^{1/2}$ [23,24]. The effect of k_{4ij} is illustrated by the parametric study given in Figure 8f.
383 Let us precise that the termination product of two radicals can be a double bond, consistently with
384 experimental observations (Figure 5).

385 Finally, k_{1ij} , k_{2ij} , k_{0i} and k_{4ij} , \square_{ki} were the remaining adjustable parameters. We assumed that $k_{21} = k_{22}$. The
386 results of a parametric study for those constants are depicted in Figures 8b, 8c and 8d. For
387 summarizing:

388 - k_{1i} was adjusted basing on the initial concavity of the curve in Figure 2. We also checked its consistency
389 with comparable results obtained by Colin et al [17] (Figure 10b).

390 - k_{2i} was adjusted on the mass loss rate at early stages. It must however be recognized that several $k_{2,}$
391 k_4 sets would lead to comparable simulations.

392 - k_{3ij} were fixed but their influence is depicted for example in Figure 8e.

393

394 Another attempt to validate the model was to fit the data by Colin et al [17], despite the fact that the
395 formulation used in their work may not exactly match with the BMI and BMI DABPA 2-1 studied in this

396 work. Results are given in Figure 9 where two cases were considered: the fictive case of a pure BMI
397 resin and the case of BMI DABPA 2-1 (on which rate constants were adjusted in a consistent manner
398 with rate constants determined from Figure 9).

399

400 Finally, it can be seen that kinetic model describes the mass loss kinetics (Figures 2 and 9) in a wide
401 range of temperatures (180 to 375°C) with elementary rate constants obeying Arrhenius law with
402 reasonable activation energies (Figure 10): $E_{1i} \sim 140 \text{ kJ mol}^{-1}$, $E_{2i} \sim E_{4i} \sim 15 \text{ kJ mol}^{-1}$.

403 Further improvements can be envisaged in order to optimize the fits under oxidative conditions:

404 - here, we assumed quasi ideal structures which may not be the case for real networks. For example, BMI-
405 DABPA networks can possibly BMI or DABPA homopolymerized sequence. Their reactivity must be
406 understood and some reactions should be added to the model. However, it is first needed to evidence
407 the presence of such sequences in networks.

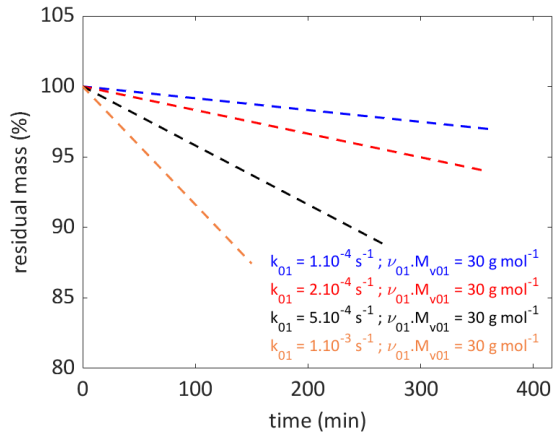
408 - the participation of sites having a lower reactivity (such as the -CH-CH-CH-CH- sequence in pure BMI).

409 - the actual effect of curing degree could also be taken into account [28].

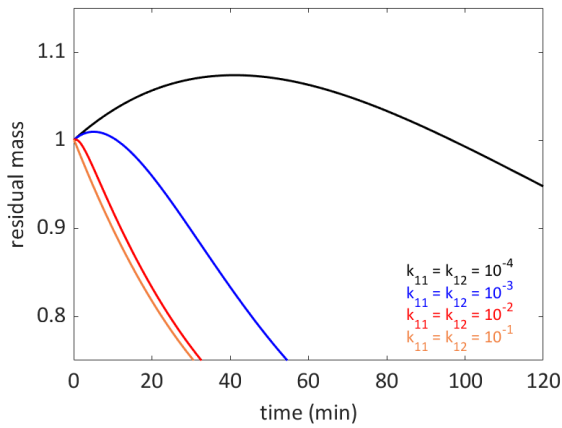
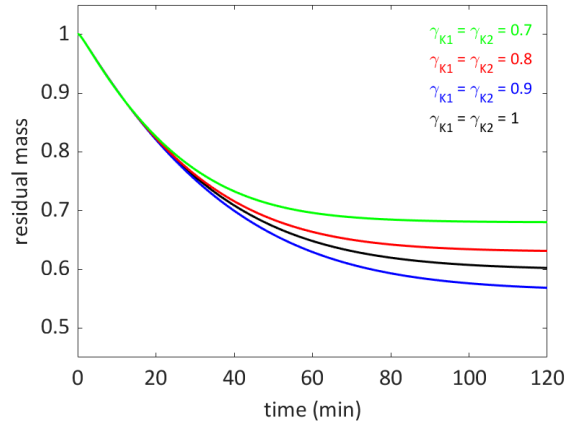
410 - we assumed that some parameters (namely $\nu_1 M_{v1}$, $\nu_2 M_{v2}$, $\nu_{01} M_{v01}$, $\nu_{02} M_{v02}$) remain constant during
411 the whole timescale under consideration which is clearly an approximation.

412 - in particular, the possibility of retro Diels Alder occurring under nitrogen for BMI-DABPA is to
413 investigate.

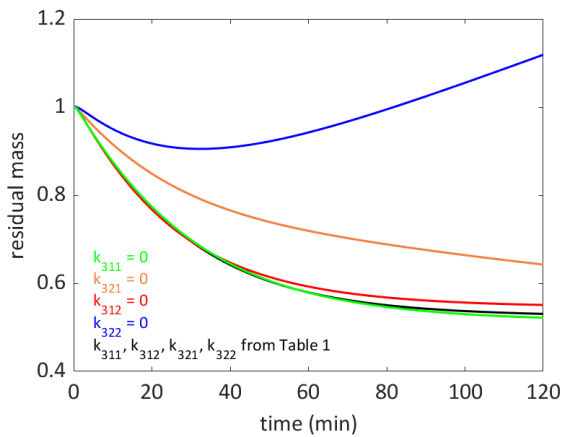
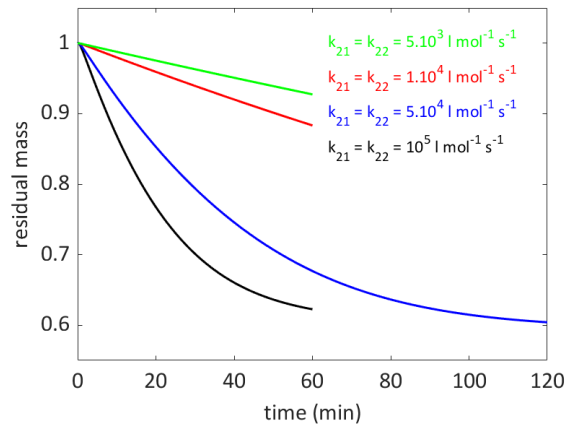
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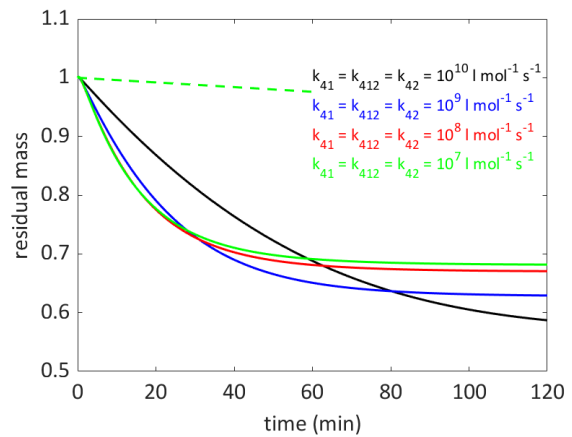


Figure 8. Parametric study with dashed lines: under inert atmosphere, full lines: under oxygen,
 using with parameters corresponding to 350°C (see Table 2).

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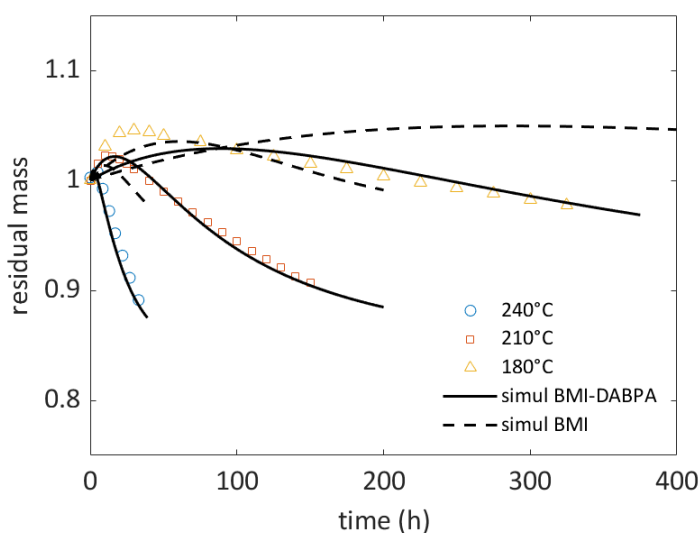
	180°C	210°C	240°C	350°C	375°C	E_a (kJ mol ⁻¹)
k_{11} (s ⁻¹)	4×10^{-7}	2.75×10^{-6}	2.5×10^{-5}	1.1×10^{-2}	2.75×10^{-2}	142.4
k_{12} (s ⁻¹)	2.7×10^{-6}	1.65×10^{-5}	1.3×10^{-5}	5.0×10^{-2}	1.4×10^{-1}	139.3
k_{21} (l mol ⁻¹ s ⁻¹)	2.5×10^4	3.1×10^4	3.75×10^4	6.5×10^4	7.5×10^4	13.6
k_{22} (l mol ⁻¹ s ⁻¹)	2.5×10^4	3.1×10^4	3.75×10^4	6.5×10^4	7.5×10^4	13.6
k_{311} (l mol ⁻¹ s ⁻¹)	366	768	1912	9450	13200	44.9
k_{321} (l mol ⁻¹ s ⁻¹)	17	46	58	292	391	39.1
k_{312} (l mol ⁻¹ s ⁻¹)	588	1100	1475	9201	12210	38.0
k_{322} (l mol ⁻¹ s ⁻¹)	28	33	75	285	362	32.2
k_{411} (l mol ⁻¹ s ⁻¹)	5×10^8	7×10^8	9×10^8	2.2×10^9	2.4×10^9	20.0
k_{422} (l mol ⁻¹ s ⁻¹)	8×10^8	1.15×10^9	1.5×10^9	3.2×10^9	3.2×10^9	18.4
k_{412} (l mol ⁻¹ s ⁻¹)	$(k_{411} \times k_{422})^{0.5}$					0
k_{511} (l mol ⁻¹ s ⁻¹)	5×10^8	5×10^8	5×10^8	5×10^8	5×10^8	0
k_{512} (l mol ⁻¹ s ⁻¹)	5×10^8	5×10^8	5×10^8	5×10^8	5×10^8	0
$k_{512} = k_{521}$ (l mol ⁻¹ s ⁻¹)	$(k_{511} \times k_{522})^{0.5}$					0
$k_{611}, k_{612}, k_{622}$	10^8	10^8	10^8	10^8	10^8	0
γ_{k1}	1	1	1	1	1	
γ_1	0	0	0	0	0	
γ_{k2}	1	1	1	0.8	0.8	
γ_2	0	0	0	0	0	
$\nu_1 M_{\nu_1}$ (g mol ⁻¹)	25	29	32.5	85	117.5	

$\nu_2 M_{v2}$ (g mol ⁻¹)	45	50	51.5	130	95	
ρ	1300	1300	1300	1300	1300	
k_{01} (s ⁻¹)	6×10^{-9}	4×10^{-8}	2×10^{-7}	5.5×10^{-5}	1.5×10^{-4}	126.9
$\nu_{01} M_{v01}$ (g mol ⁻¹)	0	0	0	1	4	
k_{02} (s ⁻¹)	7×10^{-8}	5×10^{-7}	3.0×10^{-6}	8.5×10^{-4}	1.6×10^{-3}	129.8
$\nu_{02} M_{v02}$ (g mol ⁻¹)	0	0	0	1.75	2	

424

425

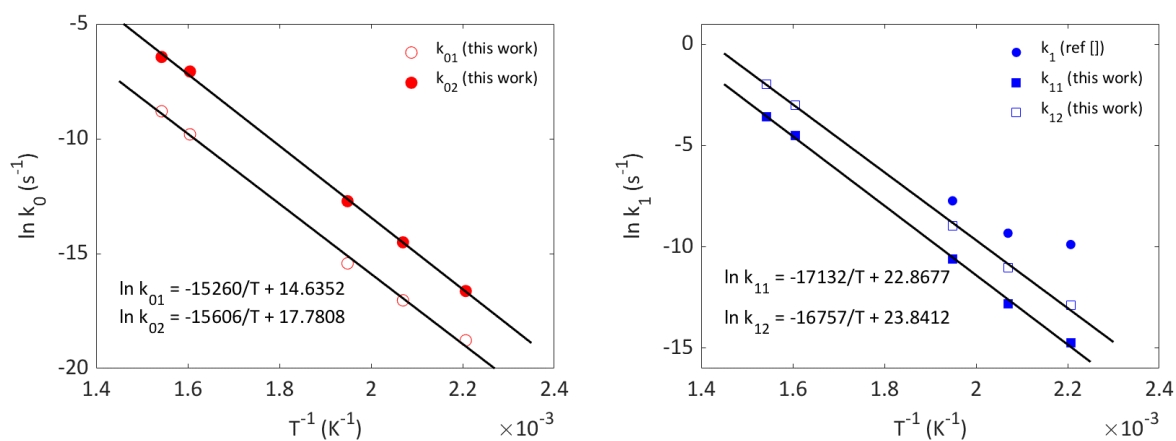
Table 3. Kinetic parameters for simulations given in Figures 2 and 9.



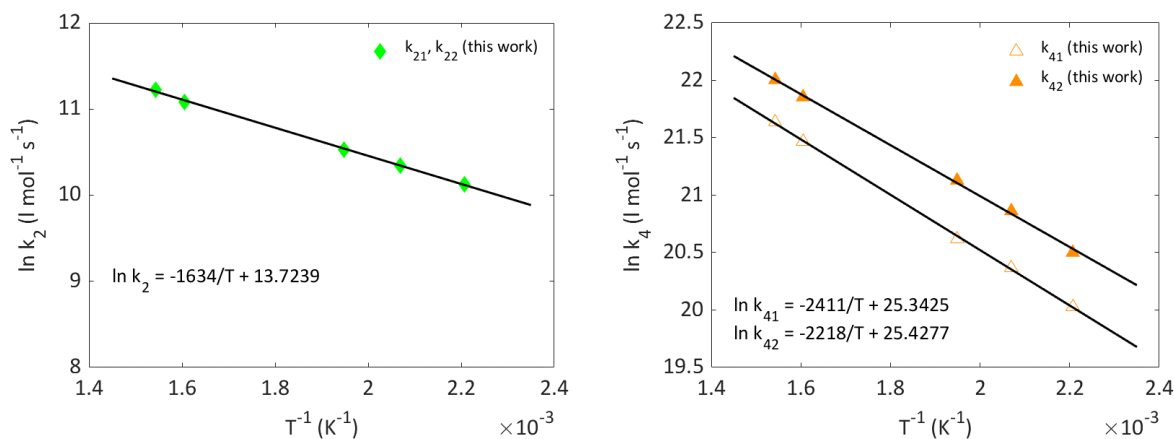
426

427 Figure 9. Simulation of results by Colin et al [17] with kinetic model working with $[P_1H]_0 = 2.5$ and
428 $[P_2H]_0 = 5 \text{ mol l}^{-1}$ (BMI-DABMA 2-1) or $[P_1H]_0 = 3.6 \text{ mol l}^{-1}$ and $[P_2H]_0 = 0$ (pure BMI).

429



430



431

432

Figure 10. Arrhenius diagram for rate constants.

433 CONCLUSIONS

434 In this paper, networks made from bismaleimide and diallylbisphenol A were synthesized and
 435 submitted to isothermal ageing at various temperatures under inert atmosphere and or under air.
 436 Results clearly show that diallyl comonomer lowers thermal stability of BMI resins. This was confirmed
 437 by an estimation of the Bond Dissociation Energies of structural units of BMI and BMI-DABPA since
 438 DABPA displays some weak bonds that can more easily undergo homolysis and radical attack. Basing on
 439 those observations, a kinetic model for co-oxidation was proposed. The complexity of such modelling
 440 tools is the high number of parameters that can influence the simulations. In order to decrease the
 441 number of adjustable parameters, some rate constants values were and some other were identified
 442 from a parametric study. Finally, the kinetic model displays an encouraging capability to simulate mass
 443 loss induced by thermal ageing of BMI based networks as confirmed by comparing its prediction with
 444 literature data. Its validation process can be pursued by performing long term ageing runs at lower
 445 temperatures.

446

447 REFERENCES

- 1 ¹ M.-F. Grenier-Loustalot, L. Da Cunha. Study of molten-state polymerization of bismaleimide monomers by solid-state ^{13}C n.m.r. and FTi.r. *Polymer* 39 (1998) 1833-1843.
- 2
- 3 ² J. Zhu. Curing behavior and properties of 4,4' bismaleimidodiphenylmethane and O,O' Diallyl bisphenol A: effect of peroxides and hybrid silsesquioxane addition. Michigan State University (2012).
- 4
- 5 ³ A. Seris, M. Feve, F. Mechin, J.P. Pascault. Thermally and Anionically Initiated Cure of Bismaleimide Monomers. *Journal of Applied Polymer Science* 48 (1993) 257-269.
- 6
- 7 ⁴ R.J. Iredale, C. Ward, I. Hamerton. Modern advances in bismaleimide resin technology: A 21st century
 8 perspective on the chemistry of addition polyimides. *Progress in Polymer Science* 69 (2017) 1-21.
- 9 ⁵ J. Hao, L. Jiang, X. Cai. Investigation on bismaleimide bearing polysiloxane (BPS) toughening of 4,4'-bismaleimido
 10 diphenylmethane (BMI) matrix—synthesis, characterization and toughness. *Polymer* 37 (1996) 3721-3727.

-
- 11 ⁶ J. Xu, H. Wu, O.P. Mills, P.A. Heiden. Morphological Investigation of Thermosets Toughened with Novel
12 Thermoplastics. I. Bismaleimide Modified with Hyperbranched Polyester. *Journal of Applied Polymer Science* 72
13 (1999) 1065-1076.
- 14 ⁷ Q. Lin, R. Zheng, P. Tian. Preparation and characterization of BMI resin/graphite oxide nanocomposites. *Polymer*
15 *Testing* 29 (2010) 537-543
- 16 ⁸ X. Jiang, F. Chu, X. Luo, Y. Hu, W. Hu. Exploring the effects of cardanol-based co-curing agents with different
17 phosphorus structures on the mechanical and flame-retardant properties of bismaleimide resin. *Composites Part*
18 *B: Engineering* 241 (2022) 110047.
- 19 ⁹ H. Tang, N. Song, Z. Gao, X. Chen, Q. Zhou. Preparation and properties of high performance bismaleimide resins
20 based on 1,3,4-oxadiazole-containing monomers. *European Polymer Journal* 43 (2007) 1313-1321.
- 21 ¹⁰ R. Torrecillas, N. Regnier, B. Mortaigne. Thermal degradation of bismaleimide and bisnadimide networks—
22 products of thermal degradation and type of crosslinking points. *Polymer Degradation and Stability* 51 (1996)
23 307-318.
- 24 ¹¹ K.S. Santhosh Kumar, C.P. Reghunadhan Nair, R. Sadhana, K.N. Ninan. Benzoxazine-bismaleimide blends:
25 Curing and thermal properties. *European Polymer Journal* 43 (2007) 5084-5096.
- 26 ¹² C. Gouri, C.P Reghunadhan Nair, R. Ramaswamy, K.N Ninan. Thermal decomposition characteristics of Alder-
27 ene adduct of diallyl bisphenol A novolac with bismaleimide: effect of stoichiometry, novolac molar mass and
28 bismaleimide structure. *European Polymer Journal* 38 (2002) 503-510.
- 29 ¹³ M. Neda, K. Okinaga, M. Shibata. High-performance bio-based thermosetting resins based on bismaleimide
30 and allyl-etherified eugenol derivatives. *Materials Chemistry and Physics* 148 (2014) 319-327.
- 31 ¹⁴ X. Colin, C. Marais, J. Verdu. Kinetic modelling and simulation of gravimetric curves: application to the oxidation
32 of bismaleimide and epoxy resins. *Polymer Degradation and Stability* 78 (2002) 545-553.
- 33 ¹⁵ X. Colin, C. Marais, J. Verdu. Thermal oxidation kinetics for a poly(bismaleimide). *Journal of Applied Polymer*
34 *Science* Volume 82 (2001) 3418-3430.
- 35 ¹⁶ C. Daily, D.J. Barnard, R.W. Jones, J.F. McClelland, N. Bowler. Dielectric and infrared inference of thermo-
36 oxidative aging of a bismaleimide composite material. *Composites Part B: Engineering* 101 (2016) 167-175.
- 37 ¹⁷ X. Colin, C. Marais, J. Verdu. Kinetic modelling and simulation of gravimetric curves: application to the oxidation
38 of bismaleimide and epoxy resins. *Polymer Degradation and Stability* 78 (2002) 545-553.
- 39 ¹⁸ J. Decelle, N. Huet, V. Bellenger. Oxidation induced shrinkage for thermally aged epoxy networks. *Polymer*
40 *Degradation and Stability* 81 (2003) 239-248.
- 41
- 42 ¹⁹ S. Konica, T. Sain. A homogenized large deformation constitutive model for high temperature oxidation in
43 fiber-reinforced polymer composites. *Mechanics of Materials* 160 (2021) 103994.
- 44
- 45 ²⁰ L. Xue, W. Fan, F. Wu, Y. Zhang, K. Guo, J. Li, L. Yuan, W. Dang, R. Sun. The influence of thermo-oxidative aging
46 on the electromagnetic absorbing properties of 3D quasi-isotropic braided carbon/glass bismaleimide composite.
47 *Polymer Degradation and Stability* 168 (2019) 108941.
- 48 ²¹ W. Shaoquan, D. Shangli, G. Yu, S. Yungang. Thermal ageing effects on mechanical properties and barely visible
49 impact damage behavior of a carbon fiber reinforced bismaleimide composite. *Materials & Design* 1155 (2017)
50 213-223.
- 51 ²² R. Delannoy, V. Tognetti, E. Richaud. Experimental and theoretical insights on the thermal oxidation of epoxy-
52 amine networks. *Polymer Degradation and Stability* 206 (2022) 110188.
- 53 ²³ E. Richaud, B. Fayolle, J. Verdu, J. Rychlý. Co-oxidation kinetic model for the thermal oxidation of polyethylene-
54 unsaturated substrate systems. *Polymer Degradation and Stability* 98 (2013) 1081-1088.
- 55 ²⁴ M. Touffet, P. Smith, O. Vitrac. A comprehensive two-scale model for predicting the oxidizability of fatty acid
56 methyl ester mixtures. *Food Research International* 173 (2023) 113289.

-
- 57 ²⁵ X. Colin, C. Marais, J. Verdu. Thermal oxidation kinetics for a poly(bismaleimide). *Journal of Applied Polymer*
58 *Science* 82 (2001) 3418-3430.
- 59 ²⁶ S. Korcek, J.H.B. Chenier, J.A. Howard, K.U. Ingold. Absolute Rate Constants for Hydrocarbon Autoxidation. XXI.
60 Activation Energies for Propagation and the Correlation of Propagation Rate Constants with Carbon-Hydrogen
61 Bond Strengths. *Canadian Journal of Chemistry* 50 (1972) 2285 - 2297.
- 62 ²⁷ E. Richaud, F. Farcas, P. Bartoloméo, B. Fayolle, L. Audouin, J. Verdu. Effect of oxygen pressure on the oxidation
63 kinetics of unstabilised polypropylene. *Polymer Degradation and Stability* 91 (2006) 398-405.
- 64 ²⁸ J. Delozanne, J.S. Montana, A. Guinault, N. Desgardin, N. Cuvillier, E. Richaud. Thermal ageing of bonded
65 assemblies. Effect of adhesive curing degree. *The Journal of Adhesion* 99 (2023), 911-929.